



REPORT

National Instrument 43-101 Technical Report for the Hollinger Tailings Project, Timmins, Ontario

Report Date: January 9, 2026

Resource Effective Date: November 25, 2025

Submitted to:

STLLR Gold Inc.

161 Bay St.,
Suite 2410,
Toronto, Ontario, Canada
M5J 2S1

Submitted by:

WSP CANADA INC. as Report Assembler of the work prepared
by or under the supervision of the Qualified Persons Named as Authors:
Brian Thomas, P.Geo., WSP Canada Inc.
David Jin, P.Eng., WSP Canada Inc.

CA0057927.7089-001-R-Rev0

January 9, 2026



Date and Signature Page

This Technical Report on the Hollinger Tailings Project is submitted to STLLR Gold Inc. (STLLR) and is dated January 9, 2026. The resource effective date is November 25, 2025.

Qualified Person	Professional Designation	Employer	Responsible for Parts	Signature
Brian Thomas	P.Geo.	WSP Canada Inc.	Items 1.1-1.5, 1.7, 1.8.1, 1.8.2, 1.8.4, 2-12, 14, 15-22, 23, 24, 25.1, 25.2, 25.4, 26.1, 26.2, 26.4, 27	<i>Signed and sealed by</i> Brian Thomas, P.Geo.
David Jin	P.Eng.	WSP Canada Inc.	Items 1.6, 1.8.3, 1.8.4, 12.3, 13, 25.3, 25.4, 26.3, 26.4, 27	<i>Signed and sealed by</i> David Jin, P.Eng.

NOTICE TO READERS

This National Instrument 43-101 Technical Report for STLLR was prepared and executed by the Qualified Persons named herein as Authors. This Technical Report contains the expressions of professional opinions of the Authors based on (i) information available at the time of preparation, (ii) data supplied by STLLR, and (iii) the assumptions, conditions, and qualifications set forth in this Technical Report. The quality of information, conclusions, and estimates contained herein are consistent with the stated levels of accuracy as well as the circumstances and constraints under which the mandate was performed. The QPs do not disclaim any responsibility for the information, conclusions, and estimates contained in this Technical Report.

This Technical Report was prepared in accordance with a contract between WSP and STLLR which contract permits STLLR to file this Technical Report as a Technical Report with Canadian securities regulators pursuant to National Instrument 43-101 - Standards of Disclosure for Mineral Projects. Except for the purposes legislated under Canadian securities law, any use of this Technical Report by any third party is at that party's sole risk. The responsibility for this disclosure remains with STLLR. The user of this document should ensure that this is the most recent Technical Report for the Property as it is not valid if a new Technical Report has been issued.

Abbreviations

Abbreviation	Definition
%	percent
>	greater than
<	less than
°	degrees
°C	degrees Celsius
µm	microns
3D	three-dimensional
3xSD	3x Standard Deviation
AAS	Atomic Absorption Spectroscopy
ALS	ALS Laboratories Inc.
ALS	ALS Geochemistry Laboratories
Au	gold
BV	Bureau Veritas Laboratories
CA\$	dollar (Canadian)
CIM	Canadian Institute of Mining
cm	centimetre
cm ³	cubic centimetre
CP	Companion Policy
CRM	Certified Reference Material
CV	coefficient of variation
Datamine	Datamine Studio RM
DO	Dissolved Oxygen
DPFZ	Destor Porcupine Fault Zone
DSI	Dam Safety Inspection
ECA	Environmental Compliance Approval
EM	electromagnetic
Erocon	Erocon Waste Management Ltd.
FA	Financial Assurance
ft	feet
ft ³	cubic feet
ft ³ /ton	cubic feet per short ton
g	gram
g/cm ³	grams per cubic centimetre
g/L	gram per litre
g/t	grams per tonne
GPS	Global Positioning System
ha	hectare
ID	Identification
ID2	Inverse Distance squared
ID3	Inverse Distance cubed
k	kilo (thousand)
Kayorum	Kayorum Gold Mines Ltd.
kg	kilogram
kg/m ³	kilograms per cubic metre
km	kilometre
KP	Knight Piésold
LIMS	Laboratory Information Management Systems
m	metre
m ³	cubic metre
metre	m
MIBC	methyl isobutyl carbinol

Abbreviation Definition	
mm	millimetre
MRE	Mineral Resource Estimate
MRMR	Mineral Resource / Mineral Reserve
Mt	million tonnes
NaCN	sodium cyanide
NI	National Instrument
NN	Nearest Neighbour
NSR	Net Smelter Royalty
ON	Ontario
Oz	Troy ounces
oz/t	Troy ounce per short ton
PAX	potassium amyl xanthate
PDAC	Prospectors and Developers Association of Canada
POX	pressure oxidation
PPM	parts per million
PPP	Precise Point Positioning
QA/QC	Quality Assurance and Quality Control
QP	Qualified Person
RMR	Rock Mass Rating
RPEEE	Reasonable Prospects for Eventual Economic Extraction
S	Sulphur
SD	Standard Deviation
SOW	Scope of Work
SPT	Standard Penetration Testing
STLLR	STLLR Gold Inc.
the Project	Hollinger Tailings Project
ton	Imperial short ton
tpd	tonnes per day
US\$	dollar (American)
UTM	Universal Transverse Mercator
WSP	WSP Canada Inc.

Table of Contents

1.0	SUMMARY	1-1
1.1	Introduction	1-1
1.2	Property Description and Ownership	1-1
1.3	Geology and Mineralization	1-1
1.4	Exploration and Drilling	1-2
1.5	Sample Preparation, QA/QC and Security.....	1-3
1.6	Mineral Processing and Metallurgical Testing	1-4
1.7	Mineral Resource Estimates	1-4
1.8	QP's Conclusions and Recommendations.....	1-6
2.0	INTRODUCTION	2-1
2.1	Terms of Reference and Purpose of the Report.....	2-1
2.2	Qualified Persons and Site Inspection	2-1
2.3	Sources of Information	2-1
2.4	Forward Looking Information	2-2
3.0	RELIANCE ON OTHER EXPERTS	3-1
4.0	PROPERTY DESCRIPTION AND LOCATION	4-1
4.1	Location.....	4-1
4.2	Mineral Tenure	4-1
4.3	Surface Rights.....	4-2
4.4	Tailings Rights.....	4-2
4.5	Royalties	4-4
4.6	Environmental Liabilities	4-4
5.0	ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE, AND PHYSIOGRAPHY .	5-1
5.1	Accessibility.....	5-1
5.2	Climate	5-1
5.3	Local Resources	5-1
5.4	Infrastructure	5-1
5.5	Physiography	5-2
6.0	HISTORY.....	6-1

6.1	Hollinger Mine	6-1
6.2	Post Hollinger Mine	6-1
6.3	Energy & Resources (CAM) Limited	6-2
6.4	508825 Ontario Limited.....	6-3
6.5	Labrador Mining and Exploration Company Ltd.	6-3
6.6	Kayorum Gold Mines Ltd.....	6-4
6.7	Herman Keller Estate	6-4
6.8	Ministry of Northern Development and Mines.....	6-4
6.9	Cogema Canada Ltd.	6-5
6.10	Erocon Waste Management Ltd.	6-5
7.0	GEOLOGICAL SETTING AND MINERALIZATION	7-1
7.1	Regional Geology.....	7-1
7.2	Local Geology	7-4
7.3	Deposit Geology.....	7-5
7.4	Mineralization	7-7
8.0	DEPOSIT TYPES	8-1
8.1	Genesis and Source of Material.....	8-1
8.2	Physical Characteristics	8-1
8.3	Exploration Potential	8-1
9.0	EXPLORATION.....	9-1
10.0	DRILLING.....	10-1
10.1	Drilling Summary.....	10-1
10.2	Core Logging.....	10-27
10.3	Geotechnical Drilling	10-33
10.4	Drill Site Closure	10-40
11.0	SAMPLE PREPARATION, ANALYSES, AND SECURITY	11-1
11.1	Core Handling, Sampling, and Security	11-1
11.2	Quality Assurance and Quality Control	11-1
11.3	QP Opinion.....	11-8
12.0	DATA VERIFICATION	12-1
12.1	Site Visit	12-1

12.2	QP Data Verification.....	12-3
12.3	Metallurgical Data Verification	12-7
12.4	Conclusions and Recommendations	12-7
13.0	MINERAL PROCESSING AND METALLURGICAL TESTING	13-1
13.1	Sample Composition	13-1
13.2	Head Sample Characterization and Mineralogical Analysis	13-3
13.3	Gravity Separation	13-4
13.4	Cyanide Leaching	13-5
13.5	Diagnostic Leach.....	13-7
13.6	Flotation	13-7
13.7	Cyanidation of Flotation Tailings.....	13-8
13.8	Deleterious Elements	13-8
14.0	MINERAL RESOURCE ESTIMATES	14-1
14.1	Introduction	14-1
14.2	Drill Hole Data	14-1
14.3	Domaining	14-3
14.4	Exploratory Data Analysis	14-9
14.5	Block Model and Resource Estimation	14-16
14.6	Mineral Resource Statement	14-28
15.0	MINERAL RESERVE ESTIMATES	15-1
16.0	MINING METHODS.....	16-1
17.0	RECOVERY METHODS	17-1
18.0	PROJECT INFRASTRUCTURE	18-1
19.0	MARKET STUDIES AND CONTRACTS	19-1
20.0	ENVIRONMENTAL STUDIES, PERMITTING, AND SOCIAL OR COMMUNITY IMPACT	20-1
21.0	CAPITAL AND OPERATING COSTS	21-1
22.0	ECONOMIC ANALYSIS.....	22-1
23.0	ADJACENT PROPERTIES.....	23-1
23.1	Hollinger Open Pit Mine	23-1
23.2	Dome Mine and Mill Complex	23-1
23.3	McIntyre Mine.....	23-1

23.4	Hoyle Pond Mine.....	23-2
23.5	Bell Creek Mine and Mill Complex	23-2
23.6	Timmins West Mine.....	23-2
23.7	Kidd Creek Met Site	23-2
24.0	OTHER RELEVANT DATA AND INFORMATION	24-1
25.0	INTERPRETATION AND CONCLUSIONS	25-1
25.1	QA/QC and Database	25-1
25.2	Mineral Resource Estimates	25-1
25.3	Metallurgical	25-1
25.4	Project Risk Summary.....	25-1
26.0	RECOMMENDATIONS	26-1
26.1	QA/QC and Database	26-1
26.2	Mineral Resource Estimates	26-1
26.3	Metallurgical	26-1
26.4	Project Recommendations	26-2
27.0	REFERENCES	27-1

TABLES

Table 1.1: Mineral Resource Estimate (Effective Date November 25, 2025)

Table 1.2: Project Recommendations

Table 4.1: Hollinger Tailings Patented Mining Claims List

Table 4.2: Hollinger Tailings Leased Mining Claims List

Table 4.3: Hollinger Tailings Unpatented Mining Claims List

Table 6.1: Summary of Historical Exploration Activities

Table 10.1: Summary of Drill Hole Details (assay results stated are for tailings material only)

Table 10.2: Logged Sediment Types

Table 10.3: Grain Size and the corresponding Sediment Types

Table 10.4: Geotechnical Data Collection Shelby Tube Sample Details

Table 11.1: 2025 Drill Program QA/QC Results

Table 12.1: Summary Comparison of QP Collar Measurements Compared to STLLR Survey Data

Table 12.2: Comparison of Independent Assay Results to the STLLR Database

Table 13.1: Composites Chemical Analysis

Table 13.2 Mineralogy of Composites by XRD

Table 13.3: Gravity Separation Tests Results

Table 13.4: Leach Tests Results for Composite 1

Table 13.5: Leach Tests Results for Composite 2

Table 13.6: Leach Tests Results for Composite 3

Table 13.7: Flotation Results (P80 of 38 μ m)

Table 14.1: Sample Statistics for the Dam Structure Components

Table 14.2: Comparison of Sample Statistics

Table 14.3: Block Model Volume Definition

Table 14.4: Search Volume Controls Used for Au Grade Estimation

Table 14.5: Statistical Comparison of Global Mean Au Grades

Table 14.6: Mineral Resource Estimate (Effective Date November 25, 2025)

Table 14.7: Indicated Mineral Resource Cut-off Sensitivity Table

Table 14.8: Inferred Mineral Resource Cut-off Table

Table 25.1: Project Risk Summary

Table 26.1: Project Recommendations

FIGURES

Figure 4.1: Location Map, Hollinger Tailings Project

Figure 4.2: Hollinger Tailings Land Tenure Map

Figure 7.1: Generalized Map of the Timmins-Porcupine Gold Camp

Figure 7.2: Stratigraphic Column of the Timmins-Porcupine Gold Camp

Figure 7.3: Local Geology Map

Figure 7.4: Generalized Deposit Sequence Downhole, Logged Material Observed within Each Unit is Described

Figure 10.1: Hollinger Drill Hole Location Map

Figure 10.2: Sonic Drill Core Displaying Metre Marks

Figure 10.3: Long-Section View Parallel to Phase 1 Wall

Figure 10.4: Cross-Section View

Figure 10.5: Hollinger Hole HTF25-193 being Surveyed by Surveyors On Site, Inc.

Figure 10.6: Geotechnical Drill Hole Location Hollinger Tailings Project

Figure 11.1: CRM Control Chart – OREAS 230, ALS Lab

Figure 11.2: CRM Control Chart – OREAS 233, ALS Lab

Figure 11.3: CRM Control Chart – OREAS 240, ALS Lab

Figure 11.4: CRM Control Chart – OREAS 231, ALS Lab

Figure 11.5: CRM Control Chart – OREAS 296, ALS Lab

Figure 11.6: Blank Material Control Chart, ALS Lab

Figure 11.7: CRM Control Chart– OREAS 230, BV Lab

Figure 11.8: CRM Control Chart– OREAS 233, BV Lab

Figure 11.9: CRM Control Chart– OREAS 240, BV Lab

Figure 11.10: Blank Material Control Chart, BV Lab

Figure 11.11: Cross-Plot of Pulp Duplicates against Orig. samples, ALS Labs

Figure 11.12: Cross-Plot of Third-Party Pulp Duplicates, ALS vs BV

Figure 12.1: Example Drill Hole Collar for Hole HTF25-224 on the Phase 1 Wall

Figure 12.2: Drill Hole Collar Survey and Field Sample Locations (Image courtesy of Google Earth June 19, 2024)

Figure 12.3: Hollinger Core Storage

Figure 12.4: Scatterplot Comparison of Verification Samples and STLLR Samples

Figure 12.5: Scatterplot Comparison of Photon Duplicate Samples and STLLR Original Samples

Figure 12.6: Summary QA/QC Plots

Figure 13.1: Sandy Silt Composite (Composite 1) – Samples Location

Figure 13.2: Sandy Silt Composite (Composite 1) – Samples Depth

- Figure 13.3: Silty Clay Composite (Composite 2) – Samples Location
- Figure 13.4: Silty Clay Composite (Composite 2) – Samples Depth
- Figure 13.5: Silty Sand Composite (Composite 3) – Samples Location
- Figure 13.6: Silty Sand Composite (Composite 3) – Samples Depth
- Figure 14.1: Plan View of the Drill Hole Collar Locations Relative to the Hollinger Tailings Facility
- Figure 14.2: Histogram of Au in the full assay database.
- Figure 14.3: Lithological/Material Model (isometric view facing Northeast)
- Figure 14.4: Plan Sketch of the Hollinger Tailings Facility from CMM Bulletin, Vol. 54 in June 1951.
- Figure 14.5: Georeferenced Images from 1951, 1969 and 2025
- Figure 14.6: Dam Exterior Walls (Phase 1 is red and Phase 2 is green).
- Figure 14.7: Pond contours.
- Figure 14.8: Histogram of Au in the Tailings
- Figure 14.9: Histograms of Au in the Organics (left) and Glacial Till (right)
- Figure 14.10: Histogram of Au in the Tailings Phase 1 Wall
- Figure 14.11: Histograms of Au in the Tailings Phase 1 Cell
- Figure 14.12: Histograms of Au in the Tailings Phase 2 Wall and Cell Combined
- Figure 14.13: Probability Plot of Au and Length/Au Scatter Plot (Tailings Material Only)
- Figure 14.14: Histogram of sample length (Tailings Material Only)
- Figure 14.15: Location of Dry Density Measurements
- Figure 14.16: Histogram of Dry Density Measurements
- Figure 14.17: North-South Sections
- Figure 14.18: North-South Sections
- Figure 14.19: North-South Sections
- Figure 14.20: North-South Sections
- Figure 14.21: North-South Swath Plot
- Figure 14.22: East-West Swath Plot
- Figure 14.23: Mineral Resource Classification (Top - Dam Walls, Bottom – Dam Cells)
- Figure 14.24: Mineral Resource Pit Shell
- Figure 14.25: Indicated Mineral Resource Cut-off Grade/Tonnage Plot
- Figure 14.26: Inferred Mineral Resource Cut-off Grade/Tonnage Plot

1.0 SUMMARY

1.1 Introduction

This Technical Report was prepared for STLLR by Brian Thomas and David Jin from WSP Canada Inc. (WSP) as a National Instrument (NI) 43-101 Technical Report, for the Hollinger Tailings Project (the Project) located in Timmins, Ontario. This Technical Report has been prepared in accordance with NI 43-101, Form 43-101F1, and Companion Policy 43-101CP.

The purpose of this Technical Report is to disclose results of exploration activities, metallurgical studies and the Maiden Mineral Resource Estimate (MRE) for the Project.

The report effective date of this Technical Report is January 9, 2026. The resource effective date is November 25, 2025.

1.2 Property Description and Ownership

The Project lies within the Deloro, Mountjoy, Ogden, and Tisdale townships in the Porcupine Mining Division, in the Province of Ontario. It is located in the city of Timmins, approximately 2.8 km south-southeast of the Timmins city hall (Figure 4.1). The location is centered about 573,445E and 5,372,432N in NAD 1983, Zone 17N Universal Transverse Mercator (UTM) coordinate system.

The Project is accessed by a 700 metre (m) gravel road traveling south from Moneta Avenue. The gravel road is the only vehicle access to the top of the facility and is gated to limit public access. The site is accessible year-round and recovery operations could occur throughout the year (STLLR, 2025).

STLLR holds a 100% interest in the patented mineral rights and has an option agreement to acquire all of the surface rights from Erocon Waste Management Ltd. (Erocon). Pursuant to the option agreement, Erocon will receive, upon the second anniversary of the exercise of the option, a 1.5% NSR on all gold (Au) recovered from the tailings.

STLLR maintains all mining taxes and rents on patents and leases to keep them in good standing, the annual totals are CA\$ (Canadian Dollars) 1,836.38 and CA\$242.81, respectively. The multi cell mineral claim is composed of two boundary cells and requires a total of CA\$800 of annual assessment credit to maintain the mineral claim in good standing.

Tailings rights in the Province of Ontario are linked to the mineral title ownership. STLLR maintains patented claims over the mineral titles, including all rights to deposit, mine, and recover materials from tailings connected to the subsurface rights.

1.3 Geology and Mineralization

The Project represents an anthropogenic (man-made) deposit of gold bearing material, which is derived from historical mining and milling operations at the prolific Hollinger Mine in the Porcupine Mining Camp of Timmins, Ontario. In contrast to natural ore bodies, the geometry, mineralogical composition, and distribution of gold within the tailings are not governed by geological processes. Instead, the spatial distribution of gold reflects historical deposition practices, metal-recovery efficiencies, variability in the original ore grade, milling procedures and construction design.

The Hollinger Mine is located within a northeast-southwest trending, ductile-brittle shear zone, the Hollinger Shear Zone. This shear zone is characterized by a strong east-northeast striking foliation that dips 80° south, and a prominent elongation-stretching lineation plunging 60° to the east (Burrows et al. 1993). The mineralization is hosted within a geologically complex zone of intensely folded and altered mafic and ultramafic volcanic rocks of the Tisdale assemblage, associated quartz-feldspar porphyry stocks, and

Timiskaming aged sediments. The vein systems are related to a major structural break, the Destor-Porcupine Fault Zone (DPFZ).

The main mineralized event at the Hollinger Mine consists of high-grade quartz-carbonate-gold shear hosted veins. These veins crosscut others containing dominant quartz with subordinate ankerite, albite, scheelite, tourmaline, sulphides (sphalerite, chalcopyrite, pyrite, galena), tellurides, and gold. Host-rock alteration consists of sericite, ankerite, rutile, chlorite and sulphides. Veining is concentrated around the north and west of the Pearl Lake porphyry and along an east-northeast trending belt of high strain (Bateman et al. 2005).

The mineralogy and geochemistry of the original Hollinger mineralization, has strongly influenced the tailings composition, including the presence of fine-grained sulphides, and gold. The tailings are typically grey, tan and brown, and mainly composed of silts and fine sands, with coarse sands and clay-rich intervals. This stratification reflects changes in historical discharge points, mill feed, plant performance, and local reworking due to dam raises, reclamation activities or erosion. The Hollinger Tailings Facility was developed in two phases, with the earlier phase interpreted to contain the higher gold grades. No correlation was identified between particle size and gold content. Moisture is variable, depending on the facility drainage, but oxidation is common in the upper horizons.

The present land surface is capped by landfill materials, vegetation, water, and waste that overlie the tailings deposit. A laterally extensive organic horizon underlies the tailings, followed by glacial till with occasional gravel horizons, and finally the bedrock surface. All units generally exhibit horizontal dips, although the tailings surface is observed to dip shallowly toward the southwest.

The Hollinger Tailings Facility was built over a gently sloping topography, grading down slope from northeast to lower southwest. The dam heights vary from 5 m to 30 m, with the wall being at its highest along the southwest. The height of the wall variation reflects historical deposition methods and topography. The Hollinger Tailings Deposit measures 1,950 m in length, 1,250 m in width, and reaches a maximum depth of 40 m, measured vertically from surface to the bottom of the tailings.

Tailings form the principal gold-mineralized unit and comprise all logged sediments overlying the organic horizon. The surface fill, organics, till, and bedrock domains are generally barren of gold, with rare anomalous values attributed either to localized contamination from the tailings or to mineralization occurring naturally outside of the tailings.

Gold mineralization was consistently observed throughout the deposit both laterally and vertically. The range in gold values reported was narrow; however, comparatively higher average grades were observed in Phase 1 and Phase 1 dam walls relative to Phase 2. This is attributed to Phase 1 containing early mine life tailings which had a lower recovery rate at the Hollinger Mill and possibly higher-grade mill feed.

1.4 Exploration and Drilling

STLLR did not conduct any exploration.

In February 2025, STLLR launched a comprehensive tailings characterization program for the Project. A total of 11,230 m of sonic drilling across 423 holes and spaced on a 50 m grid pattern was completed. A detailed list of drill holes is presented in Table 10.1. Drilling was performed by 403 Drilling Ltd., supervised by GeoMinEx Consultants and the STLLR team. The drilling was completed using a track mounted, LS 450 Boart Longyear drill rig with a 4.75-inch core barrel and 6-inch casing. STLLR retains temporary possession of the remaining half core at its Timmins core facility along Highway 655, about 7 km north-northeast of downtown Timmins. Records from the previous 1984 Energy & Resource (CAM) Limited drill program were insufficient to use.

Core was logged by a STLLR geologist and GeoMinex contract geologists, at the STLLR core shack in the city of Timmins. The logs were entered directly in MX Deposit database software. The core loggers were responsible to identify and record, if present; unit type, grain size, colour, moisture content, grading, description of textures, structures, mineralization, recovery and contact types.

The logging separated out 15 different Unit Types (Table 10.2), reflecting all materials present within and below the Tailings Facility. The primary units reflected grain size and texture variation within the sedimentary units of the tailings and glacial till. The most observed units were silty-sand, silty-clay, sandy-silt and sand, combined making up 73.2% of the logged material.

Mineralization was logged to respect the Unit Type boundaries. The most common sulphide present was pyrite and occurred as fine cubes up to 10% but on average less than 1%. No visible gold was observed. Gold mineralization from assay data showed most of the tailings was consistently mineralized both laterally and vertically throughout the facility.

Knight Piésold (KP) was retained by STLLR to support a geotechnical data collection program in tandem with the infill drilling program in late winter of 2025. The purpose of the geotechnical data collection program was to confirm tailings and foundation conditions and bedrock depth across the Tailings Facility, collect soil samples for laboratory testing to estimating moisture content, complete in situ testing of the tailings and foundation soils with a focus on estimating in situ density and assess the location of the phreatic surface (water table) within the tailings.

The site investigations for the geotechnical data collection program were carried out between March 24, and April 22, 2025. The Scope of Work (SOW) included geotechnical drilling, in situ testing, overburden and bedrock logging, sample collection, and laboratory testing of representative samples. The completed drill hole locations are shown on Table 10.1. The program included 18 drill holes and 2 monitoring well installations.

1.5 Sample Preparation, QA/QC and Security

The Hollinger Tailings core was collected by four-inch diameter continuous sonic coring. Samples were cut, with half sent to ALS Laboratories Inc. (ALS) for drying to a maximum temperature of 60-degree Celsius (°C) using ALS PREP-41 sample preparation method. The dried sample was then broken using a rubber mallet and sieved through an 180-micron screen (Tyler 80 mesh). The minus fraction that had passed through the screen was collected, homogenized, and split into a 250 g fraction. A 50-gram (g) charge was fire assayed and analyzed using an AAS finish for gold. STLLR inserted independent certified reference material and blanks with the samples, along with routine pulp repeat assays, as well as completing routine third-party check assays at Bureau Veritas Commodities Canada Ltd. ALS and BV are both ISO 17025 accredited laboratories and independent of STLLR.

The assay results were monitored and validated through QA/QC protocols where any CRM that fell above or below the mean certified 3x Standard Deviation (3xSD) was recorded as a failure, and a warning was warranted if it fell within 2x and 3x Standard Deviation. Moreover, if more than four consecutive assays of the same Certified Reference Material (CRM) fell above or below the mean but within 2xSD, it was also considered a failure. Any reported assay for a blank sample greater than five times the lower detection limit of the analytical method was considered a failure.

The assay certificates were received and imported to STLLR's secure database management web-platform, MX Deposit, and all assay results were validated through pre-assigned QA/QC procedures. All the assay related files are stored on the STLLR secure Egnyte webserver.

1.6 Mineral Processing and Metallurgical Testing

In 2025, a metallurgical testing program was carried out on three representative composite samples of the Hollinger tailings resource. The program included head sample characterization, mineralogical analysis as well as gold recovery testing via gravity separation, cyanide leaching and flotation.

The composites contained between 0.33 and 0.37 g/t Au and between 1.98 and 2.40% Sulphur (S) and consisted mainly of quartz, ankerite and muscovite.

The gravity recoverable gold in the three composites was very low. Gravity would not be an option for processing the Hollinger tailings with concentrate grades varying between 23.3 and 44.5 g/t Au and low gold recoveries ranging from 2.6 to 3.7%.

Initial bottle roll tests on the “as received” composite samples established baseline recoveries, which remained below 30% after 48 hours. Additional tests were conducted on the same composites at progressively finer grind sizes (P80 of 75 µm, 53 µm, 45 µm and 30 µm) improving gold extraction. Overall, the weighted average gold recovery across all three composites, representing the entire resource, was calculated at approximately 61.3%. A diagnostic leach test showed that the maximum gold recovery by cyanide leaching would be lower than 75% and only be achievable with ultrafine grinding.

Flotation did provide the best performance in terms of gold recovery, reaching 85.1% at the finest grind tested (approximately 33 µm). The weighted average recovery across all composites was 82.5% for gold and 96.1% for sulphur with an average rougher mass pull of approximately 11.7%. The gold grade in rougher concentrates ranged from 2.52 to 3.09 g/t Au.

1.7 Mineral Resource Estimates

The Qualified Person (QP) for this Mineral Resource Estimate (MRE) is Mr. Brian Thomas, P.Geo., an independent QP, as defined under NI 43-101 and an employee of WSP based in Sudbury, Ontario, Canada. The effective date of this Mineral Resource Estimate is November 25, 2025.

The Mineral Resource Estimate outlined in the following sections was derived from drill hole data and a lithological model (created in Leapfrog Geo software) provided by STLLR, using a Three-Dimensional (3D) block modelling approach in Datamine Studio RM (Datamine) software.

The MRE is based entirely upon data provided from a 2025 sonic drilling program, completed by STLLR. The drill hole database consisting of 423 drill holes, totalling approximately 11,230 m of core, was made available on March 20, 2025, and the close-out date of the database was on August 15, 2025.

Historical tailings dam construction drawings were used to define 4 mineral domains used for grade estimation including: Phase 1 wall and cells (original tailings dam), Phase 2 wall and cells (expansion). The MRE is stated for only tailings material and excludes any mineralization or tailings contamination seen in the underlying bedrock or organic layer.

The block model was constructed using 10 x 10 x 1 m blocks split down to 2.5 x 2.5 x 0.5 m along contacts. Gold assay intervals were bench composited to a length of 1 m, and outliers were capped using a top-cut value of 1.3 g/t.

Block grades were estimated using Inverse Distance Squared (ID²) interpolation requiring samples from a minimum of two holes per estimate. Hard boundaries were used between all mineral domains with the exception of between the Phase 2 wall and cells.

The block model was validated using a visual comparison of composites and block grades in section and plan, global comparison of mean grades and the inspection of swath plots.

Indicated and Inferred Mineral Resource categories were assigned based on drill hole spacing where Indicated required a minimum spacing of 50 m between holes and Inferred based on drill hole spacing greater than 50 m, including projections of 50 m beyond the Indicated boundary and pond areas surrounded by Indicated material that was not drilled.

Bulk dry density was assigned per domain based on limited sample data, ranging from 1.6 g/cm³ to 1.9 g/cm³ with a basic assumption of higher values in the walls and slightly increasing values with depth in the cells due to assumed compaction.

Table 1.1 summarizes the Indicated and Inferred Mineral Resources for the Project. Mineral Resources were evaluated for Reasonable Prospects for Eventual Economic Extraction (RPEEE) by reporting open pit resources within a constrained pit shell at a gold cut-off grade of 0.21 g/t. The continuity of below cut-off mineralization inside the pit shell was evaluated using a grade shell methodology and individual grade shells with a volume of greater than 2,500 m³ were assumed to be sortable during mining and excluded from the estimate. Volumes below this threshold were assumed to not be sortable and included as minor internal dilution.

Mineral Resource Estimates have been prepared in accordance with NI 43-101 following the requirements of Form 43-101F1. The MRE follows the Canadian Institute of Mining (CIM) Estimation of Mineral Resource and Mineral Reserves Best Practices Guidelines (November, 2019) and was classified following CIM Definition Standards for Mineral Resources & Mineral Reserves (May, 2014). Mineral Resources are not Mineral Reserves, and do not demonstrate economic viability. There is no certainty that all, or any part, of this Mineral Resource will be converted into Mineral Reserve. Inferred Mineral Resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorized as Mineral Reserves.

Table 1.1: Mineral Resource Estimate (Effective Date November 25, 2025)

Area	Indicated Resource			Inferred Resource		
	Tonnes (Mt)	Au Grade (g/t)	Contained Au (ozs)	Tonnes (Mt)	Au Grade (g/t)	Contained Au (ozs)
Phase 1	16.1	0.41	212,000	4.1	0.43	56,000
Phase 2	20.2	0.31	200,000	3.6	0.31	37,000
Total	36.2	0.35	412,000	7.7	0.37	93,000

Notes:

- (1) These mineral resources are not mineral reserves as they do not have demonstrated economic viability. The Hollinger MRE follows current CIM Definition Standards (2014) and CIM MRMR Best Practice Guidelines (2019). The resource estimate is presented as in-situ and undiluted and is considered to have reasonable prospects for eventual economic extraction.
- (2) The mineral resources are constrained by a resource pit shell based on a 0.21 g/t Au cut-off representing a truck and loader extraction scenario. The cut-off grade of 0.21 g/t Au was calculated using the following parameters: operating cost = CA\$17.00/t; payable gold = 99.95%; gold price = US\$3,000/oz; US\$/CA\$ exchange rate = 1.38; mill recovery of 61.3%.
- (3) The independent and qualified person for the Hollinger MRE, as defined by NI 43-101, is Brian Thomas, P. Geo. of WSP. The effective date of the MRE is November 25, 2025.
- (4) The estimation encompasses wireframes representing Phase 1 and Phase 2 walls and cells which contain the tailings material.
- (5) High-grade capping of assays was set at 1.3 g/t Au.
- (6) The estimate was completed with a sub-blocked model in Datamine Studio RM, with a parent block size of 10 m x 10 m x 1 m (X,Y,Z) and a minimum sub-block size of 2.5 m x 2.5 m x 0.5 m (X,Y,Z), using inverse distance squared (ID2) interpolation method based on 1 m composite samples.
- (7) Density values for tailings material were assigned between 1.6 g/cm³ and 1.9 g/cm³ according to depth and differences between material in walls and cells. Estimates are reported on a dry, in-situ basis.
- (8) Hollinger Mineral Resources were classified as Indicated and Inferred. Indicated mineral resources were defined for blocks where drill hole spacing is 50 m or less and Inferred mineral resources where drill hole spacing is greater than 50 m.
- (9) Potential mining continuity was evaluated inside the pit shell by generating grade shells. Grade shells below cut-off within the resource pit shell with volumes greater than 2,500 m³ were assumed to be sortable and were excluded from the MRE. Grade shells below cut-off with volumes less than 2,500 m³ were assumed to be too small for sorting and included in the MRE.
- (10) The resource tonnage was rounded to the nearest 100,000 tonnes and the metal contents are presented in troy ounces (tonnes x grade / 31.10348) rounded to the nearest thousand ounces. Any discrepancies in the totals are due to rounding effects.
- (11) The Hollinger MRE is based on a 61.3% gold recovery rate via cyanide leaching at a 30-micron grid size. The Company also tested flotation at a 38-micron grind size and achieved 82.5% gold recovery with a 11.7% mass pull and grading 2.69 g/t Au, 2.3 g/t Ag and 16.5% sulphur.
- (12) As of the effective date of the MRE, the QP is not aware of any known environmental, permitting, legal, title-related, taxation, socio-political, or marketing issues or any other relevant issue that could materially affect the Hollinger MRE.

Potential sources of uncertainty in the Mineral Resource Estimate include limited dry bulk density data coverage, sample preparation methodology and uncertainty related to the nature and location of the walls.

1.8 QP's Conclusions and Recommendations

1.8.1 QA/QC and Database

The mineral resource QP conducted a personal site inspection of the project site and the core facility. No material issues were identified with the drilling, logging, sampling, QA/QC or chain of custody procedures and these procedures were determined to be consistent with industry practices.

Based on the limited duplicate sample data available, the QP identified that the sample preparation procedure used may have introduced a small relative bias in the assay data and resulted in marginal precision for a portion of the sample data. The QP concludes that the assay data is suitable for the purpose of modelling and grade estimation which form the basis of this maiden MRE but acknowledges that further testing and analysis is warranted. It is uncertain if the issues identified would have any material impact to the MRE as there was no indication of any grade bias issues in the metallurgical testwork, based on the 3 composite samples (100 kg) described in Item 13.0.

The QP recommends that a representative 10% of remaining core be analyzed using a standard preparation procedure for rock such as ALS PREP-31 package consisting of crushing, pulverization and riffle splitting, or

optionally photon analysis, to ensure a representative and unbiased assay preparation and analysis methodology to further evaluate the sample database.

Refer to Items 12.4 and 14.6.1 for further analysis and discussion.

1.8.2 Mineral Resource Estimates

The MRE for the Project has been prepared in accordance with NI 43-101 and following the requirements of Form 43-101F1. The MRE follows the CIM Estimation of Mineral Resource and Mineral Reserves Best Practices Guidelines (November 2019) and was classified following CIM Definition Standards for Mineral Resources & Mineral Reserves (May 2014).

The QP has taken reasonable steps to make the MRE as representative as possible, however factors that could cause actual results to differ materially from the forward-looking information include any significant differences from one or more of the following material factors or assumptions that were applied in drawing the conclusions or making the estimates, forecasts or projections set forth in this Item, including: the suitability of the sample preparation method for assay, the assumptions used by the QP to prepare the data for resource estimation, the assumptions made in creating the dam walls structure, the interpretation of the mineral domain models, the selection of grade interpolation method, sample search and estimation parameters used for grade interpolation, continuity of mineralization and factors used to determine reasonable prospects for economic extraction.

The QP has the following recommendations:

- Collect more dry bulk density data on an approximate 200-250 m grid spacing.
- Conduct infill drilling to target the existing gaps in the higher-grade Phase 1 wall and infill the areas where current drilling intersects the wall at poor angles or locations and in the pond areas.
- Complete step-out drilling outside of the current resource at a grid spacing of 50 x 50 m or 100 x 100 m to increase the size of the Indicated and/or Inferred resource.
- Consider a ground penetrating radar survey to confirm the slopes and locations of the Phase 1 and 2 walls and determine if other potential internal cell walls are present.

1.8.3 Metallurgical

In the opinion of QP, the composite samples were appropriately prepared to represent the overall tailings resource in terms of spatial distribution, depth, and average gold grade per sediment type. Gravity separation testing resulted in low gold recoveries, indicating that gravity methods are unsuitable for processing the Hollinger Tailings.

Bottle roll assays indicated baseline recoveries of direct leaching without regrinding achieved 30% after 48 hours. Finer grinding improved gold extraction; recoveries for composites 1 and 2 were in the range of 60%, while Composite 3 achieved approximately 69% recovery at the finest tested P80 of around 30 µm. The diagnostic leach underscores the opportunity of integrating oxidation procedures to further enhance gold recovery from the Hollinger Tailings.

Flotation conducted at fine grind sizes yielded strong gold recoveries, reaching up to 85.1%. Concentrate grades had a weighted average of 2.69 g/t.

In future studies, it is recommended to expand testing across drill samples from multiple locations to capture variability in gold recovery, conduct direct cyanidation at finer grind sizes with repeatability studies for consistency, and incorporate oxidative pre-treatment methods to address refractory gold. Furthermore, broader flotation trials should be conducted if market conditions are favourable. Consideration should also be

given to developing a dedicated flowsheet tailored to local mill treatment options, as well as evaluating rare earth element recovery for its potential economic benefits.

1.8.4 Project Recommendations

Table 1.2 provides overall recommendations for the next phase of the Project.

Table 1.2: Project Recommendations

Type	Description	Amount (CA\$ thousands)
QA/QC Database	Conduct field duplicate analysis of 10% of tailings samples	54 ¹
MRE	Dry bulk density measurements on a 200-250 m grid spacing	350 ²
	Infill drilling, targeting existing gaps and pond areas	515
	Step-out drilling to increase resource	2,330 ³
	Ground penetrating radar survey	30 ⁴
Metallurgical	Expanded metallurgical test work	200 ⁵
	Albion tests	60 ⁵
Total		3,539

Notes:

1. 1,200 samples at \$45 per sample
2. 200 m spaced grid, 700 m of drilling at \$466 per metre rounded up
3. 5,000 m at \$466 per metre
4. Assumed only equipment rental
5. Cost estimate provided by WSP

2.0 INTRODUCTION

2.1 Terms of Reference and Purpose of the Report

This Technical Report was prepared for STLLR by WSP as an NI 43-101 Technical Report, for the Project located in Timmins, Ontario. This Technical Report has been prepared in accordance with NI 43-101, Form 43-101F1, and Companion Policy 43-101CP.

STLLR holds a 100% interest in the patented mineral rights and has an option agreement to acquire all of the surface rights from Erocon.

The purpose of this Technical Report is to disclose characterization activities, metallurgical studies and the Maiden MRE for the Project.

MRE was estimated following the CIM Estimation of Mineral Resource and Reserves Best Practices Guidelines (November 2019) and classified following the CIM Definition Standards for Mineral Resources and Reserves (May 2014).

The report effective date of this Technical Report is January 9, 2026. The resource effective date is November 25, 2025.

2.2 Qualified Persons and Site Inspection

The QP for the MRE and geology related Items of this Technical Report is Mr. Brian Thomas, P.Geo., an independent QP, as defined under NI 43-101 and employee of WSP. The QP for metallurgy is Mr. David Jin, P.Eng., an independent QP, as defined under NI 43-101 and an employee of WSP. Please refer to the Date and Signature page (page ii) of this Technical Report for further details.

A QP personal site inspection of the Project was last conducted by Mr. Brian Thomas on August 27, 2025, to observe site conditions, review geological data collection and QA/QC procedures, spot check verification of drill collar locations, and complete verification logging and sampling of sonic drill core. See Item 12.0 of this Technical Report for more details of the site inspection and data verification completed.

2.3 Sources of Information

The MRE and Technical Report are based on information provided by STLLR, including:

- Drill hole database consisting of:
 - Au assays
 - Lithology and mineralogy descriptions
 - Collar coordinates
 - Bulk density measurements
- Assay certificates provided directly from third party laboratories
- Metallurgical testwork data and reports directly from third party laboratories
- Current and historical reports
- Geological data collection procedures

Further sources of information, utilized by the authors, and references are listed in Item 27.0.

2.4 Forward Looking Information

This Technical Report contains “forward-looking information” within the meaning of applicable Canadian securities legislation. Forward-looking information includes, but is not limited to the MRE and assumptions on which it is based, planned exploration and metallurgical programs; proposed drilling, sampling and testwork; potential upgrades or conversions of mineral resources; assumptions regarding cut-off grades, metallurgical recoveries, metal prices, operating and capital costs, and other parameters used to demonstrate reasonable prospects for eventual economic extraction; the scope, timing and outcomes of future studies; permitting and other regulatory approvals; environmental and social/community considerations; infrastructure and market conditions; and the availability and cost of financing. Generally, forward-looking information can be identified by the use of forward-looking terminology such as “accelerate”, “add” or “additional”, “advancing”, “anticipates” or “does not anticipate”, “appears”, “believes”, “can be”, “conceptual”, “confidence”, “continue”, “convert” or “conversion”, “deliver”, “demonstrating”, “estimates”, “encouraging”, “expand” or “expanding” or “expansion”, “expect” or “expectations”, “fast-track”, “forecasts”, “forward”, “goal”, “improves”, “increase”, “intends”, “justification”, “leading”, “plans”, “potential” or “potentially”, “pro-forma”, “promise”, “prospective”, “prioritize”, “reflects”, “re-rating”, “robust”, “scheduled”, “stronger”, “suggesting” or “suggests”, “support”, “updating”, “upside”, “will be” or “will consider”, “work towards”, or variations of such words and phrases or state that certain actions, events or results “may”, “could”, “would”, “might”, or “will be taken”, “occur”, or “be achieved”.

Forward-looking information is based on the opinions and estimates of the QPs at the date the information is made, and is based on a number of assumptions and is subject to known and unknown risks, uncertainties and other factors that may cause the actual results, level of activity, performance or achievements of STLLR to be materially different from those expressed or implied by such forward-looking information, including risks associated with required regulatory approvals, the exploration, development and mining such as economic factors as they effect exploration, future commodity prices, changes in foreign exchange and interest rates, global inflationary pressures, actual results of current exploration activities, government regulation, political or economic developments, the ongoing wars and their effect on supply chains, tariffs, environmental risks, pandemic risks, permitting timelines, capex, operating or technical difficulties in connection with development activities, employee relations, the speculative nature of gold exploration and development, including the risks of diminishing quantities of grades of resources, contests over title to properties, and changes in project parameters as plans continue to be refined as well as those risk factors discussed in STLLR’s Annual Information Form for the year ended December 31, 2024, available on www.sedarplus.ca. Although the QPs have attempted to identify important factors that could cause actual results to differ materially from those contained in forward-looking information, there may be other factors that cause results not to be as anticipated, estimated or intended. There can be no assurance that such information will prove to be accurate, as actual results and future events could differ materially from those anticipated in such information. Accordingly, readers should not place undue reliance on forward-looking information. The QPs do not undertake to update any forward-looking information, except in accordance with applicable securities laws.

3.0 RELIANCE ON OTHER EXPERTS

In Items 4.1, Mineral Tenure, 4.3, Surface Rights, 4.5, Royalties 4.6, Environmental Liabilities of this Technical Report, the QPs have relied upon, and believe there is a reasonable basis for this reliance on, information provided by STLLR regarding mineral tenure, surface rights, ownership details, agreements, taxation, royalties, environmental obligations, permitting requirements, applicable legislation relevant to the Project, environmental studies, and social or community impact. Though the QPs have used their experience and judgement to determine if the information in these Items was suitable for inclusion in the Technical Report, the QPs have not independently verified the information in these Items and have fully relied upon information provided by STLLR in these Items. The sources of information being relied upon includes STLLR Gold, 2025; Ontario Inc. and Erocon Waste Management Ltd., 2025; Labrador Mining and Exploration Company Limited and Moneta Porcupine Mines Inc., 2025; Labrador Mining and Exploration Company Limited and Moneta Porcupine Mines Inc., 1989; Kayorum Gold Mines Limited and Moneta Porcupine Mines Inc., 1989; Davis, James B., et. al, 1996; O. Reg 169/92, 1992.

4.0 PROPERTY DESCRIPTION AND LOCATION

4.1 Location

The Project lies within the Deloro, Mountjoy, Ogden and Tisdale townships in the Porcupine Mining Division, in the province of Ontario. It is located within the city of Timmins, 2.8 km south of the city hall, along the south-southeast extent (Figure 4.1). The location is centered about 573,445E and 5,372,432N in NAD 1983, Zone 17 UTM coordinates system. The Hollinger Tailings Facility covers an approximate total area of 191 hectares (Ha) and has a perimeter of 5,867 m.

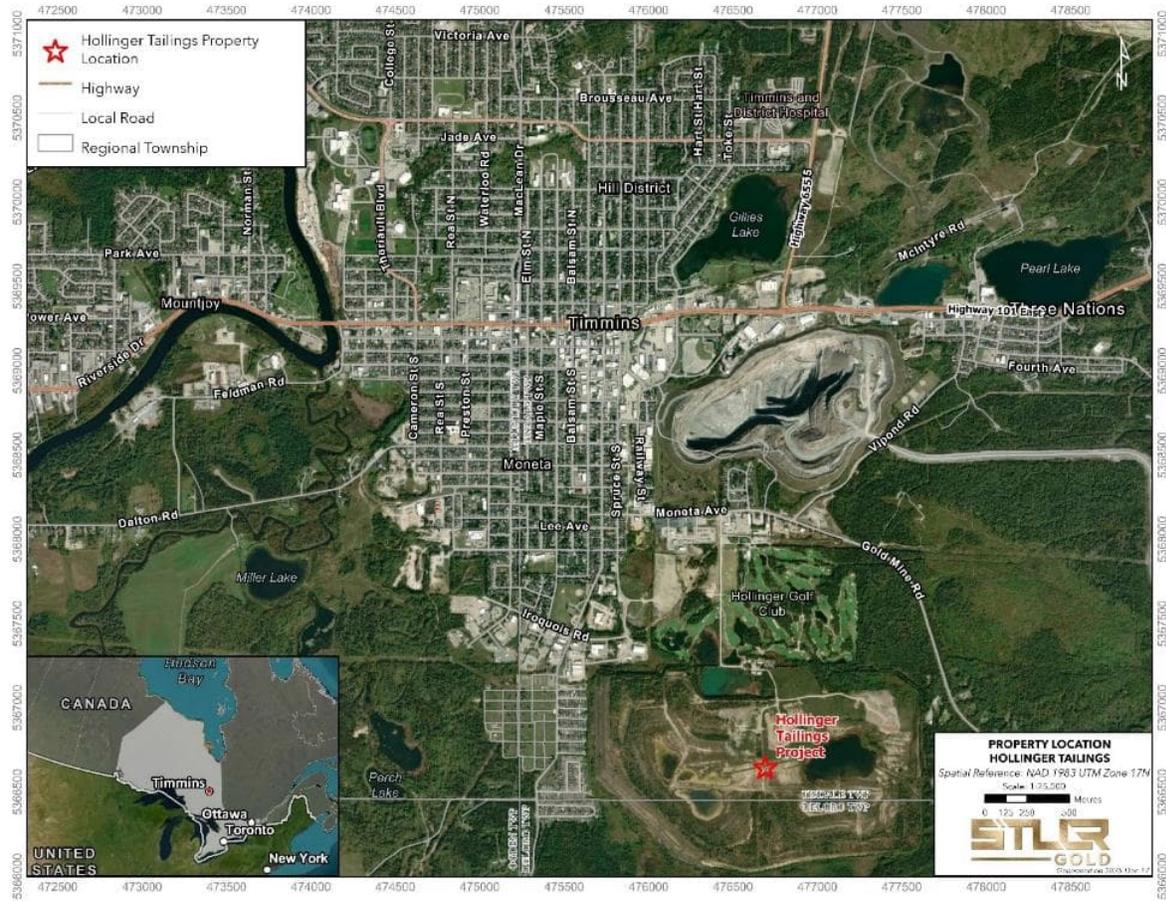


Figure 4.1: Location Map, Hollinger Tailings Project

4.2 Mineral Tenure

The Project is comprised of 22 contiguous patents, 2 leases and 1 unpatented multi cell mining claim, with a total area of 496.68 ha as outlined in Figure 4.2. A detailed list of the Project’s land tenure is found in Table 4.1, Table 4.2 and Table 4.3. All mineral patents, mineral leases and unpatented mineral claims are registered to STLLR with the exception of Lease LEA-108566. Lease LEA-108566 is registered to a numbered company, 508825 Ontario Limited (508825), which is a subsidiary of STLLR. Lease expiry dates are listed in Table 4.2. As of the date of writing, Lease LEA-107738 is in renewal process, as the 21-year lease expired on November 30, 2025. STLLR maintains all mining taxes and rents on patents and leases to keep them in good standing, the annual totals are \$1,836.38 and \$242.81 respectively. The multi cell mineral claim is composed of two boundary cells and requires a total of \$800 of annual assessment credit to maintain the mineral claim in good standing.

4.3 Surface Rights

On January 30, 2025, an option agreement was entered between 1001108570 Ontario Inc., a subsidiary of STLLR, and Erocon. The agreement provides STLLR immediate surface access rights to enter the property in exchange for \$100,000. The agreement also provided STLLR the rights to acquire the surface right ownership outright from Erocon by providing an additional \$900,000 and a 1.5% Net Smelter Royalty (NSR). The option agreement expires on January 30, 2032. The option agreement is associated with select patents which are listed in Table 4.1.

The unpatented multi cell mineral claim, 913103 was registered to STLLR on November 26, 2024, and intersects two surface rights listed to Erocon and The Hydro-Electric Power Commission of Ontario (HEPCO, now identified as Hydro One Networks Inc.).

4.4 Tailings Rights

Tailings rights in the Province of Ontario are linked as of right to the mineral title ownership. As noted in Table 4.1, STLLR maintains patented claims over the mineral titles, including all rights to deposit, mine, and recover materials from tailings connected to the subsurface rights.

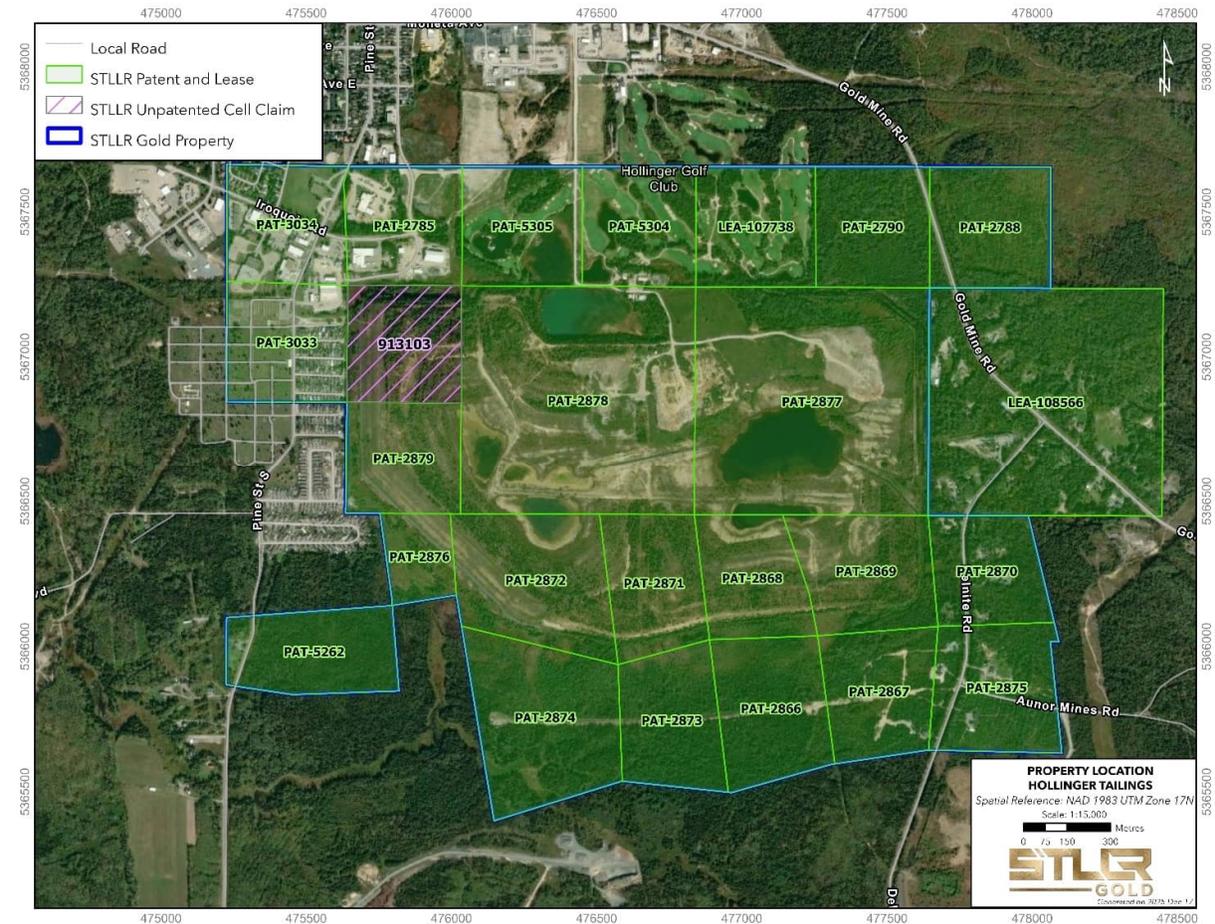


Figure 4.2: Hollinger Tailings Land Tenure Map

Table 4.1: Hollinger Tailings Patented Mining Claims List

Project	Tenure Number	Type	Parcel	Township	Surface Rights	Mining Rights	Area (Ha)
Hollinger Tailings	PAT-2785	Patent	13439W&T	TISDALE	No	Yes	16.187
Hollinger Tailings	PAT-2788	Patent	3588W&T	TISDALE	Yes	Yes	16.187
Hollinger Tailings	PAT-2790	Patent	3589W&T	TISDALE	Yes	Yes	16.187
Hollinger Tailings	PAT-2866	Patent	5833SEC	DELORO	No	Yes	17.401
Hollinger Tailings	PAT-2867	Patent	5833SEC	DELORO	No	Yes	12.646
Hollinger Tailings	PAT-2868	Patent	23081SEC	DELORO,TISDALE	Yes*	Yes	14.650
Hollinger Tailings	PAT-2869	Patent	23080SEC	DELORO,TISDALE	Yes*	Yes	21.813
Hollinger Tailings	PAT-2870	Patent	23080SEC	DELORO	No	Yes	13.962
Hollinger Tailings	PAT-2871	Patent	23081SEC	DELORO,TISDALE	Yes*	Yes	15.054
Hollinger Tailings	PAT-2872	Patent	23081SEC	DELORO,TISDALE	Yes*	Yes	23.310
Hollinger Tailings	PAT-2873	Patent	5833SEC	DELORO	No	Yes	15.580
Hollinger Tailings	PAT-2874	Patent	5833SEC	DELORO	No	Yes	24.281
Hollinger Tailings	PAT-2875	Patent	5833SEC	DELORO	No	Yes	18.373
Hollinger Tailings	PAT-2876	Patent	23080SEC	DELORO	Yes*	Yes	6.637
Hollinger Tailings	PAT-2877	Patent	13440W&T	DELORO,TISDALE	Yes*	Yes	64.750
Hollinger Tailings	PAT-2878	Patent	13440W&T	DELORO,TISDALE	Yes*	Yes	64.750
Hollinger Tailings	PAT-2879	Patent	13439W&T	DELORO,TISDALE	Yes*	Yes	16.187
Hollinger Tailings	PAT-3033	Patent	3193W&T	MOUNTJOY,TISDALE	Yes	Yes	16.187
Hollinger Tailings	PAT-3034	Patent	3193W&T	MOUNTJOY,TISDALE	Yes	Yes	16.187
Hollinger Tailings	PAT-5262	Patent	1266SEC	DELORO,OGDEN	Yes	Yes	16.390
Hollinger Tailings	PAT-5304	Patent	13438W&T	TISDALE	No	Yes	16.187
Hollinger Tailings	PAT-5305	Patent	13437W&T	TISDALE	No	Yes	16.187

Note: * Indicates patents associated with surface rights agreement between STLLR and Erocon.

Table 4.2: Hollinger Tailings Leased Mining Claims List

Project	Tenure Number	Type	Parcel	Township	Due Date	Surface Rights	Mining Rights	Area (Ha)
Hollinger Tailings	LEA-107738	Lease	1346LC	TISDALE	11/30/2025	No	Yes	16.19
Hollinger Tailings	LEA-108566	Lease	1580LC	DELORO, TISDALE	6/30/2031	No	Yes	64.75

Table 4.3: Hollinger Tailings Unpatented Mining Claims List

Project	Tenure Number	Cell ID(s)	Tenure Type	Township	Due Date	Area (Ha)
Hollinger Tailings	913103	42A06K208, 42A06K209	Multi-Cell Mining Claim	TISDALE	2026-11-26	21.40205

4.5 Royalties

The STLLR – Erocon option agreement provides that if STLLR exercises its option granted pursuant to the option agreement, Erocon will receive, upon the second anniversary of the exercise of the option, a 1.5% NSR on all gold recovered from the tailings.

As part of the May 1987 and February 1989 agreements between Labrador Mining & Exploration and STLLR (then-named “Moneta Porcupine Mines Inc.”) a 2% NSR was agreed upon for all sales of ores, minerals or other materials from one or more of the patent mining properties, leasehold properties and unpatented mining claims related to the subsurface mining rights. The NSR was exclusive of the mine tailings on the property.

As part of the 1989 agreement between Kayorum Gold Mines Ltd. (Kayorum) and STLLR, a 2% NSR was agreed upon for all sales of ores, mineral or other materials derived from one or more of the patent mineral properties related to the subsurface mining rights. The NSR was exclusive of the mine tailings on the property.

James B. Davis, William J. Millions and Gerald McNulty, the former sole and legal beneficiary owners of numbered company 508825 Ontario Limited hold a 2.1% NSR with a \$1,000 per year minimum payment, on the South Half of Lot 9, Concession 1, Parcel 1580, currently LEA-108566.

4.6 Environmental Liabilities

4.6.1 Erocon Landfill

A portion of the Hollinger Tailings Facility has been used by Erocon as a landfill for primarily wood waste, with additional permissions for a small percentage of industrial waste, since 1996. Erocon is the owner and operator of the landfill. The landfill is located in the northeast and north central portions of the Tailings Facility and covers approximately 6 Ha. The Hollinger Tailings Facility has been subject to groundwater and surface water monitoring associated with the permitted landfill.

An amended Environmental Compliance Approval (ECA; Number A770068) was issued on December 7, 2022, for the Waste Disposal Site (Landfill) to authorize disposal of wood waste, demolition and construction waste not to exceed 10% of the total volume, and wood waste ash including fly ash and bottom ash. The ECA details requirements for Financial Assurance (FA) and the filing of a Closure Plan.

As per the ECA, FA was to be submitted on January 1, 2023, and is required to reach a total cumulative amount of \$429,309 as at January 1, 2026. A re-evaluation of FA must be submitted by December 1, 2027, and every five years thereafter.

The prescribed closure date within the ECA is December 31, 2026. If the site is intended to be operated beyond the prescribed date, an ECA application with updated FA must be submitted at least six months in advance. If the site is intended to be closed, a closure plan must be submitted at least one year prior to the anticipated closure date (Ministry of Environment, Conservation and Parks, 2022).

4.6.2 Recovery of Minerals Permit

There is no registered closure plan for the Hollinger Tailings Facility.

In 2021, the province passed legislation enabling the recovery of minerals from historical sites, including sites without closure plans. The subsequent regulation came into force in 2025, paving the way for proponents to apply for a Recovery of Minerals Permit under this streamlined framework. A Recovery of Minerals Permit is required to recover the minerals from the tailings and remediate the land which will include both patented and unpatented mineral claims.

To the extent known, the QP's are not aware of any significant factors or risks that may affect access, title, or the ability to perform work on the property.

5.0 ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE, AND PHYSIOGRAPHY

5.1 Accessibility

The city of Timmins is accessible both by air and paved highway. Scheduled commercial flights to Timmins Victor M. Power Airport are available daily and serviced by multiple carriers. The airport is approximately 13 km from the Timmins City centre along Airport Road – ON-629. The city of Timmins can also be accessed by Highway 101 from both the east and west.

The Project is accessed by a 700 m gravel road traveling south from Moneta Avenue. The gravel road provides the only vehicle access to the top of the facility and is gated to limit public access. The site is accessible year-round and recovery operations could occur throughout the year (STLLR, 2025)

5.2 Climate

The Project area has four seasons with the winter average temperature ranging between -7.5 °C and -16.4 °C and long term extreme daily minimum of -37.7 °C. The summer average temperature ranging between 8.1 °C and 24.4 °C and can go as high as 38.9 °C long-term temperature extreme in July.

The property area experiences an average annual precipitation of about 543.1 mm and 307.6 mm of snow accumulation occurring on average between November through to March (Government of Canada, 2025).

Operations can occur at site year-round, however winter conditions provide additional ground stability and allow easier means of access by a wider variety of equipment.

5.3 Local Resources

The region has prolific gold and base metal mines as well as necessary mine and mineral exploration infrastructure and skilled labour. The mining industry relies heavily on Timmins (2021 population: 41,145) and Kirkland Lake (2021 population: 7,750) for its supply and service needs.

5.4 Infrastructure

The Hollinger Tailings Facility is located within the city limits of Timmins. A Hydro One substation is located along Moneta Avenue, approximately one km from the project site, and grid power is supplied to Erocon office and warehouse facilities at the entrance to the Tailings Facility.

Town water is serviced along Moneta Avenue to the north of the project area and to the neighbouring community to the west along Pine St. South. Surface water sources are locally available.

The entire area is serviced by telecommunication and includes cell phone reception.

Transportation infrastructure is well developed with paved municipal roads which can directly access highway 101. Rail networks are also available near Timmins.

Municipal services are available including the Timmins and District Hospital, emergency services for police, fire and ambulance, waste facilities as well as the Timmins Victor M. Power Airport.

The Timmins area is a well-established mining camp with existing milling capacity within the region which includes the following operations. The Dome Mill Complex lies 10.8 km east of the Project with a process plant that has a permitted capacity of up to 15,000 tonnes per day (tpd) and is operated by Discovery Silver with a current operating capacity of approximately 12,000 tpd (Discovery Silver, 2025).

The Bell Creek Complex including the processing facility lies 19 km northeast of the Project. Current mill average throughput put is reported at 4,400 tpd and operated by Pan American Silver (Pan American Silver, 2025).

The Redstone Mill is fully permitted for custom milling and is located 25 km southeast of the Project. The mill is operated by Northern Sun Mining.

Kidd Creek, mill and metallurgical sites 27 km east of the City of Timmins is owned and operated by Glencore. The Kidd Creek Metallurgy site has a concentrator, copper smelter, copper refinery, a zinc refiner, a cadmium plant, indium plant, and acid plant.

5.5 Physiography

The Hollinger Tailings Facility is located on what was once a swamp and marshy area. The Hollinger Mine began depositing tailings at this site in the 1920s and continued until the mine closed in 1968. To manage the tailings, dams and spill containment areas were built using older, coarse tailings material. Over the years raises were added to the tailings containment area gradually increasing its height to the current elevation. The topography has a relief difference of about 11 m with elevations ranging from 316.7 m to 327.7 m above mean sea level. The surface of the tailings pile is slightly concave and contains five ponds. The vegetation consists of grasses and local mixed forest dominated by jack pine, birch and poplar.

6.0 HISTORY

6.1 Hollinger Mine

The Hollinger Mine operated from 1910 to 1968 and over the life of mine, processed through the Hollinger Mill a total of 65,890,358 tonnes, producing 19,354,483 ounces (oz) of gold and 4,244,496 oz of silver. In addition, from 1940 to 1953 a total of 428,357 pounds of tungsten trioxide was produced. The mill produced approximately 58,967,000 tonnes of tailings which was placed in the Hollinger Tailings Facility.

6.2 Post Hollinger Mine

The Hollinger Mine closed in 1968, and the surrounding lands associated with the Hollinger Tailings Facility were acquired by various prospectors and companies. No historical mining has occurred on the Hollinger Tailings property however a limited amount of exploration was completed. Table 6.1 presents the full list of historical exploration activities completed on the property.

Table 6.1: Summary of Historical Exploration Activities

Year	Company	Exploration	Township
1973	A. Lepic	Electromagnetic, Magnetic / Magnetometer Survey	Tisdale
1980	Amax Minerals Exploration Ltd.	Airborne Magnetometer	Cody
1983	H. Keller	Diamond Drilling	Tisdale
1983	508825 Ontario Limited.	Assaying and Analyses	Tisdale
1984	Energy & Resources (CAM) Ltd., Lorncor Inc.	Assaying and Analyses, Boring Other Than Core Drilling, Metallurgical Testing and Bulk Sampling	Tisdale
1985	508825 Ontario Limited.	Geochemical, Other	Tisdale
1987	508825 Ontario Limited.	Diamond Drilling	Tisdale
1991	Cogema Canada Ltd.	Electromagnetic, Electromagnetic Very Low Frequency, Magnetic / Magnetometer Survey	Tisdale
1992	Cogema Canada Ltd.	Assaying and Analyses, Compilation and Interpretation - Diamond Drilling, Diamond Drilling, Geochemical, Geological Survey / Mapping, Gravity, Induced Polarization, Manual Labour	Tisdale
1993	Cogema Canada Ltd.	Compilation and Interpretation - Geology, Compilation and Interpretation - Ground Geophysics, Diamond Drilling, Electromagnetic, Electromagnetic Very Low Frequency, Geochemical, Geological Survey / Mapping, Gravity, Induced Polarization, Magnetic / Magn*	Tisdale

The earliest listed exploration activity was from 1973 when an electromagnetic (EM) survey was made for Albert Lepic on July 13, 1973 (McPhar SS15 Vertical Loop with operating frequency of 1000cps). EM Profiles along all traverse lines were nil and no conductors were located. The survey was completed on Legacy claim P354953 corresponding to current tenure number LEA-107738.

In 1980, Aeromag for Amax was flown at a line spacing of 200 m successfully outlining numerous magnetically anomalous geologic units and at least two major structural features.

6.3 Energy & Resources (CAM) Limited

Energy & Resources (CAM) Limited acquired the option to reclaim the minerals from the Hollinger Tailings Facility from three individual groups. The option agreements date 1983 between Energy & Resources Limited and Labrador Mining and Exploration, Kayorum and Ero-Con Limited & Herman Keller and covered either whole or in part the surface and mining rights or surface rights only. The agreement provided Energy & Resources (CAM) Limited to enter the property and assess the mineral potential for the tailings and to recover the minerals at a rate of treatment not to exceed 300,000 tons per month in exchange for a 2% net smelter royalty and allow Labrador Mining and Exploration the right to earn 50% of the interest in the tailings. Kidd Creek Mines Ltd. had a right of first refusal as the holder of the surface rights at the time. The purchase option was exercisable prior to February 15, 1995, and was not executed.

Energy & Resources (CAM) Limited evaluated the tailings in two stages. The first stage began in November of 1984 and included a drilling and sampling program on a 200-by-400 m grid for a total of 63 holes. Drilling was completed using a portable Winko Vibra-core drill. The drill was light weight, high frequency vibrating head and piped AQ sized sample in 5-foot lengths. The depths of holes ranged from 5 to 109 feet. The tailings recovered were composed of dry very fine grained to fine grained sand and silty to clayey sand. The mineralogy of the tailings was reported to be quartz grains; however, pyrite was visible in varying amount from less than 1% to 10%.

Peter Vevan P. Eng and C. von Hessert calculated and reported a historical non-NI 43-101 compliant resource of 57.614 million tons containing 590,604 oz of gold, grading 0.0103 oz/short ton (0.35 g/t).

The historical resource estimate was calculated using a database that included 63 drill holes designed on a grid pattern with a spacing that varied from 50-to-200 m. Gold grades were provided in oz per short ton and the depths of holes were in feet. Neither the reverse circulation material nor the assay certifications were preserved for validation. The polygonal estimation method was used by determining the area of influence around each hole using the midpoints between holes and building either rectangles, trapezoids or quadrilaterals and the sides were measured with appropriate scale. Eleven areas were measured by planimeter because one of the sides was curved. The wooded area and adjacent undrilled areas were not included in the total. The metric areas were converted to square feet then multiplied by the respective depth of each hole in its centre. The volumes were divided by a tonnage factor of 18.85 cubic feet per short ton (ft³/ton) to arrive at the tonnage of each block. The tonnage times the grade gave the contained oz in each block. The tonnages and contained oz for all blocks were totaled and an average grade calculated.

A resource category was not assigned to the historical resource estimate but in present day terms it would have been classified as an Inferred resource. Polygonal resource estimation is no longer considered as an industry accepted best practice. The QPs have not completed sufficient work to consider this historical MRE as current; and therefore, STLLR is not treating this historical estimate as a current Mineral Resource and it should no longer be relied upon. Refer to Item 14.0 of this Technical Report for the current MRE.

The second stage collected 30 tons of tailings to be used for a metallurgical study. The samples were taken after all assays from the first pass drill test were received. The sampling was completed from May 26 to June 7, 1985. The samples were collected using a large sonic drill using a 6-inch diameter bit and core barrel attached to a 4-inch diameter drill rod. A total of 43 drill holes were completed and sample for a total of 3,025 feet.

Energy & Resources (CAM) Limited. completed a metallurgical investigation on the recovery of gold in September of 1985 at Lakefield Research, a division of Falconbridge Ltd. The investigation examined gold recovery by gravity and flotation and final cyanidation on a combined concentrate. The results indicated that gravity concentration was effective in recovering non-sulphide gold, which could be solely retrieved through

flotation processes. Historical testwork showed that applying gravity concentration followed by flotation resulted in 75% to 83% of the gold being recovered into the concentrate, with a mass pull of 22% of the original sample weight. Cyanidation of the gravity and flotation concentrates yielded an overall gold extraction rate of 52% to 59%. It was concluded that regrinding the concentrate prior to cyanidation enhanced gold recovery.

Based on the positive results from the initial metallurgical investigation a pilot plan study was completed in October of 1985. The recommended flowsheet resulting from the study suggested a spiral rougher, spiral cleaner and table recleaner stop followed by flotation of the combined gravity tailings, to create an optimum concentrate for cyanidation.

6.4 508825 Ontario Limited

1985 – Assay work was done for 508825 (prior to STLLR’s acquisition of the company in 1996) on legacy claims P577599 and P577601 both situated in current lease tenure number LEA-108566 returning assay values ranging from 2-92 ppb Au, 0.2-35.0 ppm As and 1-14ppm W.

1987 – Three AQ holes were drilled for 508825 in June 1987 on legacy claim P577600 (current lease LEA-108566), with a total of 368.2 feet (112.22 m) depth.

On November 1, 1996, James B. Davis, William J. Millions, and GERAL McNulty, the former sole legal beneficial owners of numbered company 508825, sold all the issued and outstanding common shares of 508825 to STLLR. 508825 held an interest in the South Half of Lot 9, Concession 1, Parcel 1580. The shares were sold for consideration of \$30,000 and 30,000 common shares of STLLR as well as a 2.1% NSR. with a \$1,000 per year minimum payment.

6.5 Labrador Mining and Exploration Company Ltd.

The mineral title to the patented mining properties was reserved for Kayorum and Labrador Mining and Exploration Company Ltd., ownership after the expiration of the option agreement with Energy and Resource (CAM) Ltd. Note that Labrador Mining and Exploration’s interest in the mining properties is outside of the area of the MRE.

On May 1987, Labrador Mining and Exploration entered into an agreement with STLLR for the sale and transfer of the patented surface and/or mining rights, of the remainder of Parcels 7633, 3590, 3588, 3589, 7632, 1730, 1866, 1744, 1743, 3081, 2729, 1029, 1031, 1589, 1890, 1891, 1888, 5143, 1691, 1889, 2731, 2725, 1741, 1742, 2726, 2727, 2728, 3078, 3079, 2730, 3080, 1508, 272, 6408, 1785, 1663, 10632, 3479, leasehold properties 101559, 103294, 102836, 103353, unpatented mineral claims, P-529973, P-529974, P-594781, P-594782, P-594783, P-594784, P-594785, P-594789, P-594790, P-594791, P-594792, P-594793 and P-595970. The patented mining properties and leasehold properties and unpatented mining claims were transferred in consideration of \$3,000 and a 2% NSR on all sales of ores, minerals or other materials from one or more of the patent mining properties, leasehold properties and unpatented mining claims.

Also on February 21, 1989, Labrador Mining and Exploration Company Ltd. entered into an agreement with STLLR for the sale and transfer of the patented mining properties and mining leases in consideration for 50,000 common shares of STLLR and a 2% NSR payable to Labrador Mining and Exploration Company Ltd from the sales of ores, minerals or other materials derived from one or more of the mining patents or mining leases, respectively.

6.6 Kayorum Gold Mines Ltd.

The mineral title to certain patented mining properties was reserved for Kayorum ownership after the expiration of the option agreement with Energy and Resource (CAM) Ltd.

On February 21, 1989, Kayorum entered into an agreement with STLLR for the sale and transfer of patented mining rights of Parcels 4679 W&T, 4678 W&T, 5830 SEC, 5832 SEC and 5833 SEC for consideration of 200,000 common shares of STLLR and a 2% NSR on sales of ores, mineral or other materials derived from on or more of the patent mineral properties.

Kayorum was succeeded by TMI-Learnix Inc. (TMI-Learnix), a federal corporation that was dissolved on or about November 2, 2005, for non-compliance in accordance with s. 212 of the *Canada Business Corporations Act*. TMI-Learnix has not carried on business since dissolution, and the effect of dissolution confirms that TMI-Learnix has no legal status as an entity

6.7 Herman Keller Estate

Herman Keller and subsequently the Herman Keller Estate is registered on instrument number C313145 stating the release of equity from Ero-Con Ltd. to Herman Keller all tailings' deposits on the lands associated with PIN 65411-0217 (LT) now mineral claim 913103. The lands forfeited on January 1, 1977.

In 1983 Herman Keller performed the diamond drilling of 3 holes on Legacy claim P577601 corresponding to current lease with tenure number LEA-108566 returning 0.002-0.005 oz/ton (0.057 – 0.142 g/t) Au and 0.66 oz/ton (18.711 g/t) Ag.

6.8 Ministry of Northern Development and Mines

The Ministry of Northern Development and Mines (present day Ministry of Energy and Mines) declared the site abandoned, prior to conducting remediation work which commenced in November 1992. In June of 1991, Golder Associates completed a site assessment and identified the condition of the west and southwest dam walls of the Hollinger Tailings Facility to be of high priority. As a result, in August of 1991 the Ministry of Northern Development and Mines carried out follow up work which resulted in the Ministry, considering at the time, the site to be high risk to adjacent human habitations, considerable erosion on slopes, pond water on surface and subject to seismic risk for run out. On September 22, 1992, the Mayor of Timmins declared an emergency under the Emergency Plans Act of Ontario allowing the province permission to enter the site on October 14.

Between November 1992 and January of 1993, the Ministry of Northern Development and Mines addressed areas of concern related to the western and southwestern dam walls, as well as ponding and surface water containment on top of the dam. (Morin, 1993) The Ministry recommend lifting the Emergency on January 13, 1993.

The west and southwest walls were steep with a 1H:1V slope, were poorly vegetated and showed signs of sloughing. To improve condition of the west and southwest dams they were re-sloped with Ministry funding to 3H:1V slope, and a rock fill berm was installed along the toe of both the west and southwest dam. To reduce the water level of ponded water on the surface of the Tailings Facility, a spillway through the west side of the stack was installed. The surface of the tailings stack was graded and vegetated to reduce erosion and dust control (2001 Site Summary Inspection Report, S. Reitzel and N. Verma, MNDM report).

6.9 Cogema Canada Ltd.

October 1, 1990, an option agreement between STLLR and Cogema Canada Limited to acquire a 50% interest in the Project. Cogema was required to make the following payments to STLLR to exercise the options, a total of \$500,000 in five separate instalments. As well as completed \$2,500,000 in expenditures on the property in no later than four separate deadlines spanning from December 31, 1991, to December 31, 1994. In 1991 Cogema proceeded with a geophysics exploration program followed up by a diamond drill program and additional geophysics in 1992. In 1993 the work was compiled and interpreted. The joint venture was never realized, and 100% ownership remained with STLLR.

1991 – Two assessments were done for Cogema Canada Ltd. on this year – on February 25, 1991, total field Mag, VLF-EM and Horizontal Loop EM surveys were done on these patents PAT-3033, PAT-3034 and PAT-526.

Also in summer of 1991 (reported in 1992), outcrop mapping and sampling have resulted in putting the Kayorum property in two domains – a domain of relatively simple stratigraphy and structure along the axis and limbs of the south Tisdale anticline which shows low background Au lithogeochemistry and another domain with more complex stratigraphy and structure with numerous east to west trending fold axes. Two anomalous areas within the more complex domain are interpreted to be the most promising targets for future work.

6.10 Erocon Waste Management Ltd.

A Waste Disposal Site (Landfill) was authorized on October 3, 1996. The site was approved for operate on 20 Ha of the Hollinger Tailings Facility located on Part of Lots 10 and 11, Concession 1.

An amended Environmental Compliance Approval (ECA; Number A770068) was issued December 7, 2022, for the Waste Disposal Site (Landfill) to authorize disposal of wood waste, demolition and construction waste not to exceed 10% of the total volume, and wood waste ash including fly ash and bottom ash. The ECA details requirements for Financial Assurance (FA) and the filing of a Closure Plan.

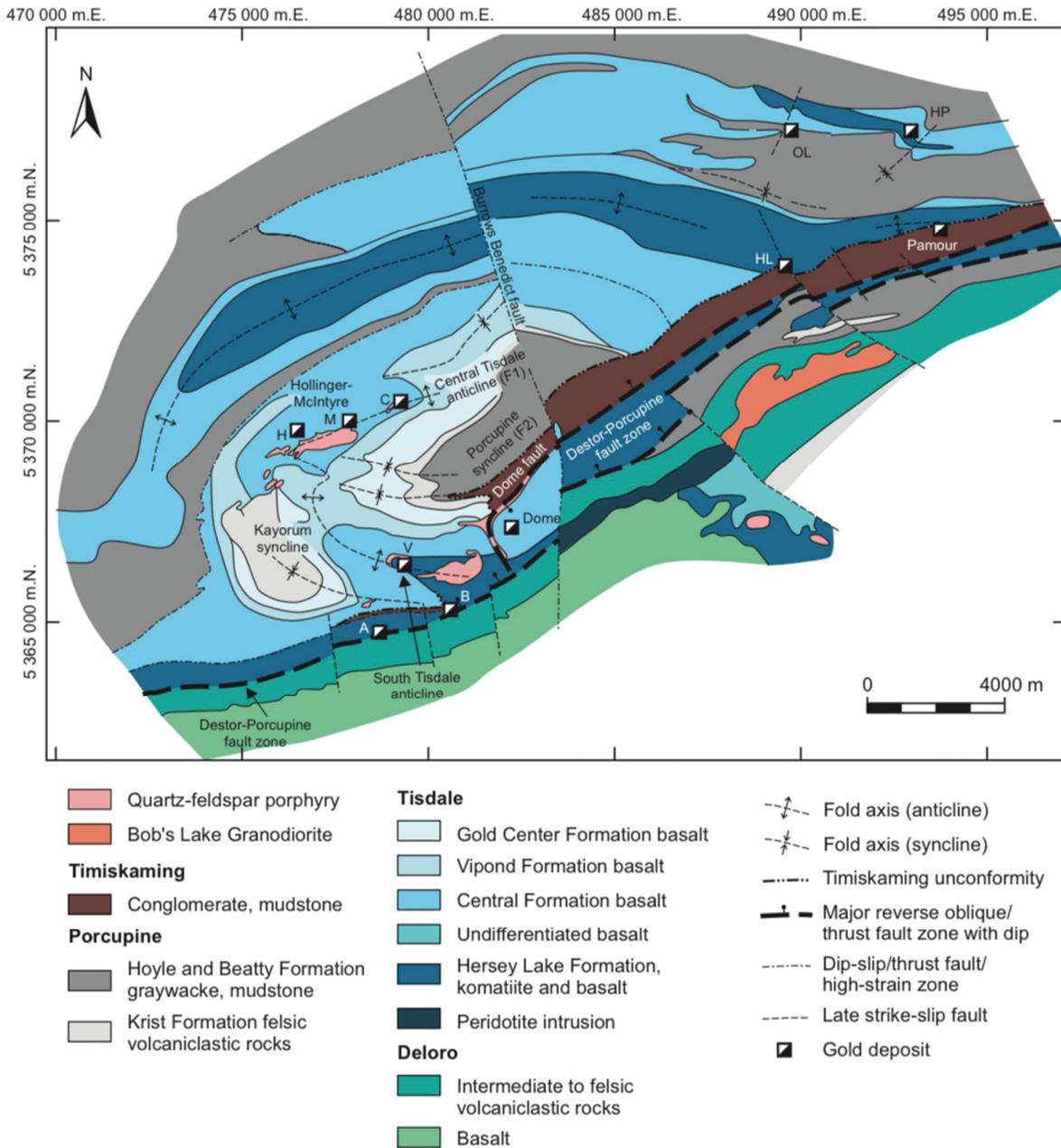
As per the ECA, FA was to be submitted on January 1, 2023, and will reach a total cumulative amount of \$429,309 as at January 1, 2026. A re-evaluation of FA must be submitted on December 1, 2027, and every five years thereafter.

The prescribed closure date within the ECA is December 31, 2026. If the site is intended to be operated beyond the prescribed date, an ECA application with updated FA must be submitted at least six months in advance. If the site is intended to be closed, a Closure Plan must be submitted at least one year prior to the anticipated closure date (Ministry of Environment, Conservation and Parks, 2022).

7.0 GEOLOGICAL SETTING AND MINERALIZATION

7.1 Regional Geology

The majority of the rock types underlying the Timmins area are Archean in age. Metavolcanic rocks have been subdivided into two groups, the Deloro and Tisdale assemblages (Figure 7.1). The Deloro Group is largely composed of calc-alkaline metavolcanics, primarily andesitic and basaltic flows in the lower part, and dacitic flows and, dacitic/rhyolitic pyroclastics towards the top of the sequence. Iron formation is common at or near the top of the group. Most of the Deloro Group is confined to a large domal structure located in the southern part of the area. A major change in volcanism marks the beginning of the younger Tisdale Group. The basal formations are largely made up of ultramafic to mafic komatiitic flows, which are overlain by a thick sequence of tholeiitic basalts. The top of the group is composed primarily of calc-alkaline, dacitic volcanoclastics. Metasedimentary rocks, including interlayered greywacke, siltstone and conglomerate are interpreted to be coeval with the upper part of the Deloro Group and all of the Tisdale Group. This turbidite sequence, together with a thin sequence of overlying fluvial sediments, has been referred to as the Porcupine Group. Small quartz-feldspar porphyry intrusions, possibly of subvolcanic origin, intruded into a restrictive stratigraphic interval of the Tisdale mafic flows.



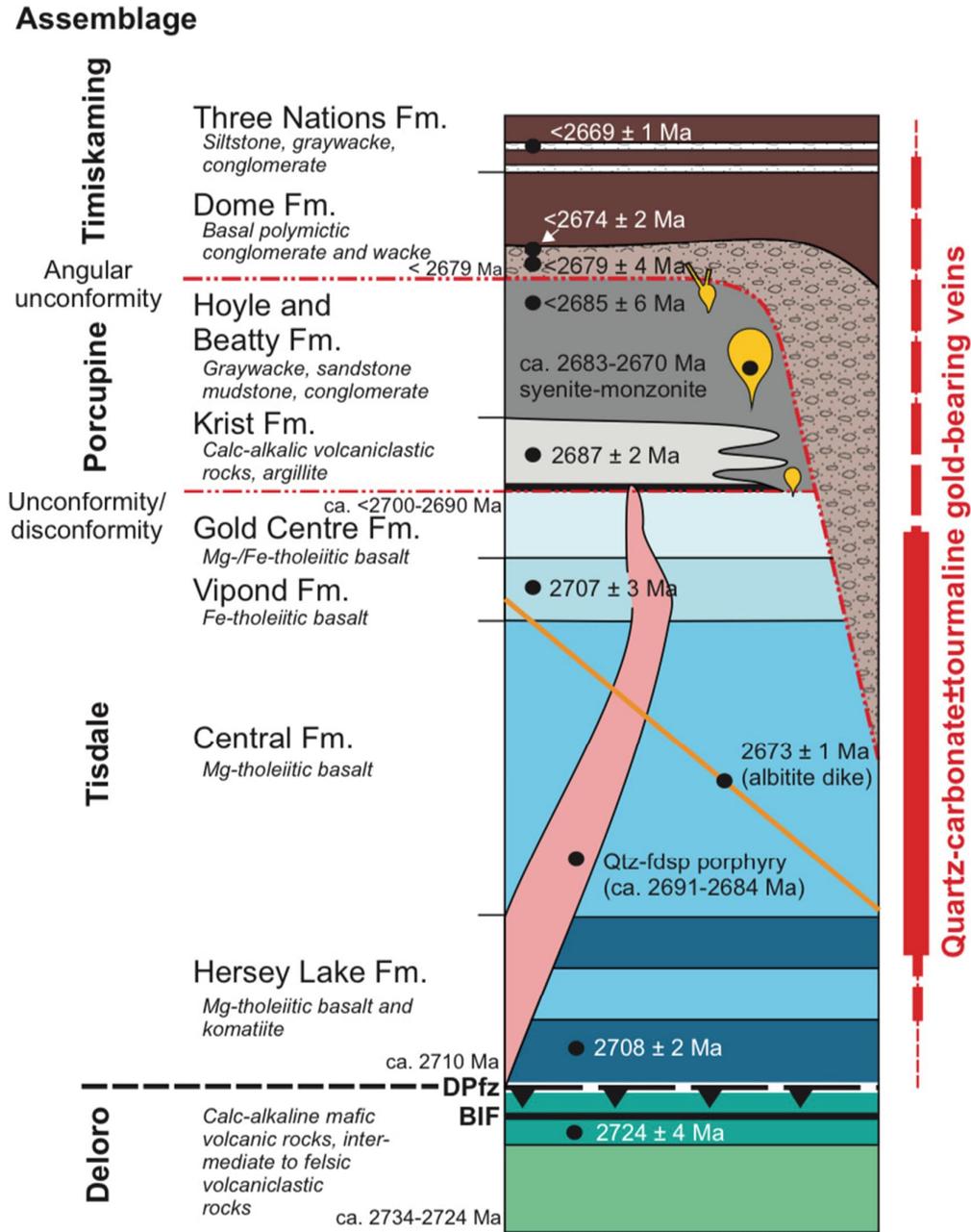
Note: Mine abbreviations: A= Aunor Delnite, B = Buffalo Ankerite, H = Hollinger, HL = Halnor, HP = Hoyle Pond, M = McIntyre, OL = Owl Creek, V = Vedron (Dubé, 2020)

Figure 7.1: Generalized Map of the Timmins-Porcupine Gold Camp

A major structural break, the DPFZ, trends northeast across the area, but is south of the property. North of the DPFZ, two periods of folding have been interpreted; an original north trending series of folds which have been refolded about an east-northeast axis. The main axis of the later folding is delineated by the Porcupine syncline.

South of the DPFZ, the Shaw Dome forms the main structural feature. This doming may be the result of the diapiric action of an underlying granitic body. Virtually all the production from the area has been from quartz

carbonate veins in metavolcanic/metasedimentary rocks and quartz stringers in porphyries north of the fault in the Tisdale Group. Most of the auriferous veins tend to be controlled by anticlinal axes.



Source: Dubé, 2020

Figure 7.2: Stratigraphic Column of the Timmins-Porcupine Gold Camp

7.2 Local Geology

The Project contains tailings generated by the Hollinger Mine. It is situated within the Abitibi Greenstone Belt, in the Porcupine Gold Camp, home to the Hollinger, McIntyre, and Dome Mines. The project area is situated immediately south of the Hollinger Mine property and to the south of the McIntyre Mine property.

The mafic volcanic stratigraphy in the core of the camp has been divided into the Deloro and Tisdale Group, and the Tisdale is comprised of four formations, the Hersey, Central, Vipond and Gold Centre (Figure 7.2). Narrow intervals of interflow sediments are formed within and at the contacts of these formations, and veins are often localized on these horizons. The Dome Mine is located mainly within the Vipond Formation, and the Hollinger-McIntyre Mines are mainly within the Central Formation. The Krist felsic volcanoclastic unit overlies the Tisdale Group.

The Central, Vipond, Gold Centre, and Krist Formations are present in the underlying rocks of the Project (Figure 7.3). This stratigraphy shows complex folding patterns, having been influenced by the Porcupine syncline and the South Tisdale anticline, and the Krist having been preserved within the Kayorum syncline.

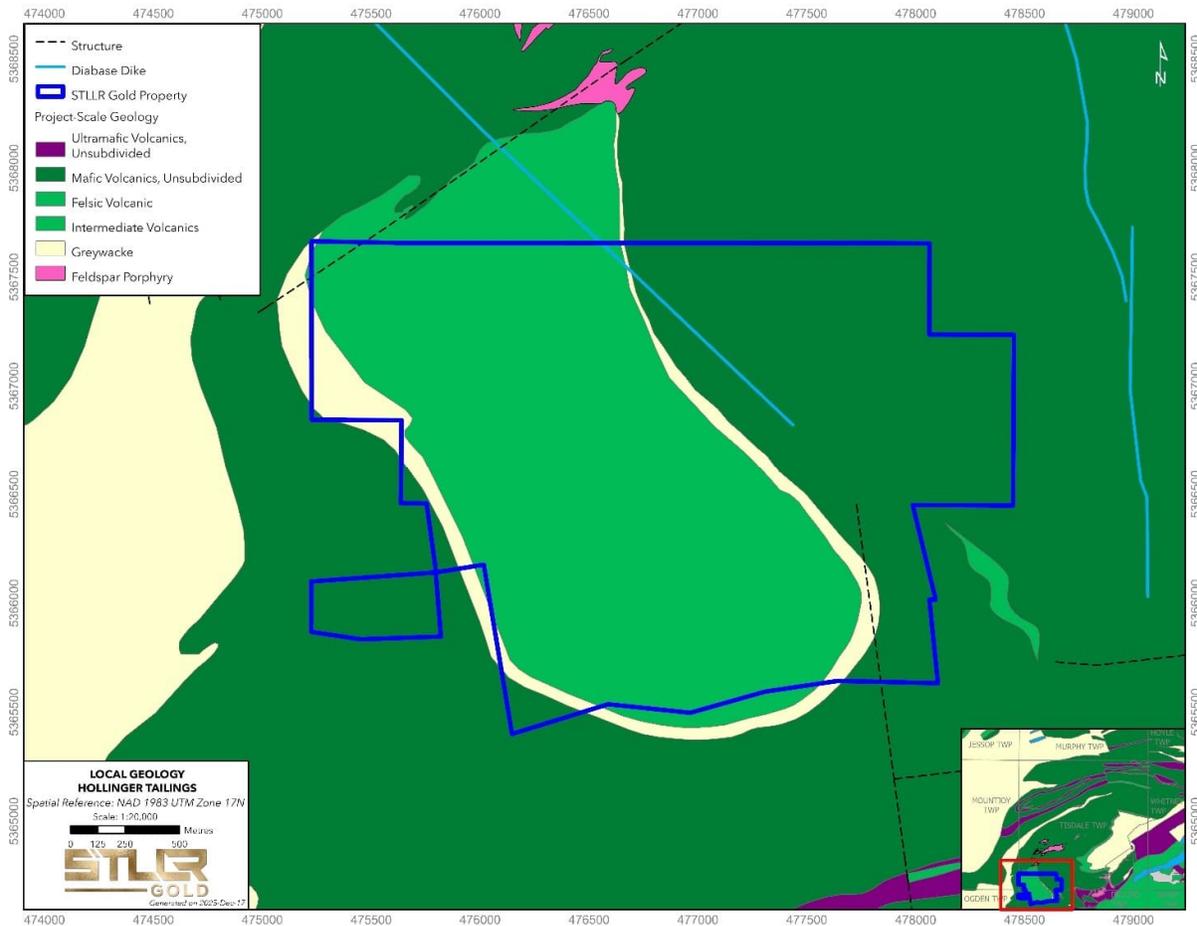


Figure 7.3: Local Geology Map

Krist Formation felsic volcanoclastic rocks and Porcupine Group turbidites, which overlie the Tisdale Group volcanic rocks, are preserved in a structural basin, the Kayorum syncline, through the eastern part of the property. The older Tisdale Group rocks flank the basin on all sides. The upper two thirds of the Tisdale Group stratigraphic section occur on the property. Pillowed and massive mafic flows comprising the upper portion of the Central Formation occur in the core of the South Tisdale anticline in the southeastern part of the property.

Carbonaceous argillites commonly occur at interflow horizons. Upper Central Formation mafic flows are by far the most important ore host in the Hollinger-McIntyre Complex.

The texturally distinctive Vipond Formation mafic flows occur in a crude S-shaped fold pattern through the centre of the property, reflecting their preservation on the flanks of the Kayorum syncline and the South Tisdale anticline. Vipond Formation mafic flows are one of the most important ore hosts at the Dome and Paymaster mines in southeastern Tisdale Township, and at the Vipond Mine on the south side of the Hollinger property.

The quaternary geology underlying the majority of the Tailings Facility is characterized as sandy glaciolacustrine plain. The east edge of the Tailings Facility is located on secondary till ground moraine deposits overlying rock ridges.

7.3 Deposit Geology

The Project represents an anthropogenic (man-made) deposit of gold bearing material, which is derived from historical mining and milling operations at the prolific Hollinger Mine in the Porcupine Mining Camp of Timmins, Ontario. In contrast to natural ore bodies, the geometry, mineralogical composition, and distribution of gold within the tailings are not governed by geological processes. Instead, the spatial distribution of gold reflects historical deposition practices, metal-recovery efficiencies, variability in the original ore grade, milling procedures and construction design.

The Hollinger Mine is located within a northeast-southwest trending, ductile-brittle shear zone, the Hollinger Shear Zone. This shear zone is characterized by a strong east-northeast striking foliation that dips 80° south, and a prominent elongation-stretching lineation plunging 60° to the east (Burrows et al., 1993). The orebody is hosted within a geologically complex zone of intensely folded and altered mafic and ultramafic volcanic rocks of the Tisdale assemblage, associated quartz-feldspar porphyry stocks, and Timiskaming aged sediments. The vein systems are related to a major structural break, the DPFZ.

The main mineralized event at the Hollinger Mine consists of high-grade quartz-carbonate-gold shear hosted veins. These veins crosscut others containing dominant quartz with subordinate ankerite, albite, scheelite, tourmaline, sulphides (sphalerite, chalcopyrite, pyrite, galena), tellurides, and gold. Host-rock alteration consists of sericite, ankerite, rutile, chlorite and sulphides. Veining is concentrated around the north and west of the Pearl Lake porphyry and along an east-northeast trending belt of high strain (Bateman et al. 2005).

The mineralogy and geochemistry of the original Hollinger ore, has strongly influenced the tailings composition, including the presence of fine-grained sulphides, and gold. The tailings are typically grey, tan and brown, and mainly composed of silts and fine sands, with coarse sands and clay-rich intervals. This stratification reflects changes in historical discharge points, mill feed, plant performance, and local reworking due to dam raises, reclamation activities or erosion.

The Hollinger Tailings Facility was built over a gently sloping topography, grading from the higher northeast to lower southwest. The dam height varies from 5 m to 30 m with the wall being at its highest along the southwest. The height of the wall variation reflects historical deposition methods and topography. The Hollinger Tailings Facility measures 1,950 m in length, 1,250 m in width and reaches a maximum depth of 40 m measured vertically from surface to the bottom of the tailings. Moisture is variable, depending on the facility drainage, but oxidation is common in the upper horizons.

The general method of tailings disposal was by pumping the tailings from the mill to the tailing disposal plant through two, twelve-inch diameter wood stave pipelines and then distributed from the plant to the surface of the facility, through spigots on 13,000 feet of 10-inch pipeline. The density of the transported tailing was reported to be between 40 and 50 percent solids which varied based on milling rates, as a minimum quantity of water was required to wash the belt conveyor carrying the cake discharge. The tailings were placed on the

facility surface through 600 feet of piping at a time, alternating spigots were opened and ran for approximately two hours then the spigots were closed, and the intervening spigots were opened. In the winter months an alternative method of distributing tailings was used, in which tailings were spilled into the ponds where solids could settle out in the water under ice. The tailings distribution from the spigot was sorted naturally by grain size, with the coarser sands remaining near the bank followed by fine sands and then by slimes being furthest from the spigot.

The facility was constructed in two phases. The first phase includes the northeast portion of the current facility and was subdivided into an east and west cell. The second phase was built later in the facility's life to expand capacity. The second phase extended the facility to the south and west and was also subdivided into an east and west cell. As tailings was added to the facility dam raises were constructed by dredging the deposited sands near the walls and shoveling it into dam walls. Each raise was constructed at approximate intervals of 8 feet high, 20 feet wide at the top and 40 feet wide at the base. The tops of the dam walls were sloped 8 to 10 inches toward the inner edge for drainage. The outer face was sloped at one and one half to one and the inner face at one to one (Mill Staff, 1951).

The stratigraphy of the Hollinger Tailings Facility shows consistency throughout with the sequence from top to bottom occurring as; surface fill, tailings, organics, glacial till and bedrock (Figure 7.4). The surface fill partially covers the till and includes, vegetation, ponded water, and in the northeast corner an active wood waste landfill owned by Erocon. Immediately below the cover is the tailings. The upper surface of the tailings shows evidence of oxidation and as a result has a brown colouring. The oxidation horizon measured in drill core varies from tens of centimetres to metre scale; however most tailings is saturated and has a dull grey colour. Below the tailings is a laterally extensive organic horizon which marks the bottom of the facility. Below the organic layer are glacial till with occasional gravel horizons, and finally the bedrock surface. The organic layer can show mixing with both the upper till and lower glacial till units due to construction methods. All units generally exhibit horizontal dips, although the tailings surface is observed to dip shallowly toward the

southwest.

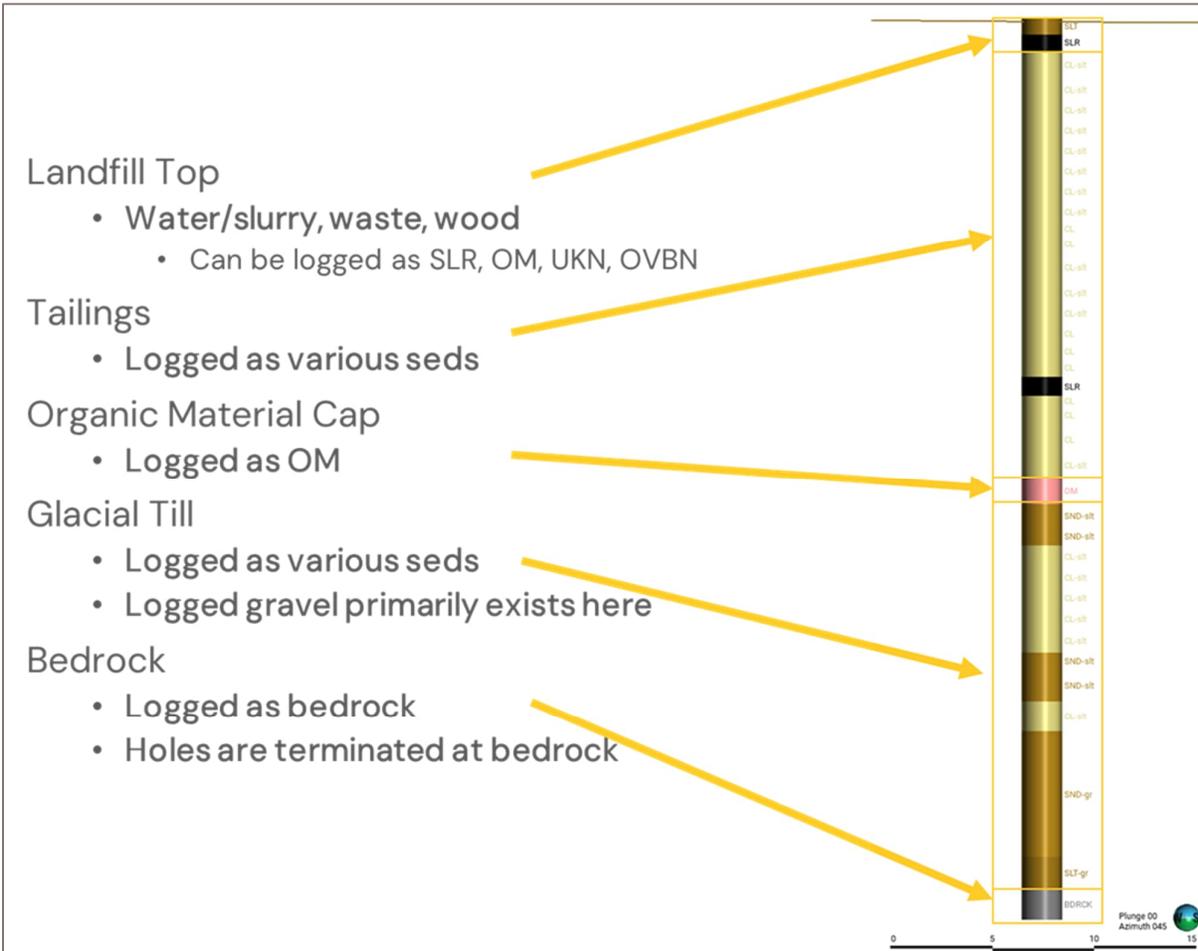


Figure 7.4: Generalized Deposit Sequence Downhole, Logged Material Observed within Each Unit is Described

7.4 Mineralization

Tailings form the principal gold-mineralized unit and comprise all logged sediments overlying the organic horizon (Figure 7.4). The surface fill, organics, till, and bedrock domains are generally barren of gold, with rare anomalous values attributed either to localized contamination from the tailings or to mineralization occurring naturally outside of the tailings.

Gold mineralization was consistently observed throughout the deposit both laterally and vertically however, distribution of gold is not governed by geological processes. Instead, the spatial distribution of gold reflects historical deposition practices, metal-recovery efficiencies, variability in the original ore grade, milling procedures, and construction design. No correlation was identified between particle size and gold content. Gold values within the tailings have a narrow range from below the detection limit to a maximum of 1.49 g/t Au. The mean gold grade within the tailings was 0.347 g/t. However, a higher-than-average grade was observed in Phase 1 cells and Phase 1 dam walls relative to the average. This is attributed to Phase 1 containing early mine life tailings which had a lower recovery rate at the Hollinger Mill and possibly higher-grade mill feed.

8.0 DEPOSIT TYPES

The Project consists of historical gold tailings material sourced from legacy milling and gravity separation, and cyanide leaching operations associated with the Hollinger Mine, in the Timmins Mining Camp of northeastern Ontario. Unlike natural geological gold deposits, the mineralized material is surficial in nature, unconsolidated, and contained within tailings storage facilities, resulting from historical mineral processing. As such, the “deposit type” is best described as anthropogenic (man-made), secondary gold mineralization hosted in engineered tailings facilities.

8.1 Genesis and Source of Material

The tailings were generated between 1910 and 1968 during the operation of the Hollinger Mine. Ore mined from quartz-carbonate veins was subjected to a combination of crushing, grinding, gravity concentration, and cyanidation. Residual gold is present due to historical metallurgical inefficiencies, or conservative processing parameters.

8.2 Physical Characteristics

The Hollinger Tailings Facility was built over a gently sloping topography, grading from the higher northeast to lower southwest. The maximum dam height is approximately 30 m high with local variations reflecting historical deposition methods and topography. Stratification can be observed in cross sections, representing multiple deposition phases, and variable grain-size distribution both laterally and vertically. The tailings exhibit fine grain distribution, dominated by silt and fine sand sized particles, with local coarser sand or clay, depending on mill configuration. The moisture content is also variable, ranging from saturated to dry depending on facility drainage. The degree of oxidation varies laterally and vertically within the facility, often forming an upper oxidized horizon.

8.3 Exploration Potential

Mining tailings are no longer viewed only as waste material. They hold exploration potential, as they are surface deposits with known history, they are uniform in scale, they have well defined boundaries, they have limited vertical extent, and they require simple mining methods. Gold tailings do require careful evaluation of metallurgy, bulk density variability, and geotechnical studies. This deposit type is common in mature mining jurisdictions, like the Timmins Camp, and offers potential for economic reprocessing using modern metallurgical techniques.

9.0 EXPLORATION

STLLR did not conduct any non-drilling exploration for the Project. Refer to Items 10.0 and 11.0 for a description of the drilling, sampling, analytical, and quality control procedures used to support this MRE.

Table 10.1: Summary of Drill Hole Details (assay results stated are for tailings material only)

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-001	5367017.9	476058.3	319.1	27.43	0	-90	33	37	2/7/2025	2/8/2025	0.00	22.86	22.86	0.37
including											19.81	22.10	2.29	0.62
HTF25-002	5367018.6	476111.4	320.0	24.38	0	-90	31	37	2/8/2025	2/8/2025	0.00	23.62	23.62	0.46
including											12.19	21.72	9.53	0.57
HTF25-003	5366967.3	476058.4	318.6	24.38	0	-90	31	34	2/8/2025	2/8/2025	0.00	23.47	23.47	0.38
including											18.29	23.47	5.18	0.69
HTF25-004	5366967.7	476107.5	320.6	27.43	0	-90	33	45	2/8/2025	2/8/2025	0.00	25.91	25.91	0.52
including											1.52	20.57	19.05	0.61
HTF25-005	5366919.7	476058.5	318.3	24.38	0	-90	30	34	2/8/2025	2/8/2025	0.00	21.79	21.79	0.27
including											21.34	21.79	0.45	1.19
HTF25-006	5366917.8	476107.3	318.3	27.43	0	-90	35	38	2/9/2025	2/9/2025	0.00	23.62	23.62	0.50
including											9.14	22.86	13.72	0.64
HTF25-007	5367018.5	476157.7	320.2	27.43	0	-90	35	38	2/9/2025	2/9/2025	0.00	24.38	24.38	0.36
HTF25-008	5366868.4	476109.3	318.1	27.43	0	-90	32	36	2/9/2025	2/9/2025	1.52	22.10	20.58	0.27
HTF25-009	5366968.8	476158.1	320.0	27.4	0	-90	34	38	2/9/2025	2/9/2025	0.00	24.40	24.40	0.44
including											11.45	23.60	12.15	0.51
HTF25-010	5367017.9	476208.5	320.8	27.45	0	-90	30	33	2/9/2025	2/9/2025	0.70	22.85	22.15	0.34
HTF25-011	5366917.9	476158.6	319.9	30.5	0	-90	39	42	2/9/2025	2/9/2025	0.00	23.55	23.55	0.48
including											3.00	4.60	1.60	0.57
including											9.10	16.80	7.70	0.56
including											19.80	21.30	1.50	0.66
HTF25-012	5366968.4	476208.2	320.6	27.45	0	-90	33	37	2/10/2025	2/10/2025	1.00	23.45	22.45	0.34
including											19.75	22.60	2.85	0.64
HTF25-013	5366865.6	476159.4	318.7	30.74	0	-90	32	35	2/9/2025	2/9/2025	0.40	23.80	23.40	0.66
including											0.40	20.43	20.03	0.72

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-014	5366918.5	476209.8	320.2	27.45	0	-90	34	38	2/10/2025	2/10/2025	0.00	23.55	23.55	0.39
HTF25-015	5366818.2	476158.5	318.9	27.45	0	-90	35	38	2/10/2025	2/10/2025	0.54	24.38	23.84	0.33
including											0.54	3.05	2.51	0.56
HTF25-016	5366867.5	476208.0	319.9	30.5	0	-90	39	43	2/10/2025	2/10/2025	0.00	23.55	23.55	0.41
including											15.25	19.80	4.55	0.53
HTF25-017	5367017.4	476258.6	321.3	24.4	0	-90	32	36	2/11/2025	2/11/2025	0.00	24.40	24.40	0.50
including											0.00	7.60	7.60	0.55
including											11.45	22.85	11.40	0.55
HTF25-018	5366817.3	476209.9	319.5	30.5	0	-90	38	43	2/11/2025	2/11/2025	0.40	28.95	28.55	0.48
including											0.40	19.05	18.65	0.51
including											24.40	27.45	3.05	0.74
HTF25-019	5366969.2	476260.7	321.0	27.45	0	-90	35	39	2/12/2025	2/12/2025	0.00	23.40	23.40	0.34
including											0.85	8.10	7.25	0.50
HTF25-020	5366767.2	476207.6	318.6	30.5	0	-90	41	44	2/10/2025	2/10/2025	0.00	24.40	24.40	0.53
including											4.90	23.40	18.50	0.61
HTF25-021	5366917.6	476257.1	320.3	24.4	0	-90	30	32	2/12/2025	2/12/2025	1.10	22.20	21.10	0.36
HTF25-022	5366720.2	476205.5	318.4	30.5	0	-90	36	49	2/10/2025	2/10/2025	0.00	1.25	1.25	0.46
and											3.80	24.00	20.20	0.59
HTF25-023	5366868	476258.3	319.8	45.74	0	-90	61	67	2/12/2025	2/12/2025	0.00	23.96	23.96	0.46
including											13.18	16.60	3.42	0.69
HTF25-024	5367021.2	476312.3	322.1	25.9	0	-90	32	44	2/12/2025	2/12/2025	0.00	25.45	25.45	0.55
including											0.00	21.90	21.90	0.60
HTF25-025	5366818.2	476258.5	319.6	30.5	0	-90	39	46	2/11/2025	2/11/2025	0.65	24.40	23.75	0.39
including											12.20	18.30	6.10	0.56
HTF25-026	5366967.6	476309.3	321.6	24.52	0	-90	29	33	2/13/2025	2/13/2025	0.75	24.52	23.77	0.44
including											0.75	5.75	5.00	0.58

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
including											20.65	23.58	2.93	0.59
HTF25-027	5366768	476258.5	319.1	27.45	0	-90	27	30	2/11/2025	2/11/2025	0.00	23.80	23.80	0.44
including											4.55	6.50	1.95	0.57
including											12.30	18.30	6.00	0.55
HTF25-028	5366917.1	476308.8	320.8	24.4	0	-90	29	31	2/13/2025	2/13/2025	1.25	24.40	23.15	0.36
including											20.60	23.15	2.55	0.59
HTF25-029	5366718	476258.0	318.8	30.5	0	-90	43	49	2/11/2025	2/11/2025	0.00	24.40	24.40	0.42
including											2.10	4.10	2.00	0.57
including											8.80	10.10	1.30	0.58
including											13.15	16.75	3.60	0.54
HTF25-030	5366867.4	476308.3	319.9	27.45	0	-90	36	39	2/13/2025	2/13/2025	0.00	22.20	22.20	0.35
HTF25-031	5367016	476357.1	319.0	24.4	0	-90	22	25	2/14/2025	2/14/2025	0.00	20.60	20.60	0.50
including											10.65	20.00	9.35	0.58
HTF25-032	5366816.1	476308.9	319.5	30.5	0	-90	30	34	2/13/2025	2/13/2025	0.00	23.35	23.35	0.32
HTF25-033	5366968.4	476357.5	322.1	27.45	0	-90	34	39	2/14/2025	2/14/2025	0.00	24.40	24.40	0.50
including											0.00	9.15	9.15	0.53
including											19.80	20.50	0.70	1.22
including											21.35	23.80	2.45	0.68
HTF25-034	5366767.3	476308.3	319.1	30.5	0	-90	26	29	2/13/2025	2/13/2025	0.00	23.65	23.65	0.37
including											21.35	23.65	2.30	0.64
HTF25-035	5366918.7	476358.1	320.9	27.45	0	-90	33	48	2/14/2025	2/14/2025	0.00	24.30	24.30	0.40
including											17.10	23.50	6.40	0.51
HTF25-036	5366717.2	476307.7	318.7	30.5	0	-90	37	43	2/13/2025	2/13/2025	0.00	23.69	23.69	0.35
HTF25-037	5366867.8	476356.8	320.0	29.06	0	-90	37	41	2/14/2025	2/14/2025	0.00	24.47	24.47	0.34
HTF25-038	5367018.8	476408.0	318.9	24.4	0	-90	25	28	2/15/2025	2/15/2025	0.00	22.05	22.05	0.53
including											0.70	6.10	5.40	0.68

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
including											8.15	18.70	10.55	0.60
HTF25-039	5366817.2	476356.5	319.5	30.5	0	-90	29	32	2/15/2025	2/15/2025	0.00	23.85	23.85	0.36
HTF25-040	5366968.1	476408.4	321.5	27.45	0	-90	35	40	2/15/2025	2/15/2025	0.35	23.40	23.05	0.54
including											0.35	6.85	6.50	0.65
including											12.20	21.35	9.15	0.57
HTF25-041	5366767.3	476357.6	318.9	30.5	0	-90	40	44	2/14/2025	2/14/2025	0.45	23.70	23.25	0.30
HTF25-042	5366918.3	476407.7	320.6	27.59	0	-90	35	40	2/15/2025	2/15/2025	0.00	23.70	23.70	0.40
including											0.00	0.80	0.80	1.10
including											2.12	4.60	2.48	0.57
including											20.93	22.37	1.44	0.61
HTF25-043	5366717.7	476358.1	318.6	30.5	0	-90	40	44	2/14/2025	2/14/2025	1.10	24.00	22.90	0.34
HTF25-044	5366867.9	476407.8	320.0	30.5	0	-90	29	32	2/16/2025	2/16/2025	0.00	22.30	22.30	0.33
HTF25-045	5367018.7	476457.1	318.7	30.5	0	-90	26	29	2/16/2025	2/16/2025	0.00	20.70	20.70	0.45
including											11.00	17.00	6.00	0.60
HTF25-046	5366819.1	476407.3	319.4	30.5	0	-90	30	32	2/16/2025	2/16/2025	0.00	23.55	23.55	0.35
HTF25-047	5366968.5	476458.3	319.5	27.45	0	-90	26	29	2/16/2025	2/16/2025	0.00	23.70	23.70	0.41
HTF25-048	5366768.5	476407.4	319.0	30.68	0	-90	40	53	2/15/2025	2/15/2025	0.40	23.50	23.10	0.30
HTF25-049	5366918.5	476457.8	320.3	27.45	0	-90	26	29	2/17/2025	2/17/2025	0.00	23.35	23.35	0.38
HTF25-050	5366718.9	476407.5	318.5	30.5	0	-90	39	43	2/15/2025	2/15/2025	0.70	24.40	23.70	0.36
HTF25-051	5366869.2	476458.4	319.9	30.5	0	-90	28	30	2/17/2025	2/17/2025	0.00	25.00	25.00	0.37
including											19.00	23.00	4.00	0.51
HTF25-052	5366668.2	476508.0	318.4	27.45	0	-90	23	26	2/17/2025	2/17/2025	1.00	22.40	21.40	0.34
HTF25-053	5366816.8	476454.9	319.4	27.45	0	-90	28	30	2/17/2025	2/17/2025	0.00	23.80	23.80	0.30
HTF25-054	5366718.2	476507.9	318.9	44.2	0	-90	31	33	2/18/2025	2/18/2025	0.00	22.55	22.55	0.24
HTF25-055	5366768.8	476457.4	319.1	27.45	0	-90	33	36	2/18/2025	2/18/2025	1.00	25.10	24.10	0.31
HTF25-056	5366668.4	476557.8	318.6	30.5	0	-90	36	49	2/18/2025	2/18/2025	0.43	23.60	23.17	0.29

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-057	5366717.5	476458.7	318.5	30.5	0	-90	29	32	2/16/2025	2/16/2025	0.00	23.30	23.30	0.29
HTF25-058	5366718.1	476558.0	318.9	30.5	0	-90	29	32	2/18/2025	2/18/2025	0.00	22.00	22.00	0.28
HTF25-059	5366667.8	476458.4	318.3	30.5	0	-90	29	33	2/17/2025	2/17/2025	0.00	22.25	22.25	0.32
including											19.80	22.25	2.45	0.54
HTF25-060	5366667.8	476609.4	319.2	30.5	0	-90	23	25	2/19/2025	2/19/2025	0.00	21.90	21.90	0.33
HTF25-061	5367017.9	476504.8	318.5	27.45	0	-90	36	47	2/18/2025	2/18/2025	0.00	24.40	24.40	0.50
including											0.00	2.15	2.15	0.53
including											9.15	22.15	13.00	0.60
HTF25-062	5366718.3	476607.6	319.0	30.5	0	-90	37	40	2/19/2025	2/19/2025	0.95	22.20	21.25	0.31
HTF25-063	5367018.1	476558.3	319.0	24.4	0	-90	30	37	2/18/2025	2/18/2025	0.00	21.35	21.35	0.50
including											9.15	20.40	11.25	0.55
HTF25-064	5366720.5	476710.9	320.9	30.5	0	-90	35	38	2/20/2025	2/20/2025	2.50	23.85	21.35	0.32
including											2.50	4.55	2.05	0.53
HTF25-065	5367018.6	476607.3	319.4	19.8	0	-90	23	23	2/19/2025	2/19/2025	0.00	19.80	19.80	0.50
HTF25-066	5366672.4	476711.5	318.9	27.45	0	-90	33	36	2/21/2025	2/21/2025	1.50	21.35	19.85	0.39
including											8.35	13.70	5.35	0.50
HTF25-067	5367023.8	476664.3	321.5	25.9	0	-90	31	35	2/19/2025	2/19/2025	0.00	23.40	23.40	0.44
including											16.75	23.40	6.65	0.57
HTF25-068	5366723.9	476752.4	321.7	28.95	0	-90	25	28	2/21/2025	2/21/2025	4.55	22.85	18.30	0.31
HTF25-069	5366966.1	476661.8	321.3	27.45	0	-90	34	38	2/19/2025	2/19/2025	0.00	24.21	24.21	0.45
including											0.00	1.80	1.80	0.64
HTF25-070	5366659.3	476760.1	318.5	24.4	0	-90	31	35	2/21/2025	2/21/2025	0.30	21.35	21.05	0.34
HTF25-071	5366917.2	476654.8	321.6	27.45	0	-90	33	35	2/20/2025	2/20/2025	2.40	26.70	24.30	0.43
including											21.35	25.90	4.55	0.58
HTF25-072	5366769	476809.9	321.7	22.85	0	-90	23	26	2/22/2025	2/22/2025	3.45	22.85	19.40	0.37
including											13.00	15.25	2.25	0.59

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-073	5366872.8	476656.2	320.5	30.5	0	-90	36	40	2/20/2025	2/20/2025	0.00	26.70	26.70	0.35
HTF25-074	5366718	476807.4	317.9	24.4	0	-90	29	40	2/20/2025	2/20/2025	0.00	20.70	20.70	0.30
HTF25-075	5366810.5	476658.9	320.0	30.5	0	-90	38	43	2/20/2025	2/20/2025	0.60	22.50	21.90	0.33
HTF25-076	5366667.3	476810.5	318.1	24.4	0	-90	31	35	2/21/2025	2/21/2025	0.50	20.75	20.25	0.30
HTF25-077	5366768.2	476658.7	320.3	30.5	0	-90	35	37	2/20/2025	2/20/2025	2.10	24.40	22.30	0.31
HTF25-078	5366766.1	476700.1	322.2	27.45	0	-90	30	34	2/22/2025	2/22/2025	3.30	24.40	21.10	0.40
including											3.30	8.85	5.55	0.58
HTF25-079	5366718.4	476658.2	319.9	30.5	0	-90	37	41	2/20/2025	2/20/2025	1.40	24.40	23.00	0.37
including											1.40	3.05	1.65	0.54
HTF25-080	5366664.9	476854.9	317.6	21.35	0	-90	27	30	2/22/2025	2/22/2025	0.00	21.35	21.35	0.34
HTF25-081	5366670	476654.9	320.7	30.5	0	-90	38	42	2/19/2025	2/19/2025	0.00	23.35	23.35	0.41
HTF25-082	5367017.4	476856.6	327.0	25.9	0	-90	21	24	2/23/2025	2/23/2025	8.60	23.65	15.05	0.45
HTF25-083	5367023.6	476710.2	321.6	19.8	0	-90	22	25	2/20/2025	2/20/2025	0.00	19.80	19.80	0.47
including											4.00	18.30	14.30	0.51
HTF25-084	5366967.9	476857.9	327.3	30.5	0	-90	28	32	2/23/2025	2/23/2025	8.35	24.40	16.05	0.40
including											19.00	21.35	2.35	0.71
HTF25-085	5367016.5	476757.0	321.4	15.25	0	-90	17	19	2/21/2025	2/21/2025	0.00	15.25	15.25	0.48
including											0.00	3.05	3.05	0.56
including											5.20	15.25	10.05	0.51
HTF25-086	5366920.7	476860.1	327.0	28.95	0	-90	26	29	2/24/2025	2/24/2025	8.55	25.90	17.35	0.34
including											16.00	18.30	2.30	0.50
HTF25-087	5366965.9	476713.2	324.4	30.5	0	-90	34	48	2/21/2025	2/21/2025	3.70	25.90	22.20	0.46
including											13.00	25.90	12.90	0.55
HTF25-088	5366869	476854.8	327.4	33.5	0	-90	23	24	2/24/2025	2/24/2025	9.61	28.70	19.09	0.30
HTF25-089	5366922.1	476715.0	326.0	30.5	0	-90	28	31	2/21/2025	2/21/2025	7.30	29.70	22.40	0.42
including											18.30	24.40	6.10	0.54

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-090	5367018.2	476902.6	327.6	27.45	0	-90	27	38	2/25/2025	2/25/2025	7.05	23.00	15.95	0.45
including											17.50	22.30	4.80	0.57
HTF25-091	5366867.1	476719.3	327.0	25.9	0	-90	23	25	2/21/2025	2/21/2025	7.15	25.90	18.75	0.40
including											17.55	23.60	6.05	0.50
HTF25-092	5366963.9	476906.4	327.8	21.35	0	-90	13	15	2/24/2025	2/24/2025	8.70	20.82	12.12	0.36
HTF25-093	5366962.2	476759.3	325.7	22.85	0	-90	20	22	2/22/2025	2/22/2025	6.10	22.85	16.75	0.38
HTF25-094	5366918.3	476906.5	327.5	25.9	0	-90	21	24	2/24/2025	2/24/2025	9.75	23.95	14.20	0.36
HTF25-095	5366917.3	476758.1	325.9	28.95	0	-90	27	30	2/22/2025	2/22/2025	7.20	25.10	17.90	0.43
including											18.30	24.40	6.10	0.52
HTF25-096	5366877.5	476911.0	325.8	27.45	0	-90	18	20	2/27/2025	2/27/2025	9.00	26.40	17.40	0.34
HTF25-097	5366870.7	476762.3	326.0	25.9	0	-90	23	25	2/22/2025	2/22/2025	8.05	25.90	17.85	0.40
including											18.30	21.35	3.05	0.68
HTF25-098	5366821.4	476908.8	320.2	25.9	0	-90	30	39	2/25/2025	2/25/2025	2.70	22.00	19.30	0.27
HTF25-099	5366824.6	476756.4	326.2	30.5	0	-90	27	30	2/22/2025	2/22/2025	6.63	26.15	19.52	0.36
HTF25-100	5366922.9	476959.9	326.9	28.95	0	-90	24	26	2/25/2025	2/25/2025	8.52	25.90	17.38	0.31
HTF25-101	5367007.1	476814.7	327.0	27.45	0	-90	23	26	2/23/2025	2/23/2025	8.70	24.40	15.70	0.39
HTF25-102	5366874.9	476957.2	324.9	28.95	0	-90	27	31	2/25/2025	2/25/2025	7.10	25.70	18.60	0.31
HTF25-103	5366968.9	476808.1	326.0	25.9	0	-90	16	17	2/23/2025	2/23/2025	7.20	10.65	3.45	0.43
and											13.70	24.40	10.70	0.34
HTF25-104	5366818.7	476959.3	317.9	19.8	0	-90	21	24	2/26/2025	2/26/2025	0.00	17.87	17.87	0.26
HTF25-105	5366919.3	476807.5	327.2	30.5	0	-90	24	27	2/22/2025	2/22/2025	7.98	25.90	17.92	0.36
including											19.80	21.35	1.55	0.68
HTF25-106	5366872.2	477006.7	318.4	21.35	0	-90	27	30	2/26/2025	2/26/2025	0.60	18.30	17.70	0.26
HTF25-107	5366868	476806.9	327.1	30.5	0	-90	29	31	2/23/2025	2/23/2025	8.75	26.50	17.75	0.35
including											19.80	21.35	1.55	0.77
HTF25-108	5366767.8	476907.7	317.7	24.4	0	-90	26	29	2/26/2025	2/26/2025	0.75	17.45	16.70	0.29

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-109	5367068.3	476255.8	320.6	24.4	0	-90	17	19	2/26/2025	2/26/2025	0.00	6.80	6.80	0.43
and											9.40	20.30	10.90	0.49
including											11.00	20.30	9.30	0.51
HTF25-110	5366820.2	477007.9	318.1	22.85	0	-90	19	21	2/26/2025	2/26/2025	0.75	18.65	17.90	0.26
HTF25-111	5367119.6	476259.5	321.2	18.3	0	-90	22	24	2/26/2025	2/26/2025	0.75	17.50	16.75	0.54
including											0.75	7.60	6.85	0.57
including											12.20	17.50	5.30	0.68
HTF25-112	5366817.8	475809.5	319.2	30.5	0	-90	29	37	3/1/2025	3/1/2025	0.00	25.00	25.00	0.31
including											0.00	3.05	3.05	0.53
HTF25-113	5367118.3	476208.1	320.3	18.3	0	-90	17	19	2/27/2025	2/27/2025	0.00	17.60	17.60	0.40
including											11.75	17.60	5.85	0.52
HTF25-114	5366920.6	477009.6	324.6	28.95	0	-90	27	30	2/26/2025	2/26/2025	6.85	25.90	19.05	0.27
HTF25-115	5367069.6	476206.5	320.2	24.4	0	-90	23	25	2/27/2025	2/27/2025	0.00	22.55	22.55	0.42
including											0.00	1.00	1.00	1.26
including											18.75	21.85	3.10	0.48
HTF25-116	5366968.5	476961.5	324.6	24.4	0	-90	16	18	2/27/2025	2/27/2025	5.40	20.10	14.70	0.30
HTF25-117	5367059.1	476158.2	320.2	24.4	0	-90	29	32	2/27/2025	2/27/2025	0.00	22.40	22.40	0.34
HTF25-118	5367015.6	476961.4	324.8	30.5	0	-90	21	23	2/28/2025	2/28/2025	5.55	16.00	10.45	0.43
HTF25-119	5367119.9	476158.0	320.5	22.85	0	-90	26	29	2/27/2025	2/27/2025	0.00	21.65	21.65	0.34
HTF25-120	5366820.2	475856.5	319.0	30.5	0	-90	24	28	3/1/2025	3/1/2025	0.00	22.30	22.30	0.25
HTF25-121	5367169	476157.4	320.8	22.85	0	-90	22	23	2/27/2025	2/27/2025	0.00	22.40	22.40	0.37
including											2.00	4.55	2.55	0.60
HTF25-122	5366817.3	475907.5	318.2	24.4	0	-90	22	24	3/1/2025	3/1/2025	0.00	22.45	22.45	0.22
HTF25-123	5367163	476208.7	320.9	16.75	0	-90	18	20	2/27/2025	2/27/2025	0.00	16.75	16.75	0.48
including											0.00	4.10	4.10	0.57
including											11.30	16.75	5.45	0.51

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-124	5366715.9	475805.4	319.4	30.5	0	-90	29	32	3/1/2025	3/1/2025	0.00	27.45	27.45	0.27
HTF25-125	5367168.3	476105.2	320.9	21.35	0	-90	19	21	2/28/2025	2/28/2025	0.00	17.85	17.85	0.48
including											0.00	2.00	2.00	0.58
including											5.00	7.60	2.60	0.56
including											12.00	15.60	3.60	0.66
HTF25-126	5366718.7	475854.8	319.1	30.5	0	-90	31	34	3/6/2025	3/6/2025	0.00	24.85	24.85	0.30
HTF25-127	5367117.9	476109.2	320.6	22.85	0	-90	19	27	2/28/2025	2/28/2025	0.00	21.35	21.35	0.55
including											1.20	5.00	3.80	0.86
including											13.00	21.35	8.35	0.60
HTF25-128	5366713.6	475909.1	318.6	30.5	0	-90	27	30	3/2/2025	3/2/2025	0.00	25.90	25.90	0.21
HTF25-129	5367070.7	476107.3	320.0	25.9	0	-90	21	23	2/28/2025	2/28/2025	0.00	23.40	23.40	0.54
including											3.70	9.65	5.95	0.52
including											13.70	23.40	9.70	0.62
HTF25-130	5366718.9	475956.9	318.1	30.5	0	-90	29	32	3/2/2025	3/2/2025	0.00	23.55	23.55	0.19
HTF25-131	5367069.5	476060.8	320.1	24.4	0	-90	25	28	2/28/2025	2/28/2025	0.00	23.80	23.80	0.39
including											0.00	3.70	3.70	0.58
including											18.30	23.80	5.50	0.55
HTF25-132	5366618.2	475857.9	319.1	30.5	0	-90	32	35	3/2/2025	3/2/2025	0.00	27.45	27.45	0.31
HTF25-133	5367118.5	476058.5	320.4	21.35	0	-90	22	24	2/28/2025	2/28/2025	0.00	21.35	21.35	0.43
including											0.00	2.50	2.50	0.71
including											16.75	21.35	4.60	0.54
HTF25-134	5366615.1	475909.5	318.7	30.5	0	-90	28	31	3/3/2025	3/3/2025	0.00	26.50	26.50	0.26
HTF25-135	5367165.6	476061.1	320.7	21.35	0	-90	24	26	2/28/2025	2/28/2025	0.00	21.10	21.10	0.42
including											0.00	2.00	2.00	0.53
including											19.80	21.10	1.30	0.86
HTF25-136	5366614.4	475956.8	318.4	30.5	0	-90	27	29	3/3/2025	3/3/2025	0.45	25.60	25.15	0.24

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
including											23.85	25.60	1.75	0.50
HTF25-137	5366766.8	475807.1	319.2	27.45	0	-90	23	26	2/28/2025	2/28/2025	0.00	22.50	22.50	0.33
HTF25-138	5366620.9	476007.6	318.0	30.5	0	-90	27	30	3/3/2025	3/3/2025	0.00	29.30	29.30	0.31
including											23.00	29.30	6.30	0.67
HTF25-139	5366767.3	475855.5	318.9	30.5	0	-90	30	33	3/1/2025	3/1/2025	0.00	27.45	27.45	0.25
HTF25-140	5366619.5	476058.6	317.7	30.5	0	-90	32	36	3/3/2025	3/3/2025	0.00	27.00	27.00	0.30
including											19.80	27.00	7.20	0.63
HTF25-141	5366768.4	475907.7	318.3	30.5	0	-90	28	31	3/1/2025	3/1/2025	0.00	24.80	24.80	0.18
HTF25-142	5366569.2	476057.4	318.0	30.5	0	-90	28	32	3/4/2025	3/4/2025	0.00	26.00	26.00	0.29
including											19.80	26.00	6.20	0.59
HTF25-143	5366770	475958.7	318.1	30.5	0	-90	31	34	3/1/2025	3/1/2025	0.00	22.00	22.00	0.20
HTF25-144	5366567.9	476106.9	317.7	24.4	0	-90	28	31	3/5/2025	3/5/2025	0.00	23.05	23.05	0.22
HTF25-145	5366665.4	475813.6	319.4	30.5	0	-90	28	31	3/2/2025	3/2/2025	0.00	28.00	28.00	0.27
HTF25-146	5366567.1	476160.9	318.8	27.45	0	-90	24	33	3/5/2025	3/5/2025	0.00	25.50	25.50	0.48
including											9.00	20.50	11.50	0.60
HTF25-147	5366667	475855.1	319.1	32	0	-90	30	42	3/2/2025	3/2/2025	0.00	26.40	26.40	0.29
HTF25-148	5366516	476106.3	317.9	30.5	0	-90	33	35	3/5/2025	3/5/2025	0.00	23.85	23.85	0.37
including											14.50	23.85	9.35	0.63
HTF25-149	5366669.4	475910.0	318.6	30.5	0	-90	31	33	3/2/2025	3/2/2025	0.00	27.45	27.45	0.25
HTF25-150	5366463	476157.8	317.9	24.4	0	-90	23	25	3/8/2025	3/8/2025	0.00	22.85	22.85	0.19
HTF25-151	5366667.9	475961.4	318.4	30.5	0	-90	31	34	3/3/2025	3/3/2025	0.00	23.25	23.25	0.23
HTF25-152	5366567	476013.4	318.2	32	0	-90	33	36	3/4/2025	3/4/2025	0.00	23.40	23.40	0.20
HTF25-153	5366667	476008.2	317.9	33.55	0	-90	34	38	3/2/2025	3/2/2025	0.00	27.45	27.45	0.34
including											21.35	27.45	6.10	0.83
HTF25-154	5366565.5	475959.4	318.7	30.5	0	-90	29	32	3/4/2025	3/4/2025	0.00	26.00	26.00	0.24
HTF25-155	5366716.3	476009.2	317.8	30.5	0	-90	31	34	3/3/2025	3/3/2025	0.00	26.00	26.00	0.23

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
including											22.00	23.70	1.70	0.76
HTF25-156	5366516.8	476008.3	318.5	36.6	0	-90	34	38	3/4/2025	3/4/2025	0.00	24.40	24.40	0.24
HTF25-157	5366767.6	476009.3	317.7	30.5	0	-90	32	36	3/3/2025	3/3/2025	0.40	30.50	30.10	0.29
including											19.00	21.35	2.35	0.50
HTF25-158	5366518	476056.2	318.3	30.5	0	-90	29	32	3/6/2025	3/6/2025	0.00	27.45	27.45	0.47
including											19.00	27.45	8.45	0.97
HTF25-159	5366819.4	476002.3	317.7	30.5	0	-90	29	32	3/4/2025	3/4/2025	0.00	22.65	22.65	0.20
HTF25-160	5366468.7	476058.6	318.5	30.5	0	-90	29	32	3/5/2025	3/5/2025	0.00	25.70	25.70	0.26
HTF25-161	5366817.8	475957.7	318.0	30.5	0	-90	30	33	3/4/2025	3/4/2025	0.00	23.00	23.00	0.20
HTF25-162	5366468	476004.9	319.0	33.5	0	-90	33	36	3/5/2025	3/5/2025	0.00	28.40	28.40	0.28
HTF25-163	5366870.7	476056.9	317.8	30.5	0	-90	29	30	3/4/2025	3/4/2025	0.00	24.45	24.45	0.33
including											20.45	24.45	4.00	0.97
HTF25-164	5366567.3	475908.3	319.0	30.5	0	-90	34	38	3/7/2025	3/7/2025	0.00	26.20	26.20	0.32
HTF25-165	5366819.7	476109.1	318.1	30.5	0	-90	29	33	3/4/2025	3/4/2025	0.00	23.20	23.20	0.29
HTF25-166	5366465.7	476107.6	318.1	27.45	0	-90	29	33	3/6/2025	3/6/2025	0.00	25.00	25.00	0.23
HTF25-167	5366768.1	476157.9	318.3	27.45	0	-90	26	29	3/5/2025	3/5/2025	0.00	23.20	23.20	0.23
HTF25-168	5366420	476107.4	318.6	27.45	0	-90	30	32	3/6/2025	3/6/2025	0.00	24.70	24.70	0.24
HTF25-169	5366665.6	476208.7	318.5	28.95	0	-90	27	30	3/5/2025	3/5/2025	0.00	23.60	23.60	0.39
HTF25-170	5366371.5	476111.1	318.9	27.45	0	-90	28	31	3/6/2025	3/6/2025	0.00	26.90	26.90	0.28
HTF25-171	5366671.3	476258.8	318.1	30.5	0	-90	30	33	3/5/2025	3/5/2025	0.00	22.85	22.85	0.39
including											15.00	17.00	2.00	0.54
HTF25-172	5366418	476009.5	319.3	36.6	0	-90	34	38	3/7/2025	3/7/2025	0.00	28.50	28.50	0.29
HTF25-173	5366670.5	476307.6	318.2	30.5	0	-90	35	39	3/5/2025	3/5/2025	0.00	23.50	23.50	0.36
HTF25-174	5366371.7	476064.7	319.2	36.6	0	-90	35	39	3/7/2025	3/7/2025	0.00	27.45	27.45	0.29
HTF25-175	5366667.6	476357.3	318.2	30.5	0	-90	29	31	3/6/2025	3/6/2025	0.00	23.30	23.30	0.36
HTF25-176	5366325.5	476112.5	319.4	33.5	0	-90	33	36	3/7/2025	3/7/2025	0.00	27.45	27.45	0.30

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-177	5366668.2	476407.0	318.0	30.5	0	-90	30	35	3/6/2025	3/6/2025	0.00	22.15	22.15	0.37
including											15.25	16.75	1.50	0.69
HTF25-178	5366406.4	476205.7	318.0	25.9	0	-90	26	29	3/8/2025	3/8/2025	0.00	23.25	23.25	0.22
HTF25-179	5366718.1	476858.2	317.4	24.4	0	-90	23	25	3/6/2025	3/6/2025	0.00	20.40	20.40	0.33
HTF25-180	5366417.6	476158.1	318.2	30.5	0	-90	29	32	3/7/2025	3/7/2025	0.00	21.05	21.05	0.25
including											19.60	21.05	1.45	0.63
HTF25-181	5366224.2	476213.5	319.6	30.5	0	-90	30	33	3/9/2025	3/9/2025	0.00	24.40	24.40	0.32
HTF25-182	5366368.8	476158.1	318.5	27.45	0	-90	29	33	3/7/2025	3/7/2025	0.00	23.10	23.10	0.27
HTF25-183	5366275.4	476165.5	319.4	30.5	0	-90	31	34	3/8/2025	3/8/2025	0.00	25.90	25.90	0.30
HTF25-184	5366313.1	476158.4	319.1	32	0	-90	30	39	3/7/2025	3/7/2025	0.00	24.40	24.40	0.30
HTF25-185	5366266.6	476208.4	319.1	27.45	0	-90	25	28	3/8/2025	3/8/2025	0.00	24.00	24.00	0.30
HTF25-186	5366315.5	476204.9	318.6	25.9	0	-90	24	26	3/8/2025	3/8/2025	0.00	24.10	24.10	0.28
HTF25-187	5366363.3	476207.3	318.1	24.1	0	-90	27	31	3/8/2025	3/8/2025	0.00	22.05	22.05	0.27
HTF25-188	5366219.3	476260.2	319.3	30.5	0	-90	33	37	3/9/2025	3/9/2025	0.00	24.25	24.25	0.30
HTF25-189	5366270.3	476262.3	318.5	27.45	0	-90	27	31	3/9/2025	3/9/2025	0.00	23.50	23.50	0.26
HTF25-190	5366319.7	476258.2	318.1	24.4	0	-90	24	26	3/8/2025	3/8/2025	0.00	23.50	23.50	0.21
HTF25-191	5366314.9	476300.3	318.0	27.45	0	-90	27	31	3/8/2025	3/8/2025	0.00	23.30	23.30	0.24
HTF25-192	5366272.2	476304.2	318.3	30.5	0	-90	31	34	3/9/2025	3/9/2025	0.00	23.85	23.85	0.27
HTF25-193	5366220.8	476308.8	318.9	27.45	0	-90	26	29	3/9/2025	3/9/2025	0.00	24.80	24.80	0.29
HTF25-194	5366170.5	476309.4	319.5	27.45	0	-90	26	30	3/9/2025	3/9/2025	0.00	26.20	26.20	0.32
HTF25-195	5366514.2	476159.5	317.6	27.45	0	-90	28	31	3/8/2025	3/8/2025	0.00	25.30	25.30	0.45
including											7.00	9.15	2.15	0.65
including											11.00	22.85	11.85	0.63
HTF25-196	5366515.4	475954.3	319.0	28.9	0	-90	26	28	3/10/2025	3/10/2025	0.00	28.10	28.10	0.29
HTF25-197	5366416.7	476055.4	319.0	30.5	0	-90	29	32	3/10/2025	3/10/2025	0.00	26.70	26.70	0.31
HTF25-198	5366171.1	476263.1	319.8	30.5	0	-90	32	35	3/9/2025	3/9/2025	0.00	26.90	26.90	0.32

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-199	5366166.2	476365.6	319.0	27.45	0	-90	23	26	3/9/2025	3/9/2025	0.00	25.15	25.15	0.33
HTF25-200	5366216.2	476363.1	318.5	27.45	0	-90	26	29	3/10/2025	3/10/2025	0.00	24.40	24.40	0.27
HTF25-201	5366266.5	476360.9	318.1	30.5	0	-90	30	33	3/10/2025	3/10/2025	0.00	23.35	23.35	0.24
HTF25-202	5366318.3	476357.4	317.7	32	0	-90	32	36	3/10/2025	3/10/2025	0.00	23.50	23.50	0.22
HTF25-203	5366167.3	476409.3	319.0	27.45	0	-90	25	28	3/11/2025	3/11/2025	0.00	25.00	25.00	0.28
HTF25-204	5366219.2	476405.3	318.3	30.5	0	-90	29	30	3/11/2025	3/11/2025	0.00	23.60	23.60	0.29
HTF25-205	5366264.5	476406.1	318.1	24.4	0	-90	21	23	3/11/2025	3/11/2025	0.00	22.35	22.35	0.25
HTF25-206	5366316.7	476408.4	317.9	24.4	0	-90	22	24	3/10/2025	3/10/2025	0.00	22.85	22.85	0.21
HTF25-207	5366118.2	476454.9	319.5	28.95	0	-90	28	31	3/10/2025	3/10/2025	0.00	25.50	25.50	0.34
HTF25-208	5366166.6	476459.3	319.0	30.5	0	-90	30	33	3/10/2025	3/10/2025	0.00	25.60	25.60	0.30
HTF25-209	5366219.6	476454.6	318.4	27.45	0	-90	26	28	3/11/2025	3/11/2025	0.00	23.40	23.40	0.24
HTF25-210	5366264.1	476454.5	318.2	28.95	0	-90	29	32	3/11/2025	3/11/2025	0.00	23.45	23.45	0.23
HTF25-211	5366316.9	476456.4	318.1	25.9	0	-90	22	24	3/11/2025	3/11/2025	0.45	23.10	22.65	0.20
HTF25-212	5366365.8	476458.3	317.8	27.45	0	-90	26	28	3/12/2025	3/12/2025	0.40	22.50	22.10	0.21
HTF25-213	5366415.4	476455.5	317.8	25.5	0	-90	23	27	3/12/2025	3/12/2025	0.00	24.40	24.40	0.22
HTF25-214	5366478.9	476460.9	317.9	25.55	0	-90	26	29	3/12/2025	3/12/2025	0.00	22.10	22.10	0.27
HTF25-215	5366510.6	476460.5	318.4	24.4	0	-90	25	28	3/12/2025	3/12/2025	0.00	23.70	23.70	0.70
HTF25-216	5366118.6	476514.2	319.5	27.45	0	-90	27	30	3/12/2025	3/12/2025	0.00	23.55	23.55	0.32
HTF25-217	5366174	476513.0	319.2	28.95	0	-90	28	31	3/12/2025	3/12/2025	0.00	23.60	23.60	0.30
HTF25-218	5366214.7	476506.4	318.6	27.45	0	-90	28	30	3/12/2025	3/12/2025	0.00	22.30	22.30	0.26
HTF25-219	5366264.1	476507.9	318.2	27.45	0	-90	29	32	3/12/2025	3/12/2025	0.00	23.50	23.50	0.21
HTF25-220	5366317.6	476496.4	318.2	27.45	0	-90	26	29	3/13/2025	3/13/2025	0.00	22.40	22.40	0.21
HTF25-221	5366368.3	476503.2	318.3	25.9	0	-90	21	24	3/13/2025	3/13/2025	0.00	22.85	22.85	0.22
HTF25-222	5366416.5	476505.9	318.5	24.4	0	-90	22	25	3/13/2025	3/13/2025	0.00	22.50	22.50	0.20
HTF25-223	5366467.8	476507.7	318.3	27.45	0	-90	26	29	3/13/2025	3/13/2025	0.00	21.90	21.90	0.23
HTF25-224	5366516.2	476509.7	319.5	27.45	0	-90	23	26	3/12/2025	3/12/2025	0.00	23.45	23.45	0.56

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
including											3.00	6.00	3.00	0.58
including											9.50	21.35	11.85	0.63
HTF25-225	5366526.2	476409.9	318.4	27.45	0	-90	27	30	3/14/2025	3/14/2025	0.00	25.35	25.35	0.54
including											0.00	3.05	3.05	0.53
including											11.00	24.40	13.40	0.64
HTF25-226	5366529.8	476359.9	318.2	27.1	0	-90	26	30	3/14/2025	3/14/2025	0.00	26.40	26.40	0.52
including											11.00	25.00	14.00	0.61
HTF25-227	5366532.8	476309.4	318.4	27.45	0	-90	26	29	3/13/2025	3/13/2025	0.00	23.60	23.60	0.52
including											0.00	4.00	4.00	0.62
including											9.60	21.35	11.75	0.60
HTF25-228	5366535.2	476260.7	318.4	27.45	0	-90	26	30	3/14/2025	3/14/2025	0.00	23.30	23.30	0.43
including											3.40	6.10	2.70	0.50
including											11.00	23.30	12.30	0.53
HTF25-229	5366541.4	476205.6	318.4	27.45	0	-90	26	30	3/13/2025	3/13/2025	0.00	23.75	23.75	0.54
HTF25-230	5366620.7	476158.2	317.7	27.45	0	-90	27	30	3/14/2025	3/14/2025	0.00	23.25	23.25	0.48
including											0.00	2.00	2.00	0.59
including											5.50	14.30	8.80	0.54
including											20.00	22.00	2.00	0.52
HTF25-231	5366568.5	476502.5	317.8	27.45	0	-90	24	27	3/13/2025	3/13/2025	0.00	25.90	25.90	0.45
including											9.15	13.20	4.05	0.54
including											17.30	22.85	5.55	0.60
HTF25-232	5366523.1	476556.7	318.7	25.9	0	-90	26	29	3/13/2025	3/13/2025	0.00	23.90	23.90	0.52
including											0.00	3.05	3.05	0.65
including											10.65	23.00	12.35	0.55
HTF25-233	5366513	476673.2	319.8	24.4	0	-90	25	28	3/15/2025	3/15/2025	0.00	21.90	21.90	0.53
including											0.00	3.05	3.05	0.51

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
including											8.10	12.20	4.10	0.56
including											14.50	21.90	7.40	0.59
HTF25-234	5366518.4	476708.4	319.1	24.4	0	-90	24	27	3/16/2025	3/16/2025	0.00	22.45	22.45	0.53
including											0.00	5.60	5.60	0.53
including											11.80	22.45	10.65	0.61
HTF25-235	5366515	476757.4	318.6	24.4	0	-90	26	29	3/15/2025	3/15/2025	0.00	22.85	22.85	0.41
including											13.70	18.70	5.00	0.64
HTF25-236	5366607.4	476714.5	318.4	24.4	0	-90	20	22	3/25/2025	3/25/2025	0.70	22.00	21.30	0.36
HTF25-237	5366523.3	476608.0	319.1	21.35	0	-90	18	20	4/6/2025	4/6/2025	0.00	20.55	20.55	0.49
HTF25-238	5366474.6	476562.7	318.9	27.45	0	-90	23	25	3/14/2025	3/14/2025	0.00	22.85	22.85	0.32
including											18.70	22.85	4.15	0.66
HTF25-239	5366410.7	476568.5	318.8	25.9	0	-90	25	28	3/14/2025	3/14/2025	0.00	23.60	23.60	0.29
HTF25-240	5366369.1	476564.3	318.6	27.45	0	-90	25	27	3/14/2025	3/14/2025	0.00	24.40	24.40	0.28
HTF25-241	5366318.2	476558.7	318.4	27.45	0	-90	26	29	3/14/2025	3/14/2025	0.00	22.50	22.50	0.28
HTF25-242	5366613	476759.3	318.1	21.35	0	-90	20	22	3/25/2025	3/25/2025	0.00	20.15	20.15	0.42
including											15.25	16.75	1.50	0.70
HTF25-243	5366268.4	476566.7	318.6	27.45	0	-90	29	33	3/15/2025	3/15/2025	0.00	23.00	23.00	0.27
HTF25-244	5366216.8	476566.1	319.0	27.45	0	-90	27	30	3/15/2025	3/15/2025	0.00	22.00	22.00	0.26
HTF25-245	5366164.8	476555.8	319.3	27.45	0	-90	27	29	3/15/2025	3/15/2025	0.00	22.65	22.65	0.27
HTF25-246	5366120.1	476561.5	319.6	27.45	0	-90	28	31	3/15/2025	3/15/2025	0.00	23.75	23.75	0.31
HTF25-247	5366565.1	476212.2	317.4	27.45	0	-90	28	31	3/15/2025	3/15/2025	0.00	23.10	23.10	0.41
including											14.00	21.35	7.35	0.52
HTF25-248	5366569	476255.8	317.4	27.45	0	-90	25	28	3/15/2025	3/15/2025	1.50	23.25	21.75	0.39
HTF25-249	5366514.8	476805.0	318.4	24.4	0	-90	20	22	3/16/2025	3/16/2025	0.00	19.60	19.60	0.52
including											3.05	4.55	1.50	0.70
including											9.15	18.00	8.85	0.55

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-250	5366515.8	476858.1	318.4	24.4	0	-90	24	24	3/16/2025	3/16/2025	0.00	20.10	20.10	0.53
including											1.00	6.10	5.10	0.56
including											12.00	20.10	8.10	0.56
HTF25-251	5366516.9	476903.2	318.3	24.4	0	-90	24	26	3/16/2025	3/16/2025	0.00	19.30	19.30	0.49
including											0.00	3.05	3.05	0.51
including											9.00	11.10	2.10	0.60
including											13.00	19.30	6.30	0.53
HTF25-252	5366516.6	476956.4	318.1	24.1	0	-90	22	25	3/17/2025	3/17/2025	0.65	19.30	18.65	0.51
including											0.65	2.60	1.95	0.65
including											9.00	12.00	3.00	0.57
including											14.00	19.30	5.30	0.57
and											21.35	22.85	1.50	0.32
HTF25-253	5366520.2	477007.9	318.0	24.4	0	-90	23	25	3/17/2025	3/17/2025	0.00	19.50	19.50	0.51
including											9.65	19.50	9.85	0.57
HTF25-254	5366571.7	476807.1	318.1	21.35	0	-90	19	21	3/26/2025	3/26/2025	0.55	20.65	20.10	0.40
HTF25-255	5366173.5	476966.5	319.3	24.4	0	-90	21	23	3/24/2025	3/24/2025	0.00	20.20	20.20	0.34
HTF25-256	5366116.3	476613.9	319.6	27.45	0	-90	23	25	3/16/2025	3/16/2025	0.00	23.50	23.50	0.33
HTF25-257	5366166.8	476606.7	319.4	27.45	0	-90	25	28	3/16/2025	3/16/2025	0.00	23.30	23.30	0.29
HTF25-258	5366220.8	476609.7	319.5	27.45	0	-90	27	30	3/16/2025	3/16/2025	0.00	23.40	23.40	0.32
HTF25-259	5366260.5	476595.1	318.9	27.45	0	-90	26	29	3/16/2025	3/16/2025	0.00	26.40	26.40	0.31
including											24.40	26.40	2.00	0.53
HTF25-260	5366315.1	476595.6	318.8	27.45	0	-90	27	30	3/17/2025	3/17/2025	0.00	22.20	22.20	0.35
HTF25-261	5366370.7	476594.5	318.9	27.2	0	-90	24	25	3/17/2025	3/17/2025	0.00	24.70	24.70	0.29
HTF25-262	5366413.2	476596.3	319.0	27.45	0	-90	28	31	3/17/2025	3/17/2025	0.00	23.30	23.30	0.28
HTF25-263	5366467.5	476600.2	319.1	25.5	0	-90	25	28	3/17/2025	3/17/2025	0.00	23.95	23.95	0.30
including											21.35	23.95	2.60	0.60

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-264	5366519.6	477057.3	317.9	21.35	0	-90	19	21	3/17/2025	3/17/2025	0.00	17.25	17.25	0.50
including											7.00	9.65	2.65	0.50
including											10.65	17.25	6.60	0.55
HTF25-265	5366518.7	477108.4	318.1	21.35	0	-90	18	20	3/18/2025	3/18/2025	0.00	16.20	16.20	0.56
including											1.00	3.45	2.45	0.51
including											7.60	16.20	8.60	0.65
HTF25-266	5366471.7	476809.0	318.3	24.4	0	-90	19	21	3/17/2025	3/17/2025	1.00	20.25	19.25	0.24
HTF25-267	5366470.1	476763.3	318.6	24.4	0	-90	24	28	3/17/2025	3/17/2025	0.00	22.95	22.95	0.33
including											0.00	3.75	3.75	0.59
including											17.75	19.15	1.40	0.78
HTF25-268	5366116.7	476659.1	320.1	27.45	0	-90	28	31	3/17/2025	3/17/2025	0.00	24.40	24.40	0.39
including											14.00	17.00	3.00	0.58
HTF25-269	5366167.1	476658.9	319.9	27.45	0	-90	30	33	3/18/2025	3/18/2025	0.00	23.40	23.40	0.39
HTF25-270	5366218.8	476659.5	319.7	27.45	0	-90	23	25	3/18/2025	3/18/2025	0.00	23.35	23.35	0.41
including											15.00	17.00	2.00	0.56
HTF25-271	5366269.1	476656.1	319.5	25.9	0	-90	24	27	3/18/2025	3/18/2025	0.00	22.20	22.20	0.43
including											0.00	2.00	2.00	0.61
including											14.00	19.00	5.00	0.52
HTF25-272	5366316.7	476658.6	319.7	27.45	0	-90	28	30	3/18/2025	3/18/2025	0.00	25.00	25.00	0.44
including											0.00	2.00	2.00	0.57
including											18.00	21.00	3.00	0.62
HTF25-273	5366372	476658.6	319.6	27.45	0	-90	24	27	3/18/2025	3/18/2025	0.00	23.25	23.25	0.39
including											13.70	17.00	3.30	0.54
HTF25-274	5366418.3	476662.1	319.5	27.45	0	-90	29	32	3/18/2025	3/18/2025	0.00	22.30	22.30	0.37
including											0.00	2.00	2.00	0.53
HTF25-275	5366463.7	476656.8	319.5	25.9	0	-90	22	24	3/18/2025	3/18/2025	0.30	22.45	22.15	0.34

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
including											20.00	22.45	2.45	0.60
HTF25-276	5366116.6	476702.4	320.1	27.2	0	-90	26	29	3/19/2025	3/19/2025	0.00	23.90	23.90	0.30
HTF25-277	5366164.4	476704.5	319.9	25.9	0	-90	23	25	3/19/2025	3/19/2025	0.00	23.55	23.55	0.34
HTF25-278	5366218.3	476707.8	319.6	24.4	0	-90	21	23	3/19/2025	3/19/2025	0.00	23.20	23.20	0.28
HTF25-279	5366268.1	476708.1	319.5	25.9	0	-90	20	23	3/19/2025	3/19/2025	0.00	25.90	25.90	0.29
HTF25-280	5366318.6	476704.8	319.5	27.45	0	-90	25	28	3/20/2025	3/20/2025	0.00	22.55	22.55	0.32
including											0.00	2.60	2.60	0.54
HTF25-281	5366367.3	476713.2	319.3	25.9	0	-90	25	27	3/20/2025	3/20/2025	0.00	21.10	21.10	0.30
including											0.00	3.05	3.05	0.58
HTF25-282	5366419.1	476709.6	319.3	27.45	0	-90	25	27	3/19/2025	3/19/2025	0.00	25.90	25.90	0.29
including											0.00	2.30	2.30	0.50
HTF25-283	5366470.3	476706.9	319.0	24.4	0	-90	22	25	3/19/2025	3/19/2025	0.45	20.30	19.85	0.32
including											0.45	3.50	3.05	0.59
HTF25-284	5366116.3	476759.7	319.7	27.45	0	-90	25	28	3/21/2025	3/21/2025	0.00	23.25	23.25	0.36
HTF25-285	5366167.9	476763.3	319.4	27.45	0	-90	23	26	3/20/2025	3/20/2025	0.00	20.80	20.80	0.30
HTF25-286	5366215.7	476762.1	319.2	25.9	0	-90	20	23	3/20/2025	3/20/2025	0.00	23.45	23.45	0.28
HTF25-287	5366269.1	476761.8	319.1	25.9	0	-90	25	26	3/20/2025	3/20/2025	0.00	21.80	21.80	0.26
HTF25-288	5366319.9	476760.9	319.1	27.45	0	-90	28	30	3/20/2025	3/20/2025	0.00	20.55	20.55	0.37
including											0.00	8.00	8.00	0.55
HTF25-289	5366369.6	476761.6	319.1	27.45	0	-90	22	25	3/19/2025	3/19/2025	0.00	22.40	22.40	0.27
including											1.20	3.05	1.85	0.69
HTF25-290	5366420.3	476762.2	319.0	25.55	0	-90	24	27	3/19/2025	3/19/2025	0.00	21.35	21.35	0.25
HTF25-291	5366119	476807.7	319.8	25.9	0	-90	19	22	3/20/2025	3/20/2025	0.00	20.50	20.50	0.32
HTF25-292	5366168.1	476808.3	319.2	24.4	0	-90	23	27	3/20/2025	3/20/2025	0.00	19.95	19.95	0.35
HTF25-293	5366218	476811.7	318.9	24.4	0	-90	22	24	3/21/2025	3/21/2025	0.00	20.40	20.40	0.28
HTF25-294	5366268.6	476812.3	318.7	25.9	0	-90	24	27	3/21/2025	3/21/2025	0.50	20.95	20.45	0.26

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-295	5366367.8	476808.2	318.6	24.4	0	-90	22	24	3/21/2025	3/21/2025	0.00	22.10	22.10	0.25
HTF25-296	5366415.9	476805.5	318.5	24.4	0	-90	22	25	3/21/2025	3/21/2025	0.00	22.40	22.40	0.28
including											0.00	1.85	1.85	0.64
HTF25-297	5366120.9	476855.7	319.7	24.4	0	-90	25	26	3/22/2025	3/22/2025	0.00	20.65	20.65	0.40
including											12.50	15.25	2.75	0.50
HTF25-298	5366171.2	476859.5	319.0	24.4	0	-90	21	23	3/21/2025	3/21/2025	0.00	20.80	20.80	0.31
HTF25-299	5366218.3	476853.3	318.9	24.4	0	-90	21	24	3/21/2025	3/21/2025	0.00	20.25	20.25	0.26
HTF25-300	5366265.6	476853.5	318.4	24.4	0	-90	21	23	3/21/2025	3/21/2025	0.00	19.45	19.45	0.25
HTF25-301	5366317.1	476854.2	318.3	24.4	0	-90	22	24	3/22/2025	3/22/2025	0.00	19.20	19.20	0.27
HTF25-302	5366363.4	476853.6	318.2	24.4	0	-90	18	19	3/22/2025	3/22/2025	0.50	21.65	21.15	0.29
including											18.30	19.80	1.50	0.60
HTF25-303	5366424	476853.8	318.0	24.4	0	-90	20	23	3/22/2025	3/22/2025	0.00	19.35	19.35	0.27
HTF25-304	5366469.8	476856.7	317.7	21.35	0	-90	17	18	3/22/2025	3/22/2025	0.00	17.70	17.70	0.20
HTF25-305	5366124.1	476906.3	319.9	24.4	0	-90	20	22	3/22/2025	3/22/2025	0.00	21.60	21.60	0.37
HTF25-306	5366165.8	476907.1	319.2	24.4	0	-90	18	20	3/22/2025	3/22/2025	0.50	19.80	19.30	0.36
HTF25-307	5366221.1	476908.5	318.6	24.4	0	-90	21	22	3/22/2025	3/22/2025	0.65	19.80	19.15	0.30
HTF25-308	5366267	476907.4	318.4	24.4	0	-90	23	25	3/22/2025	3/22/2025	0.85	19.80	18.95	0.27
HTF25-309	5366315.9	476904.6	317.9	24.4	0	-90	22	25	3/23/2025	3/23/2025	0.00	19.30	19.30	0.23
and											21.35	21.90	0.55	0.39
HTF25-310	5366367.5	476906.1	317.4	21.35	0	-90	17	19	3/24/2025	3/24/2025	0.50	20.25	19.75	0.26
HTF25-311	5366126.6	476957.2	320.3	27.45	0	-90	18	20	3/23/2025	3/23/2025	0.00	22.50	22.50	0.27
HTF25-312	5366217.1	476956.7	318.7	24.4	0	-90	23	25	3/23/2025	3/23/2025	0.00	19.30	19.30	0.33
HTF25-313	5366267.1	476957.7	318.4	24.4	0	-90	21	24	3/23/2025	3/23/2025	0.75	23.50	22.75	0.29
HTF25-314	5366319.2	476956.8	317.9	24.4	0	-90	22	25	3/23/2025	3/23/2025	0.00	19.25	19.25	0.26
HTF25-315	5366362.9	476955.4	317.3	24.4	0	-90	21	23	3/24/2025	3/24/2025	0.00	22.00	22.00	0.28
HTF25-316	5366130.3	477008.8	320.3	44.25	0	-90	38	42	3/23/2025	3/23/2025	0.00	20.20	20.20	0.41

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-317	5366166.3	477006.5	319.4	24.4	0	-90	20	22	3/23/2025	3/23/2025	0.00	22.10	22.10	0.33
HTF25-318	5366218.8	477007.6	318.8	24.4	0	-90	22	25	3/24/2025	3/24/2025	0.80	20.30	19.50	0.31
HTF25-319	5366268.1	477008.3	318.5	18.3	0	-90	18	19	3/24/2025	3/24/2025	0.00	17.45	17.45	0.26
HTF25-320	5366312.4	476999.3	318.1	24.4	0	-90	20	22	3/24/2025	3/24/2025	0.60	19.80	19.20	0.25
HTF25-321	5366170.3	477059.0	319.5	24.4	0	-90	18	20	3/23/2025	3/23/2025	0.60	18.00	17.40	0.38
including											1.90	3.40	1.50	0.64
HTF25-322	5366223.6	477063.2	318.9	24.4	0	-90	22	25	3/24/2025	3/24/2025	0.00	18.75	18.75	0.29
HTF25-323	5366270.9	477062.9	318.7	18.3	0	-90	19	21	3/24/2025	3/24/2025	0.00	17.40	17.40	0.28
HTF25-324	5366318.5	477064.9	318.1	21.35	0	-90	17	19	3/24/2025	3/24/2025	0.35	17.55	17.20	0.28
HTF25-325	5366369.4	477072.8	317.5	21.35	0	-90	19	21	3/24/2025	3/24/2025	0.00	16.25	16.25	0.29
HTF25-326	5366165	477106.0	319.6	24.4	0	-90	21	24	3/25/2025	3/25/2025	0.00	19.45	19.45	0.38
HTF25-327	5366216.8	477100.6	319.0	22.85	0	-90	18	20	3/25/2025	3/25/2025	0.00	18.10	18.10	0.36
HTF25-328	5366265.6	477108.8	318.7	21.35	0	-90	21	23	3/25/2025	3/25/2025	0.00	17.90	17.90	0.31
including											0.00	2.00	2.00	0.56
HTF25-329	5366318.6	477110.1	318.2	21.35	0	-90	20	23	3/25/2025	3/25/2025	0.70	17.40	16.70	0.27
HTF25-330	5366365.3	477108.0	317.8	21.35	0	-90	20	22	3/25/2025	3/25/2025	0.60	17.60	17.00	0.24
HTF25-331	5366166	477157.1	319.6	21.35	0	-90	21	24	3/27/2025	3/27/2025	0.00	18.75	18.75	0.39
including											3.50	6.70	3.20	0.56
HTF25-332	5366213.1	477157.6	319.1	21.35	0	-90	21	24	3/28/2025	3/28/2025	0.00	17.55	17.55	0.33
HTF25-333	5366265	477161.1	318.7	38.1	0	-90	22	25	3/29/2025	3/29/2025	0.45	17.30	16.85	0.31
HTF25-334	5366318.9	477155.5	318.2	21.35	0	-90	20	23	3/28/2025	3/28/2025	0.00	16.50	16.50	0.30
HTF25-335	5366364.4	477162.3	317.7	21.35	0	-90	18	20	3/28/2025	3/28/2025	0.00	19.80	19.80	0.20
HTF25-336	5366416	477158.6	316.8	21.35	0	-90	17	19	3/28/2025	3/28/2025	0.00	19.80	19.80	0.22
HTF25-337	5366165.8	477208.9	319.6	21.35	0	-90	16	18	3/29/2025	3/29/2025	0.00	17.15	17.15	0.35
HTF25-338	5366217.2	477208.0	318.9	21.35	0	-90	19	21	3/29/2025	3/29/2025	0.00	19.10	19.10	0.32
including											0.00	1.50	1.50	0.82

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-339	5366263.2	477211.2	318.6	18.3	0	-90	17	19	3/29/2025	3/29/2025	0.00	15.65	15.65	0.32
HTF25-340	5366320	477209.7	318.1	18.3	0	-90	20	22	3/30/2025	3/30/2025	0.00	17.85	17.85	0.32
HTF25-341	5366568.8	476661.0	319.3	24.4	0	-90	22	25	3/26/2025	3/26/2025	0.00	22.00	22.00	0.45
including											18.00	22.00	4.00	0.53
HTF25-342	5366567.7	476709.0	318.7	27.45	0	-90	22	24	3/24/2025	3/24/2025	0.00	20.30	20.30	0.43
HTF25-343	5366564.4	476609.2	318.7	25.9	0	-90	24	28	3/26/2025	3/26/2025	0.00	21.35	21.35	0.42
including											10.00	12.20	2.20	0.55
HTF25-344	5366614.5	476609.2	318.8	25.9	0	-90	24	27	3/26/2025	3/26/2025	0.00	22.00	22.00	0.38
HTF25-345	5366623.3	476660.0	320.0	24.4	0	-90	23	26	3/26/2025	3/26/2025	0.00	23.45	23.45	0.52
including											0.00	2.00	2.00	0.66
including											14.90	23.45	8.55	0.57
HTF25-346	5366614.2	476809.1	317.7	21.35	0	-90	17	19	3/27/2025	3/27/2025	0.55	20.10	19.55	0.34
HTF25-347	5366620.2	476859.7	317.4	24.4	0	-90	21	24	3/27/2025	3/27/2025	0.00	22.35	22.35	0.36
HTF25-348	5366567.5	476857.5	317.4	21.35	0	-90	19	21	3/27/2025	3/27/2025	0.00	20.20	20.20	0.46
including											10.65	17.00	6.35	0.56
HTF25-349	5366561.7	476907.1	316.8	21.35	0	-90	18	19	3/27/2025	3/27/2025	0.00	17.40	17.40	0.46
including											11.00	16.75	5.75	0.56
HTF25-350	5366173.7	477259.1	319.4	39.65	0	-90	22	25	3/30/2025	3/30/2025	0.00	17.55	17.55	0.36
HTF25-351	5366214.4	477255.8	318.9	21.35	0	-90	21	23	3/30/2025	3/30/2025	0.00	16.50	16.50	0.32
HTF25-352	5366262.1	477255.5	318.7	15.25	0	-90	14	16	3/31/2025	3/31/2025	0.00	15.05	15.05	0.29
including											0.00	3.05	3.05	0.52
HTF25-353	5366312.7	477254.0	317.9	18.3	0	-90	20	22	3/31/2025	3/31/2025	0.00	14.60	14.60	0.29
HTF25-354	5366369.7	477257.7	317.4	38.1	0	-90	27	30	3/31/2025	3/31/2025	0.00	14.50	14.50	0.27
HTF25-355	5366405.7	477258.3	317.1	15.25	0	-90	13	15	4/1/2025	4/1/2025	0.70	14.00	13.30	0.20
HTF25-356	5366164.6	477308.5	319.7	18.3	0	-90	14	15	4/1/2025	4/1/2025	0.00	16.75	16.75	0.33
HTF25-357	5366217	477306.8	319.0	19.8	0	-90	23	26	4/1/2025	4/1/2025	0.00	17.25	17.25	0.31

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-358	5366264.6	477305.1	318.5	13.7	0	-90	14	16	4/1/2025	4/1/2025	0.00	13.30	13.30	0.28
HTF25-359	5366316.9	477307.1	318.1	13.7	0	-90	13	14	4/1/2025	4/1/2025	0.00	13.70	13.70	0.29
HTF25-360	5366367.5	477305.8	317.7	19.8	0	-90	19	21	4/1/2025	4/1/2025	0.00	16.75	16.75	0.22
HTF25-361	5366418.6	477304.9	317.4	18.3	0	-90	17	19	4/1/2025	4/1/2025	0.50	12.95	12.45	0.20
HTF25-362	5366462.5	477309.8	317.1	15.25	0	-90	17	19	4/2/2025	4/2/2025	1.50	13.00	11.50	0.21
HTF25-363	5366523.1	477305.2	318.1	12.2	0	-90	14	15	4/2/2025	4/2/2025	0.00	11.75	11.75	0.41
HTF25-364	5366523.6	477259.0	318.1	18.3	0	-90	13	15	4/3/2025	4/3/2025	0.00	12.20	12.20	0.44
including											1.30	4.30	3.00	0.55
HTF25-365	5366516.5	477208.1	318.3	13.7	0	-90	14	15	4/3/2025	4/3/2025	0.00	13.70	13.70	0.51
including											8.00	13.70	5.70	0.63
HTF25-366	5366523	477159.4	318.6	21.35	0	-90	15	16	4/2/2025	4/2/2025	0.00	16.75	16.75	0.47
HTF25-367	5366566.4	477156.3	316.9	18.3	0	-90	17	20	4/2/2025	4/2/2025	1.50	17.00	15.50	0.50
including											7.60	11.00	3.40	0.52
including											13.00	16.00	3.00	0.68
HTF25-368	5366568.1	477207.9	316.9	18.3	0	-90	14	15	4/2/2025	4/2/2025	0.00	13.70	13.70	0.44
including											6.30	9.75	3.45	0.61
HTF25-369	5366561.6	477257.6	317.0	15.25	0	-90	16	18	4/2/2025	4/2/2025	0.00	14.70	14.70	0.36
HTF25-370	5366568	477309.0	317.0	15.25	0	-90	15	17	4/2/2025	4/2/2025	0.00	13.10	13.10	0.35
including											0.00	2.20	2.20	0.65
HTF25-371	5366770.1	476510.7	322.4	33.55	0	-90	22	26	4/10/2025	4/10/2025	3.80	26.10	22.30	0.30
HTF25-372	5366216.8	477355.8	319.2	15.25	0	-90	10	12	4/4/2025	4/4/2025	0.00	12.60	12.60	0.31
HTF25-373	5366263.5	477354.9	318.7	15.25	0	-90	12	13	4/4/2025	4/4/2025	0.00	13.30	13.30	0.30
HTF25-374	5366321.7	477354.9	318.3	12.2	0	-90	11	12	4/3/2025	4/3/2025	0.00	11.80	11.80	0.26
HTF25-375	5366366.9	477359.8	318.1	7.6	0	-90	5	5	4/4/2025	4/4/2025	0.35	6.10	5.75	0.20
HTF25-376	5366416.3	477353.5	317.8	15.25	0	-90	13	14	4/3/2025	4/3/2025	0.40	12.20	11.80	0.26
HTF25-377	5366466.2	477353.8	317.7	15.25	0	-90	15	16	4/3/2025	4/3/2025	0.65	11.40	10.75	0.18

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
HTF25-378	5366523.2	477358.2	318.2	16.75	0	-90	16	18	4/3/2025	4/3/2025	0.50	14.55	14.05	0.37
HTF25-379	5366169.7	477413.6	319.8	15.25	0	-90	14	15	4/5/2025	4/5/2025	0.00	11.20	11.20	0.38
HTF25-380	5366217.5	477411.6	319.3	12.2	0	-90	12	12	4/5/2025	4/5/2025	0.00	11.25	11.25	0.31
HTF25-381	5366267.1	477415.3	319.2	12.2	0	-90	11	12	4/5/2025	4/5/2025	0.00	11.70	11.70	0.31
HTF25-382	5366318.1	477410.3	319.8	12.2	0	-90	12	12	4/4/2025	4/4/2025	0.00	9.15	9.15	0.28
HTF25-383	5366367.3	477409.9	319.9	12.2	0	-90	12	14	4/4/2025	4/4/2025	0.00	8.05	8.05	0.30
HTF25-384	5366421.4	477399.5	320.2	10.65	0	-90	10	11	4/4/2025	4/4/2025	0.00	10.10	10.10	0.27
HTF25-385	5366469.7	477410.8	318.4	12.2	0	-90	10	12	4/4/2025	4/4/2025	0.60	9.15	8.55	0.19
HTF25-386	5366515.7	477408.0	318.7	12.2	0	-90	10	10	4/4/2025	4/4/2025	0.60	8.80	8.20	0.41
HTF25-387	5366268.7	477461.9	319.0	12.2	0	-90	12	14	4/5/2025	4/5/2025	0.00	9.60	9.60	0.24
HTF25-388	5366315.7	477464.2	318.9	12.2	0	-90	11	12	4/5/2025	4/5/2025	0.00	8.20	8.20	0.27
HTF25-389	5366369.7	477457.3	319.8	15.25	0	-90	17	19	4/5/2025	4/5/2025	0.00	9.15	9.15	0.31
HTF25-390	5366417.4	477454.8	319.6	12.2	0	-90	13	14	4/5/2025	4/5/2025	0.00	10.10	10.10	0.25
HTF25-391	5366465.3	477460.3	319.7	12.2	0	-90	10	11	4/6/2025	4/6/2025	0.00	10.00	10.00	0.30
HTF25-392	5366983.4	476608.8	319.0	27.45	0	-90	20	23	4/11/2025	4/11/2025	0.00	20.40	20.40	0.41
including											12.20	18.00	5.80	0.53
HTF25-393	5366917.9	476605.1	323.3	30.5	0	-90	25	27	4/12/2025	4/12/2025	4.55	23.70	19.15	0.38
HTF25-394	5366868.2	476600.6	321.7	27.45	0	-90	21	24	4/11/2025	4/11/2025	5.65	26.50	20.85	0.34
including											15.00	16.75	1.75	0.57
HTF25-395	5366821.2	476603.6	322.9	30.5	0	-90	27	31	4/10/2025	4/10/2025	3.35	25.40	22.05	0.32
HTF25-396	5366769.8	476603.1	322.7	30.5	0	-90	27	31	4/10/2025	4/10/2025	3.70	22.85	19.15	0.27
HTF25-397	5366971.9	476561.1	322.2	30.5	0	-90	29	32	4/7/2025	4/7/2025	0.00	0.70	0.70	8.50
and											2.70	26.10	23.40	0.38
HTF25-398	5366913.4	476558.6	322.8	30.5	0	-90	23	25	4/7/2025	4/7/2025	5.10	24.25	19.15	0.38
and											27.45	30.50	3.05	0.32
HTF25-399	5366862.3	476560.2	322.8	30.5	0	-90	17	19	4/8/2025	4/8/2025	9.15	25.30	16.15	0.36

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
and											27.45	28.95	1.50	0.29
HTF25-400	5366812.8	476567.8	323.3	30.5	0	-90	26	28	4/9/2025	4/9/2025	3.05	25.80	22.75	0.29
HTF25-401	5366762.2	476562.6	322.7	30.5	0	-90	21	24	4/8/2025	4/8/2025	2.55	25.55	23.00	0.27
HTF25-402	5366961.4	476507.6	322.1	27.45	0	-90	25	28	4/7/2025	4/7/2025	3.05	24.40	21.35	0.42
HTF25-403	5366913.4	476509.1	322.2	27.45	0	-90	27	29	4/6/2025	4/6/2025	0.00	26.60	26.60	0.39
HTF25-404	5366865.6	476521.0	322.8	28.95	0	-90	22	25	4/6/2025	4/6/2025	7.00	25.55	18.55	0.33
HTF25-405	5366805.3	476509.6	322.5	30.5	0	-90	25	28	4/9/2025	4/9/2025	4.20	26.75	22.55	0.31
KP25-01	5366565.7	476757.0	318.3	42.65	0	-90	31	33	3/25/2025	3/27/2025	0.00	20.15	20.15	0.56
including											6.00	18.75	12.75	0.65
KP25-02	5366678.9	476383.9	317.9	48.75	0	-90	35	40	3/27/2025	3/29/2025	0.00	22.30	22.30	0.37
KP25-03	5367020.8	476407.9	318.9	27.45	0	-90	22	24	3/29/2025	3/30/2025	0.00	22.20	22.20	0.48
including											9.15	16.25	7.10	0.62
KP25-04	5367035.5	476404.2	320.7	28.95	0	-90	24	28	3/30/2025	3/31/2025	0.00	21.75	21.75	0.57
KP25-05	5366153	477362.2	320.3	48.75	0	-90	34	36	3/31/2025	4/2/2025	0.00	15.60	15.60	0.43
including											12.00	14.50	2.50	0.51
KP25-06	5366159.3	477362.6	320.1	62.5	0	-90	31	36	4/2/2025	4/4/2025	0.00	15.90	15.90	0.42
KP25-07	5366366.9	477209.8	317.6	39.6	0	-90	14	16	4/4/2025	4/5/2025	0.00	14.30	14.30	0.25
KP25-08	5366315.8	476809.5	318.6	33.55	0	-90	25	28	4/5/2025	4/6/2025	0.00	18.30	18.30	0.25
KP25-09	5366128.6	477016.2	320.3	45.75	0	-90	35	39	4/6/2025	4/8/2025	0.00	20.40	20.40	0.40
KP25-10	5366582.2	477591.3	320.9	19.8	0	-90	6	7	4/8/2025	4/9/2025	0.00	3.50	3.50	0.48
KP25-11	5367064.6	477018.2	322.9	18.3	0	-90	13	14	4/9/2025	4/9/2025	1.90	12.10	10.20	0.41
KP25-12	5367011.1	477558.2	320.3	24.4	0	-90	13	14	4/9/2025	4/10/2025	0.00	2.50	2.50	0.63
KP25-13	5366794.4	475780.1	319.2	50.3	0	-90	44	49	4/10/2025	4/12/2025	0.00	23.40	23.40	0.36
and											25.90	28.30	2.40	0.35
KP25-14	5366796.7	475759.4	319.8	51.8	0	-90	43	45	4/12/2025	4/13/2025	0.00	28.35	28.35	0.33
KP25-15	5366533.7	475872.8	319.3	59.45	0	-90	50	56	4/14/2025	4/15/2025	0.00	28.45	28.45	0.32

Hole ID	Northing	Easting	Elevation	Hole Length (m)	Azimuth	Inclination	No of Samples Collected	No of Samples Assayed	Start Date	End Date	From (m)	To (m)	Interval (m)	Au (g/t)
KP25-16	5366552.3	475879.2	319.1	28.95	0	-90	28	31	4/16/2025	4/16/2025	0.00	28.00	28.00	0.31
KP25-17	5366074.5	476471.3	320.3	57.95	0	-90	48	53	4/17/2025	4/18/2025	0.00	24.60	24.60	0.40
including											0.00	3.00	3.00	0.51
KP25-18	5366101.2	476461.0	319.6	25.9	0	-90	27	30	4/18/2025	4/19/2025	0.00	25.25	25.25	0.33

10.2 Core Logging

The core was drilled using a 5-ft core barrel and collected 5-feet of continuous samples into a plastic sleeve. The plastic sleeves were tied off preserving solid and liquid content. At the drill, the sleeves were then placed in 5-foot wooden boxes that were labeled with the drill hole number and box sequence number. The boxes were covered and nailed shut. The boxes were transported daily to STLLR's Timmins core shack to be prepared for logging.

10.2.1 Core Preparation

Prior to logging, the boxes containing the drill core were laid out on the core tables in numerical sequence working from the top of the hole, Box 1, to the bottom of the hole. Once the boxes were laid out in sequence, the lids were removed, and the plastic sleeves were cut open to reveal the tailings. The boxes were marked up and converted to the metric system, which was set at 1.50 m equal to 5 ft. Example core shown in Figure 10.2.

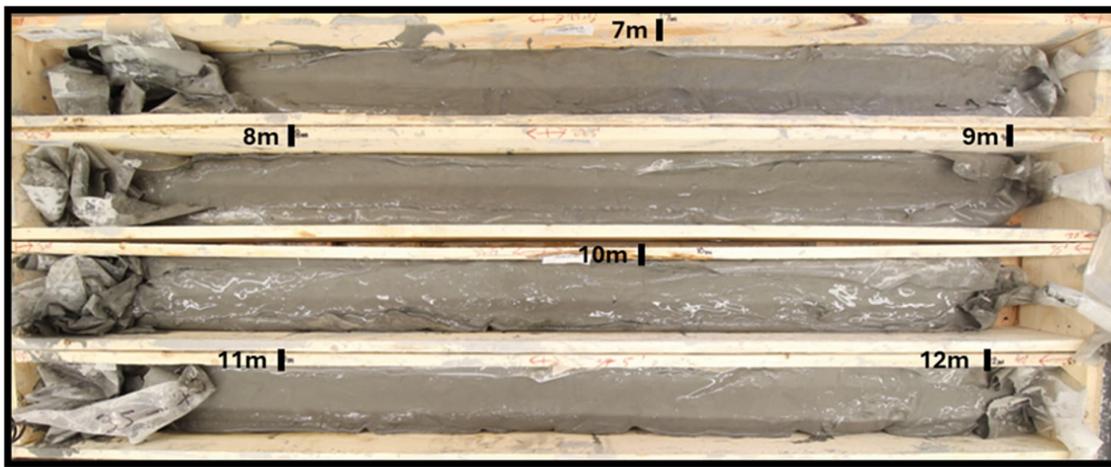


Figure 10.2: Sonic Drill Core Displaying Metre Marks

10.2.2 Core Logging

Core was logged by a STLLR geologist and GeoMinex contract geologists, at the STLLR core shack in the City of Timmins. The logs were entered directly in MX Deposit database software. The core loggers were responsible to identify and record, if present; unit type, grain size, colour, moisture content, grading, description of textures, structures, mineralization, recovery, and contact types.

The logging separated out 15 different Unit Types (Table 10.2), reflecting all materials present within and below the Tailings Facility. The primary units reflected grain size and texture variation within the sedimentary units of the tailings and glacial till. The most observed units were silty-sand, silty-clay, sandy-silt and sand, combined making up 73.2% of the logged material.

Some drill holes were spotted on top of the wood waste landfill and the upper units were classified as, Unknown, a specific distinction from the organic layers which both contained wood pieces.

The Organic Matter unit is an organic layer that was consistently identified in each hole and marked the bottom of the tailings and the contact to the glacial till. The organics consisted primarily of soils and wood debris assumed to be the scrubbed forest floor from the original construction of the dam. However, in some drill holes, tailings were observed below the organic layer for several feet, which is interpreted to be due to voids created from the methods used during construction.

All drilling was completed until first refusal at the contact to bedrock. Several holes periodically drilled into the bedrock to confirm geological mapping and understand foundation lithologies.

Table 10.2: Logged Sediment Types

Unit Type	Description	Frequency (%)
GR	Gravel	0.05
GR-snd/slt	Sandy/silty gravel	0.75
SND	Sand	9.58
SND-gr	Gravelly sand	1.54
SND-slt	Silty sand	24.79
SLT-gr	Gravelly silt	0.78
SLT-snd	Sandy silt	17.09
SLT	Silt	4.03
CL-slt	Silty clay	21.74
CL	Clay	8.54
OM	Organic matter	3.69
SLR	Slurry/poor recovery	4.37
LC	Lost Core	0.36
UNK	Unknown	2.21
BDRCK	Bedrock	0.46

Grain size was recorded; however, the measurement was qualitative, determined by visual and textural observation and varied between loggers. The Grain Size was limited to five options for loggers to characterize (Table 10.3) which merged multiple Unit Types.

Table 10.3: Grain Size and the corresponding Sediment Types

Grain Size	Unit Type
1	Fine grained clay, silty clay, silt
2	Fine to medium grained sandy silt, silty sand
3	Medium grained sand (very fine to fine)
4	Medium to coarse grained sand (medium to coarse)
5	Coarse grained gravel, anything with gravel
NA	Not Applicable

Other commonly recorded items for each Unit Type included Colour, Moisture Content (which ranged from wet, moist and dry), and Grading if present in the sedimentary units including normal and reverse.

If present, both the upper and lower Contacts were recorded and described as either, broken, deformed, gradational, irregular or sharp. No bedding, flame structures, slump structures features were visible in the sonic drill holes.

10.2.3 Mineralization

Mineralization was logged to respect the Unit Type boundaries. The most common sulphide present was pyrite and occurred as fine cubes up to 10% but on average less than 1%. No visible gold was observed. Gold mineralization from assay data showed most of the tailings was consistently mineralized both laterally and vertically throughout the facility (Table 10.4). Higher than average Au grades were observed within the original tailing's disposal area than within the extension tailings cell area. (Table 10.4). Additional observations of gold distribution are described in Item 14.3.2.

The core length per sample was broken on Unit Type rather than mineralization since the entirety of the Tailings Facility is mineralized, and individual layers of tailings deposition were not identifiable by loggers. The tailings were deposited in horizontal sheets with very shallow dips. Vertical (90° to horizontal) drill hole orientation is appropriate to assume core length is equivalent to true thickness and the intercept angle to be perpendicular or 90°. The exception to this is the dam walls. The Phase 1 inward facing wall angle was estimated to be 45° and outside facing at 34°, while Phase 2 both inward and outward facing wall angles are 45°. Vertical (90° to horizontal) drill holes would intercept the inward facing walls at 45° and outward facing walls at 56 degrees. However, the dam walls were constructed by dredging and piling the tailings, which disturbed horizontal layering and blended tailings material. Additional details regarding dam wall designs are in Item 14.3.2.

Because of the narrow range in gold assay values, the significant intercepts are generally calculated using a cut-off grade of 0.20 g/t Au, while including intercepts are calculated using a 0.50 g/t Au cut-off grade. Occasional lower than cut-off grade intervals are also highlighted, when interval lengths are significant enough.

Representative example sections are provided in Figure 10.3 and Figure 10.4.

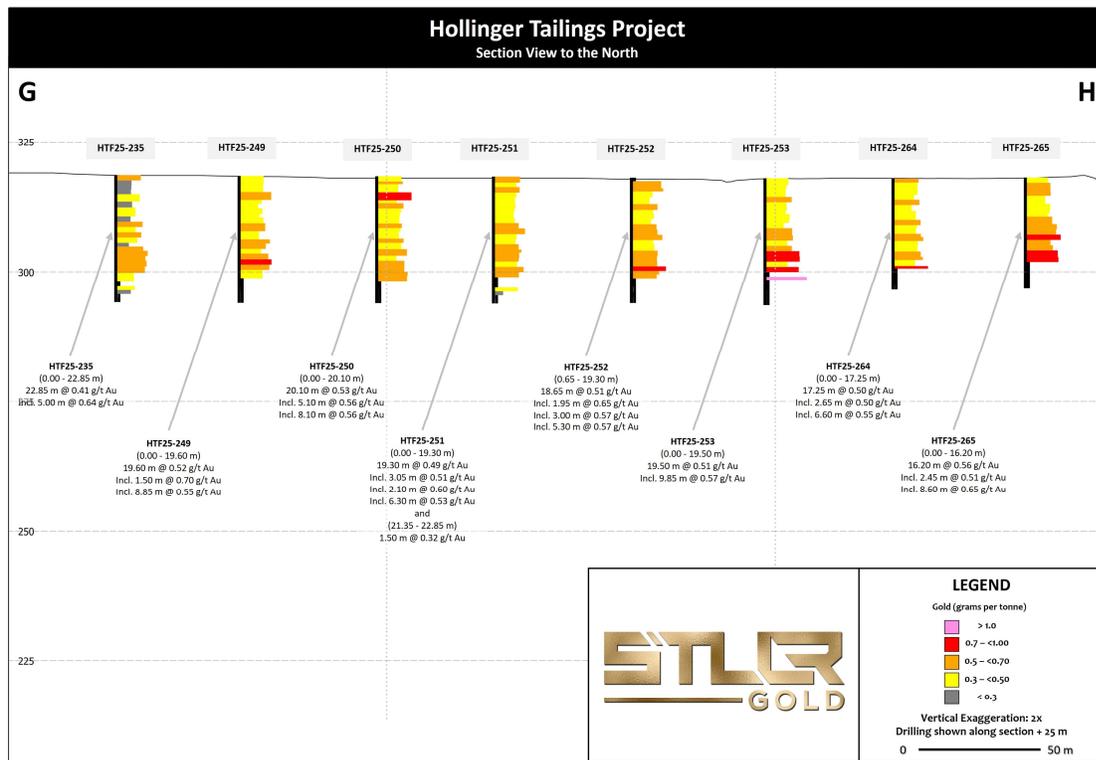
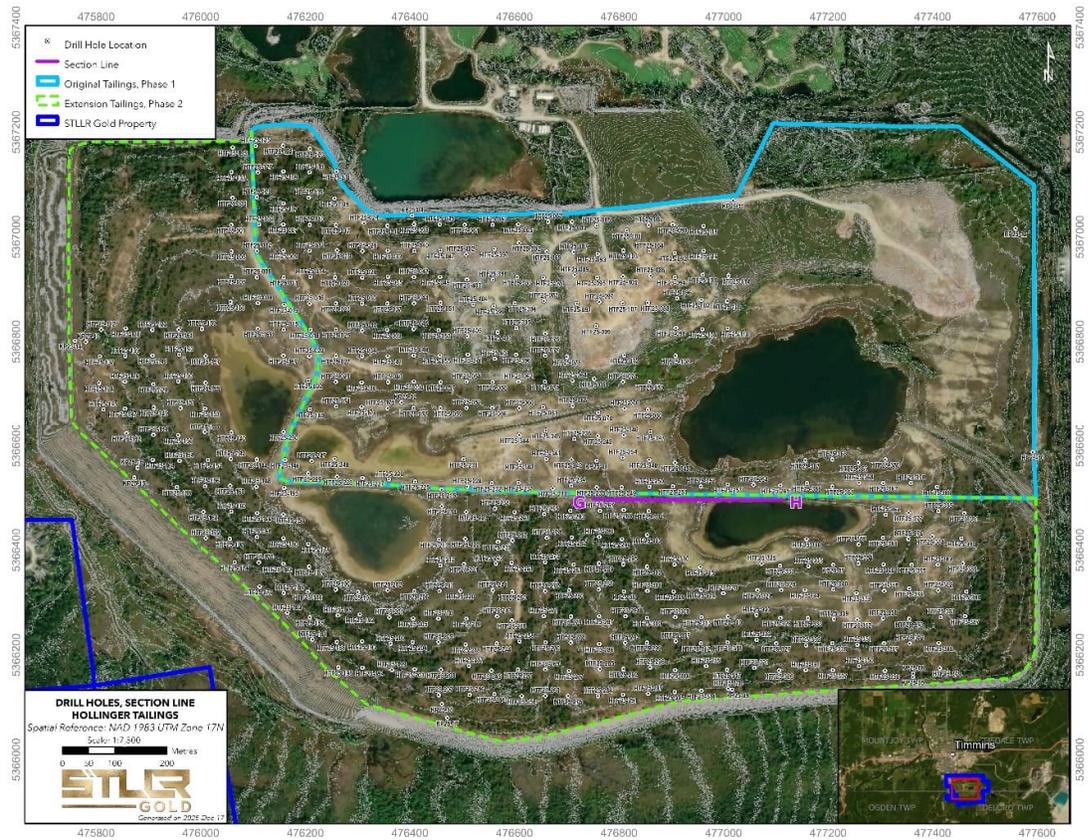


Figure 10.3: Long-Section View Parallel to Phase 1 Wall

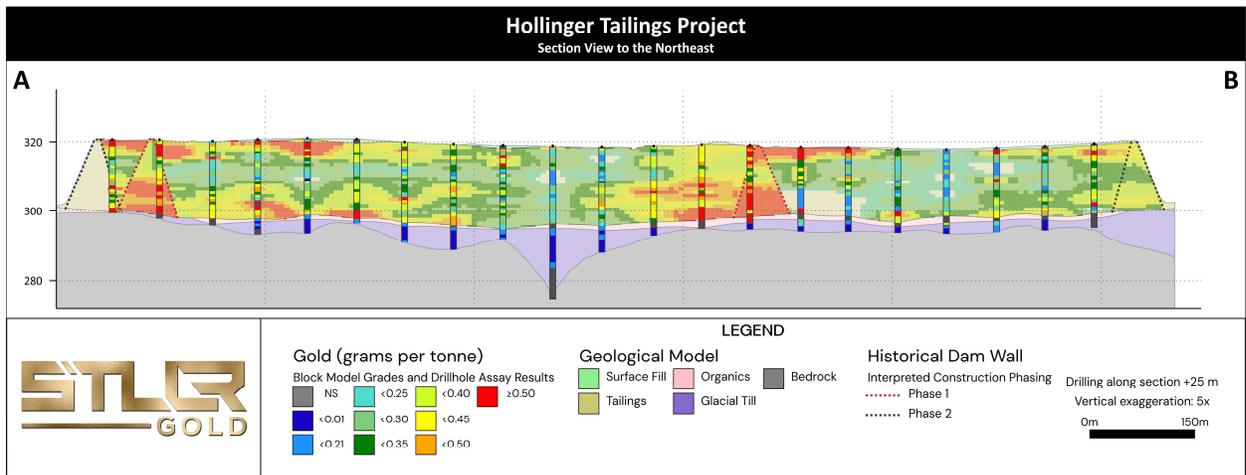
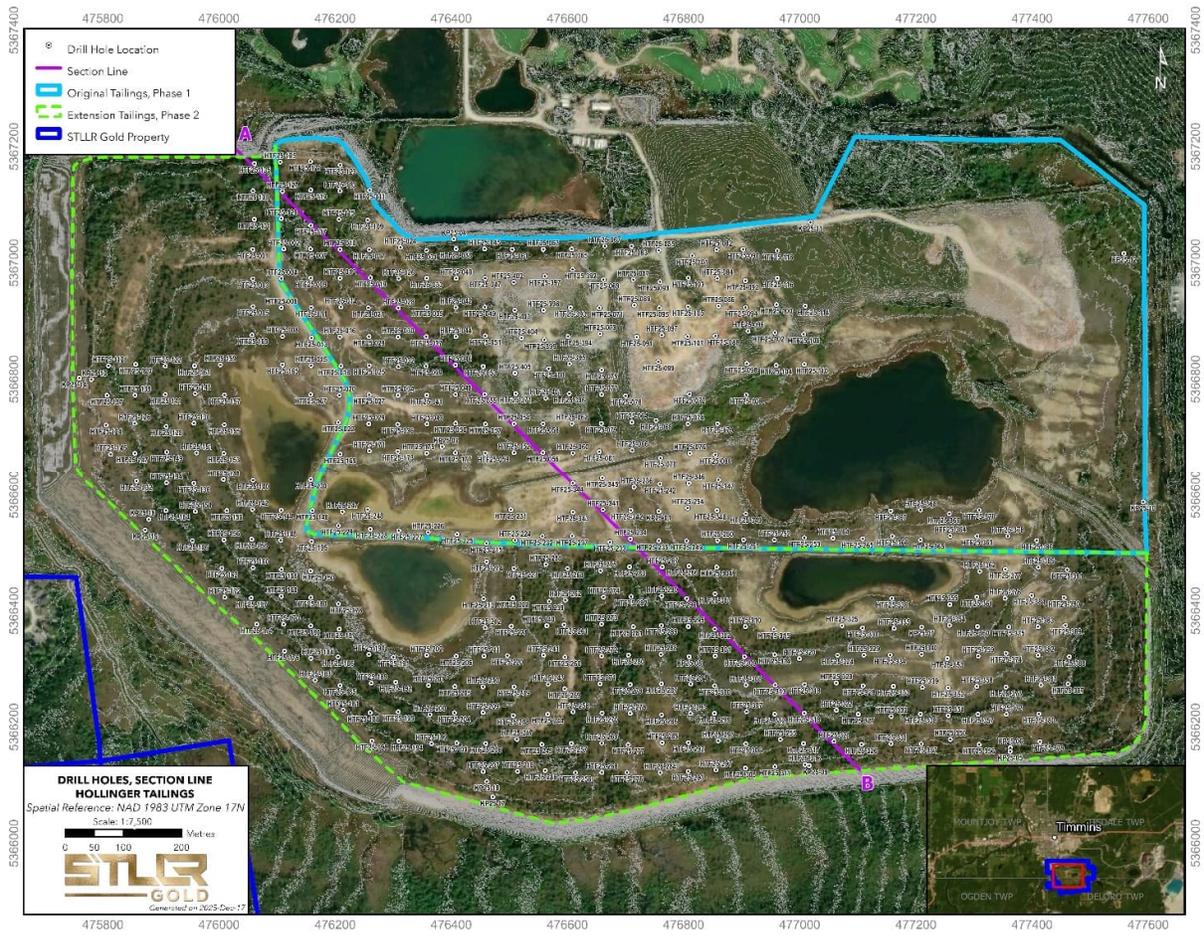


Figure 10.4: Cross-Section View

10.2.4 Downhole Survey

All drill holes were designed with a dip of 90 degrees. 331 downhole surveys for dip and deviation were conducted by the drill company, using a Reflex EZ Shot tool. However, no significant deviation was observed as the average depth of the sonic holes is 26.5 with the deepest hole being, 62.5 m. Holes were assumed to be vertical.

10.2.5 Collar Survey

All collars were surveyed by Surveyors On Site Inc., a third-party surveyor located in New Liskeard, Ontario (Figure 10.5). The survey method was by a precise RTK GPS base Leica GS15 and rover GS14 with a standard baseline error of 8 mm. This translates to 2 cm horizontal and 3 cm vertical error. Field work started by setting up a base station on known control points in a digital job file, logging Precise Point Positioning (PPP) to be processed to verify base position, and checking into a secondary control point to verify under 2 cm horizontal and 3 cm vertical distances. Location readings were then taken on the drill holes. At the end of each survey day, the crew checked in to the same secondary control point which was set at the beginning of the day. The collar survey results in CSV, TXT and PDF formats were then reviewed, officially signed off by their certified surveyor, Robert Wannack, O.L.S., and sent to STLLR Gold database geologists for second level validation prior to MX Deposit import.



Figure 10.5: Hollinger Hole HTF25-193 being Surveyed by Surveyors On Site, Inc.

10.2.5 Recovery

Lost Core unit was used to represent intervals of missing core due to drillers having dropped the core barrel or dropped core at surface. Lost Core only represents 0.36% of all logged units. If a drill run had less than 100% recovery, the Recovery was measured and marked as Slurry with Poor Recovery. Poor recovery due to slurry makes up 4.37% of all logged core. There were no naturally occurring voids within the Tailings Facility.

10.2.6 Photos

After core logging was completed, core photos were taken to capture a record of the core, ensuring that the hole number, box numbers, meterage and sample tags were visible. All photos are stored on the STLLR's secure Egnyte webserver.

10.3 Geotechnical Drilling

KP was retained by STLLR to support a geotechnical data collection program in tandem with the infill drilling program in late winter of 2025. The purpose of the geotechnical data collection program was to confirm tailings and foundation conditions and bedrock depth across the Tailings Facility, collect soil samples for laboratory testing to estimating moisture content, complete in situ testing of the tailings and foundation soils with a focus on estimating in situ density and assess the location of the phreatic surface (water table) within the tailings.

The site investigations for the geotechnical data collection program were carried out between March 24th, and April 22, 2025. The SOW included geotechnical drilling, in situ testing, overburden and bedrock logging, sample collection, and laboratory testing of representative samples. The completed drill hole locations are shown on Figure 10.6. The program included 18 drill holes and 2 monitoring well installations.

Drill holes were generally advanced through the tailings, underlying foundation soils and 3 m into bedrock, for a total combined length of 712 m. The drill rig was equipped with HW casing, an HQ core barrel, a standard automatic hammer for Standard Penetration Testing (SPT), split spoons, and Shelby tubes. Drill holes were advanced vertically (-90° inclination) by advancing casing and sampling via SPTs and Shelby tubes until refusal. HQ coring was completed thereafter into bedrock.

Logging of the overburden was completed on samples from the drill holes and surface samples to characterize the encountered soils. All logging was undertaken in accordance with the Canadian Foundation Engineering Manual (Canada Geotechnical Society, 2006) and the Standard Practice for Description Identification of Soils (ASTM, D2488). Information collected included the following:

- A description of the site conditions
- Recording depths and soil characteristics of split spoon samples from SPTs and recovered drill core including the observed:
 - Particle size and shape
 - Gradation
 - Plasticity
 - Colour
 - Relative density or consistency
 - Structure
 - Moisture condition

■ Geological Interpretation

Representative overburden samples were collected using grab sampling, split spoons and Shelby tubes. The grab samples and split spoon samples were logged, photographed, labelled, and placed in sealed, double bagged plastic bags for transportation to the laboratory.

Basic logging was undertaken on the core recovered from the geotechnical drill holes. The purpose of this logging was to characterize the recovered shallow bedrock (where encountered). The rock mass was logged by drill run and characterized by typical joint parameters. Recovered bedrock drill core was placed in core boxes, labelled, and photographed.

Bedrock core logging included estimation of the key intact rock and discontinuity characteristics. The logging results were used to estimate the rock mass quality of bedrock using the Rock Mass Rating (RMR) system (Bieniawski, 1989). Approximately 40 m of bedrock was recovered and logged from the drill holes.

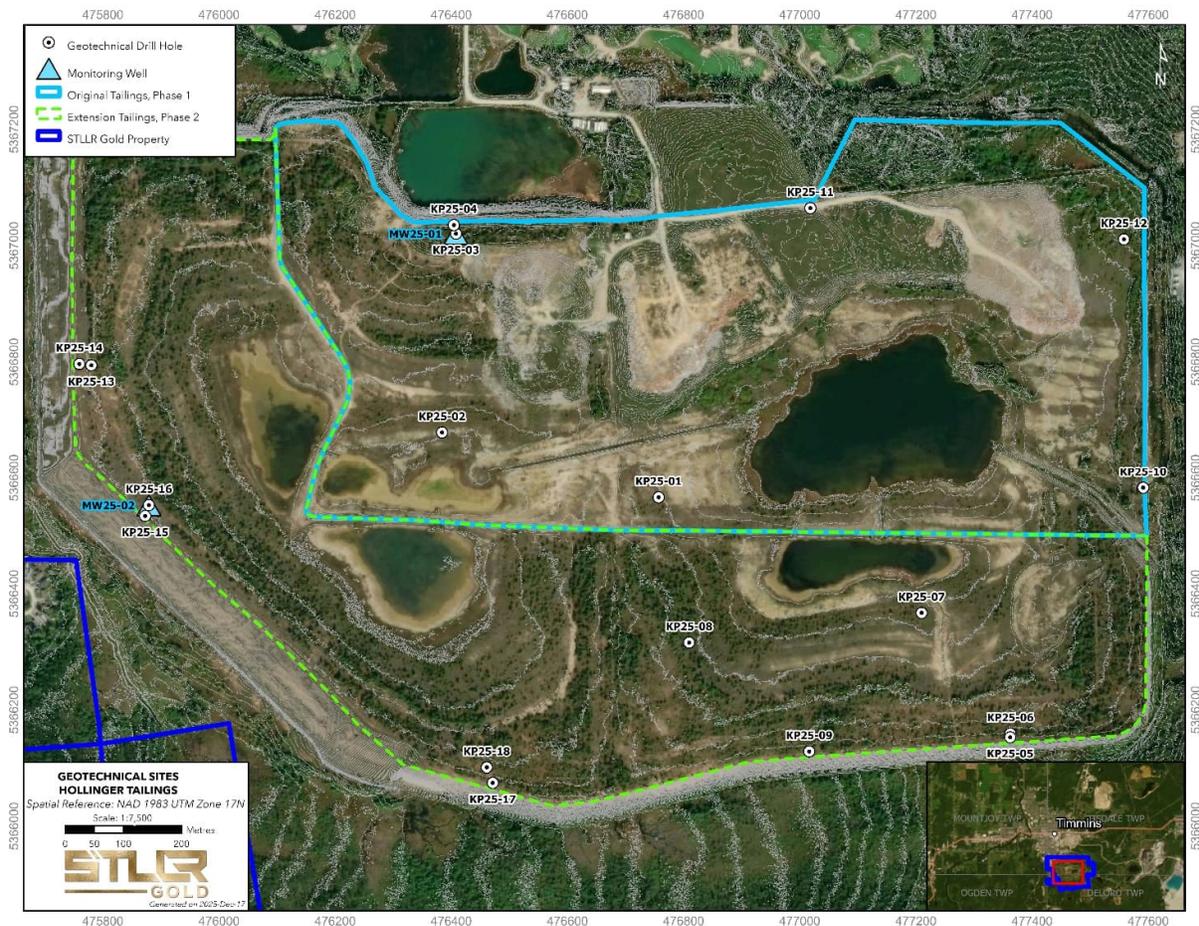


Figure 10.6: Geotechnical Drill Hole Location Hollinger Tailings Project

10.3.1 Bulk Density

In situ bulk density measurement was derived from SPTs and Shelby tube sampling. Representative soil samples were collected prior to the soil being disturbed through drilling process from the overburden surface within the drill hole by SPTs and Shelby tube samples were obtained from the bottom of the open drill hole up to the undisturbed overburden surface to analyzed loose or compact soil bulk density, depending on the stress history of the field, using ASTM D1587 standard. The bulk density measurements of the soil collected in the field considered the total weight of both soil and the water within the sample. A basic soil mechanics phase relationship following formula was used to estimate bulk density and convert it from bulk density to dry density:

$$\text{Dry Density } (\rho_d) = \text{Bulk density } (\rho_b) / [1 + \text{Moisture content } (w)]$$

In this formula, moisture content is expressed as a decimal.

Where:

Dry Density (ρ_d): is the density of the soil without water.

Bulk Density (ρ_b): (or wet density) is the density of the soil including water.

Moisture Content (w): is the amount of water in the soil, expressed as a decimal (e.g., 22% is 0.22).

Table 10.4: Geotechnical Data Collection Shelby Tube Sample Details

Drill Hole ID	Sample ID	Depth From	Depth To	Sample Length	WT Soil	Sample Volume	Bulk Density	Estimated Dry Density
		(m)	(m)	(m)	(kg)	(m ³)	(kg/m ³)	(kg/m ³)
KP25-01	ST-01	1.52	2.27	0.22	1.5	0.0009	1,675	1,298
	ST-03	6.1	6.85	0.527	4.6	0.0021	2,145	1,896
	ST-05	12.19	12.95	0.615	5.25	0.0025	2,098	1,738
KP25-02	ST-01	1.52	2.28	0.605	4.65	0.0025	1,889	1,574
	ST-02	4.57	5.33	0.49	4.1	0.0020	2,056	1,637
	ST-03	9.14	9.9	0.605	4.8	0.0025	1,950	1,625
	ST-04	13.72	14.42	0.6	4.95	0.0024	2,027	1,726
	ST-05	18.28	19.04	0.592	5.1	0.0024	2,117	1,772
	ST-06	25.6	26.36	0.587	4.85	0.0024	2,030	1,674
	ST-08	27.74	28.5	0.556	4.1	0.0023	1,812	1,494
	ST-09	29.26	30.02	0.335	2.75	0.0014	2,017	1,663
	ST-10	30.02	30.78	0.248	2.56	0.0010	2,537	2,091
KP25-03	ST-01	1.52	2.28	0.462	3.95	0.0019	2,101	1,746
	ST-02	4.57	5.33	0.23	2.05	0.0009	2,190	1,820
	ST-03	7.62	8.38	0.38	2.35	0.0015	1,520	1,263
	ST-04	10.66	11.42	0.71	6.39	0.0029	2,212	1,821
	ST-05	12.18	12.94	0.695	6.25	0.0028	2,210	1,820
	ST-06	15.22	15.98	0.645	5.85	0.0026	2,229	1,836
KP25-04	ST-03	19.81	20.57	0.645	6.35	0.0027	2,353	1,961
KP25-05	ST-01	3.48	4.24	0.694	5.1	0.0028	1,806	1,700

Drill Hole ID	Sample ID	Depth From	Depth To	Sample Length	WT Soil	Sample Volume	Bulk Density	Estimated Dry Density
		(m)	(m)	(m)	(kg)	(m ³)	(kg/m ³)	(kg/m ³)
	ST-02	6.09	6.85	0.689	5.35	0.0028	1,908	1,789
	ST-03	9.14	9.9	0.61	4.95	0.0025	1,994	1,689
	ST-04	12.19	12.95	0.698	6.1	0.0028	2,148	1,822
	ST-05	18.29	18.9	0.572	5.35	0.0023	2,298	1,983
	ST-06	21.34	22.1	0.234	2.1	0.0010	2,205	1,902
	ST-07	25.91	26.67	0.56	5.05	0.0023	2,216	1,983
	ST-08	39.62	40.38	0.376	3.5	0.0015	2,287	2,047
	KP25-06	ST-01	1.52	2.28	0.341	2.5	0.0014	1,802
ST-05		19.81	20.57	0.757	6.15	0.0031	1,996	1,644
ST-07		23.16	23.92	0.66	6.1	0.0027	2,271	2,044
KP25-08	ST-01	15.39	16.05	0.59	5.75	0.0024	2,395	1,914
	ST-01	25.91	26.59	0.68	5.55	0.0028	2,006	1,647
	ST-02	27.74	28.5	0.595	4.85	0.0024	2,003	1,644
	ST-03	29.26	29.85	0.595	5.85	0.0024	2,416	1,983
KP25-10	ST-01	3.05	3.81	0.59	4.35	0.0024	1,812	1,670
KP25-11	ST-01	9.14	9.86	0.66	5.5	0.0027	2,048	1,868
KP25-13	ST-01	1.52	2.28	0.66	4.85	0.0027	1,806	1,666
	ST-03	9.14	9.9	0.66	5.05	0.0027	1,880	1,430
	ST-04	30.78	31.54	0.68	5.75	0.0028	2,078	1,584
	ST-05	32.31	33.07	0.67	5.35	0.0027	1,962	1,398
	ST-06	35.36	36.12	0.26	2.75	0.0011	2,599	1,982

Drill Hole ID	Sample ID	Depth From	Depth To	Sample Length	WT Soil	Sample Volume	Bulk Density	Estimated Dry Density
		(m)	(m)	(m)	(kg)	(m ³)	(kg/m ³)	(kg/m ³)
	ST-07	36.58	37.34	0.69	5.5	0.0028	1,959	1,493
KP25-14	ST-01	4.57	5.33	0.655	4.4	0.0027	1,651	1,388
	ST-02	9.14	9.9	0.18	1.1	0.0007	1,502	1,263
	ST-03	16.76	17.52	0.605	5.15	0.0025	2,092	1,759
	ST-05	28.96	29.72	0.69	5.85	0.0028	2,083	1,604
	ST-06	30.48	31.24	0.69	5.9	0.0028	2,101	1,617
	ST-07	32	32.76	0.69	5.65	0.0028	2,012	1,549
	ST-08	36.58	37.34	0.59	5.05	0.0024	2,103	1,619
KP25-15	ST-01	9.14	9.9	0.665	5.2	0.0027	1,922	1,601
	ST-04	30.78	31.38	0.535	4.65	0.0020	2,305	1,876
	ST-05	32	32.6	0.52	4.5	0.0020	2,295	1,867
	ST-06	35.05	35.65	0.48	3.55	0.0018	1,962	1,596
	ST-07	36.58	37.18	0.505	4.35	0.0019	2,285	1,859
	ST-08	38.1	38.86	0.61	5.15	0.0023	2,239	1,822
	ST-09	39.62	39.87	0.32	2.55	0.0012	2,114	1,720
KP25-16	ST-02	21.34	22.08	0.719	6.55	0.0027	2,416	2,052
KP25-17	ST-02	13.72	14.48	0.713	5.75	0.0029	1,981	1,614
	ST-04	33.53	34.29	0.42	3.75	0.0017	2,193	1,832
	ST-05	35.05	35.81	0.68	5.70	0.0028	2,059	1,720
	ST-06	36.58	37.34	0.70	5.85	0.0029	2,053	1,715
	ST-07	38.10	38.86	0.70	5.60	0.0029	1,965	1,642

Drill Hole ID	Sample ID	Depth From	Depth To	Sample Length	WT Soil	Sample Volume	Bulk Density	Estimated Dry Density
		(m)	(m)	(m)	(kg)	(m ³)	(kg/m ³)	(kg/m ³)
	ST-08	39.62	40.22	0.32	2.85	0.0013	2,187	1,828
KP25-18	ST-01	10.67	11.27	0.40	3.35	0.0016	2,057	1,729
	ST-02	13.72	14.32	0.55	4.85	0.0022	2,166	1,832
	ST-03	16.76	17.36	0.55	4.75	0.0022	2,121	1,699
	ST-04	21.34	21.94	0.54	4.80	0.0022	2,183	1,833

10.3.2 Laboratory Soil Testing

Sampling of select soil units was completed during the site investigations to help characterize the encountered materials and to provide samples for laboratory testing. The collected samples are representative of the soil conditions. Following the completion of the drilling program, the select soil samples were delivered to KP's North Bay office and remaining samples were stored in STLLR's core shack. KP reviewed the drill hole information, photographs and samples provided and developed a laboratory testing schedule for select samples. Laboratory testing was completed by Englobe in North Bay, Ontario. KP coordinated the lab testing and provided input on testing, as required.

10.4 Drill Site Closure

Upon completion of drilling, the drill sites were closed in compliance with the Prospectors and Developers Association of Canada's (PDAC's) E-plus Framework for Responsible Exploration to minimize any adverse effects on the environment. This included chipping any vegetation down to surface level, grading to original topography, filling the drill holes where necessary with sand, seeding and placing straw to promote vegetation growth.

11.0 SAMPLE PREPARATION, ANALYSES, AND SECURITY

11.1 Core Handling, Sampling, and Security

For the Project, samples were generally collected at 1 m interval lengths, while respecting the Unit Type boundaries, unless a shorter or longer sample length was required depending on core recovery. The sequential sampling was carried out with the exception of organic material which could not be processed in the laboratory. Samples were cut manually along the core axis. One half was kept as a reference sample in the core boxes for core inventory, and the other half was sampled for analysis.

Samples were submitted to the primary lab, ALS Geochemistry Laboratories (ALS), and secondary (umpire) lab, Bureau Veritas Laboratories (BV), which are independent of the issuer and ISO/IEC 17025-accredited laboratories.

Samples were collected directly from the secured STLLR core facility in Timmins., by ALS staff and were delivered directly in sealed rice sacks to their respective sample preparation facilities in Timmins. STLLR staff shipped third-party check pulps directly to Bureau Veritas laboratory facilities in Timmins.

The tailings sample was initially weighed wet, dried in the oven up to 60-degree Celsius temperature until fully dried, then weighed dry. The dried sample was then broken using a rubber mallet and sieved through a 180-micron screen (Tyler 80 mesh). The minus fraction that had passed through the screen was collected, homogenized, and split into a 250 g fraction and used in the analytical packages, and the remaining plus and minus fractions were stored at the primary lab for 90 days. The homogenized sample was analyzed by a 50 g charge fire assay with AAS finish.

CRMs were inserted at a frequency of ~1 in 25 (4%) by the core loggers (three samples per batch of 72). The standards used covered 3 grade ranges: near cut-off (~0.3 g/t Au), average grade of mineralization in the area (~0.9 g/t Au) and higher grade (3 to 5 g/t Au). Independent CRMs were sourced by OREAS through Analytical Solutions Ltd. Silica sand material was used as a blanks, which were inserted at a frequency of 2 per batch of 72 samples (~3%). The pulp duplicate samples, a second repeat sample from the sample prepared pulp, were inserted right after the preceding original sample twice per batch of 72 samples.

Check assay pulp samples (third-party checks) were selected from 5% of the prepared sample pulps and sent to an independent third-party laboratory, BV in Timmins, ON, upon receipt of the returned pulps from the primary laboratory. The samples were selected to cover the grade range of interest. New CRMs and check assay pulp blanks were inserted at a rate of 3 standards and 2 blanks in each batch of 72 samples.

The original certified assay certificates (pdf, csv file formats) were received from ALS and BV Laboratories' Information Management Systems (LIMS) upon completion of the laboratory process and were imported to STLLR's secure database management web-platform, MX Deposit. The sampling database mapped the sample IDs from the relative imported assay certificates, and assay results incorporated and validated through pre-assigned QA/QC procedures in MX Deposit. All the assay files are stored on the STLLR secure Egnyte webserver for assay calculations and QA/QC analysis report.

11.2 Quality Assurance and Quality Control

The assay results for CRMs were plotted upon receipt of the initial assays. Any CRM that fell above or below the mean certified 3xSD were recorded as a failure, and a warning warranted if it fell within 2x and 3x SD. Moreover, if more than four consecutive assays of the same CRM fell above or below the mean but within 2xSD, it was also considered a failure. Re-assay requests submitted to the Lab required that the samples halfway between the CRMs before and after the failure be re-analyzed. Moreover, a different CRM type was provided to the Lab in place of the failed CRM. This methodology was repeated until the CRM within the re-assay batch passed.

For a blank sample, any reported assay greater than five times the lower detection limit of the analytical method was considered a failure. Failures were noted, and significant failures or continued failures resulted in batch re-assaying. Blanks that reported assays within five times the lower detection limit were considered a warning. Blank results reported up to the lower detection limit were considered a pass.

11.2.1 2025 Drill Program QA/QC Results

From January 2025 to October 2025, a total of 11,927 samples were sent to ALS for fire-assay and geochemical analysis, including 1200 QA/QC samples (CRM, Blanks, Pulp Duplicates). In addition, 536 Original pulp samples along with 40 QA/QC samples were sent to BV lab for third-party checks (Table 11.1 and Figure 11.1 through Figure 11.12).

Table 11.1: 2025 Drill Program QA/QC Results

QA/QC Sample Type	Certified Au Value (ppm)	No. QA/QC Samples Analyzed	No. QA/QC Samples Pass	No. QA/QC Samples Warning	No. QA/QC Samples Fail
OREAS 230	0.337	173	171	2	0
OREAS 231	0.542	9	9	0	0
OREAS 233	1.05	167	163	4	0
OREAS 240	5.51	177	168	6	3
OREAS 296	2.19	1	1	0	0
Blanks	-	350	350	0	0
Pulp Duplicates	-	335	-	-	-

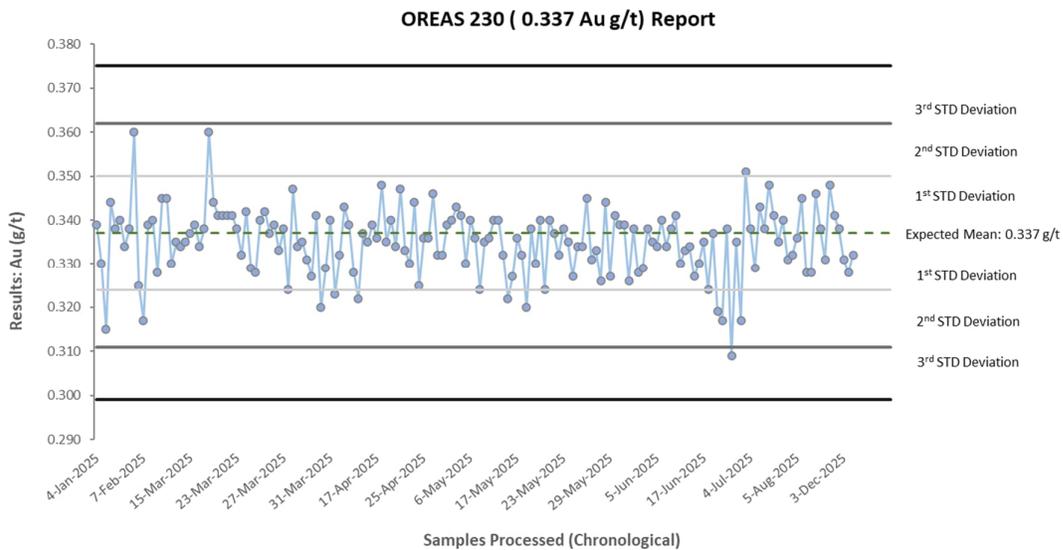


Figure 11.1: CRM Control Chart – OREAS 230, ALS Lab

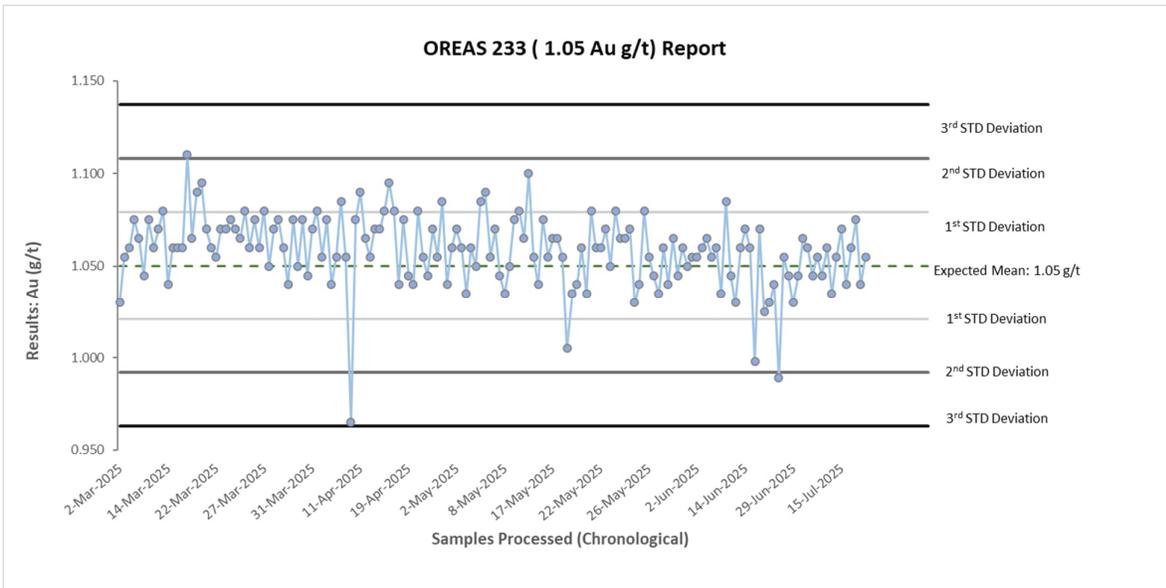


Figure 11.2: CRM Control Chart – OREAS 233, ALS Lab

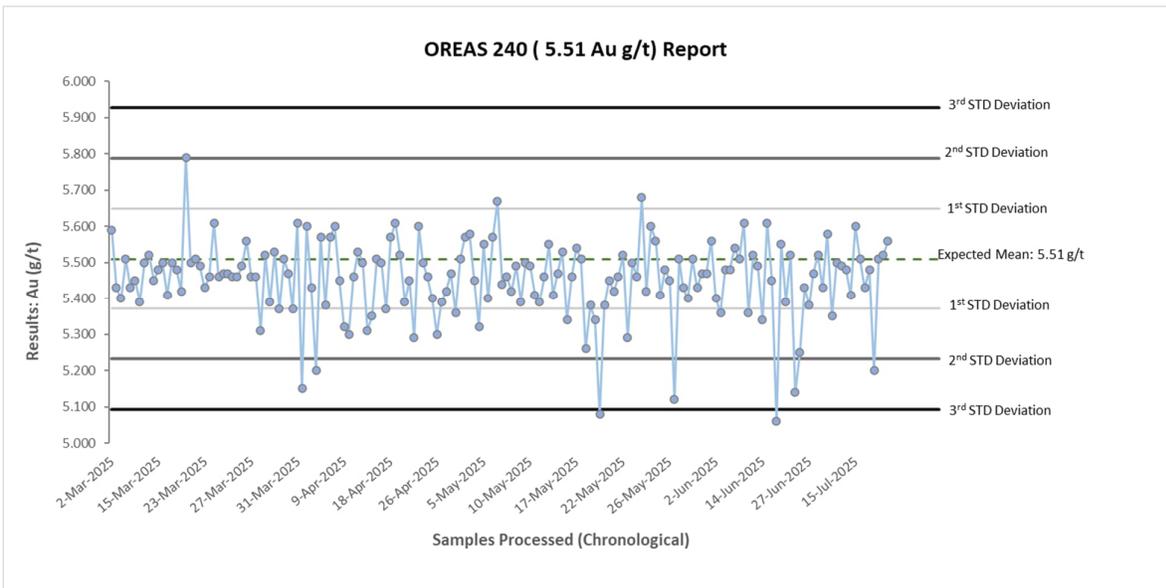


Figure 11.3: CRM Control Chart – OREAS 240, ALS Lab

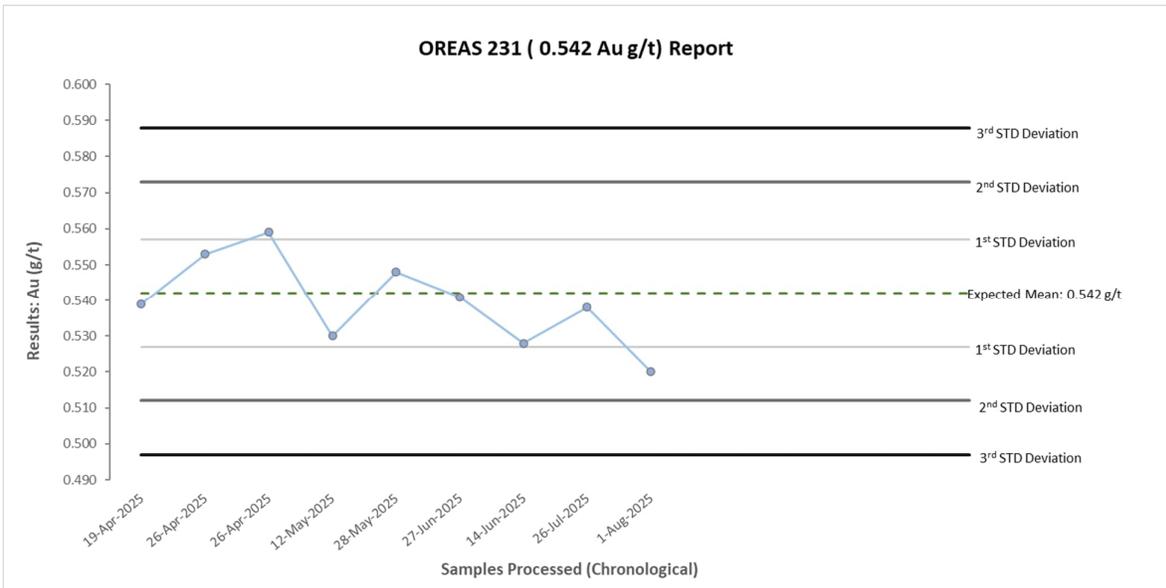


Figure 11.4: CRM Control Chart – OREAS 231, ALS Lab

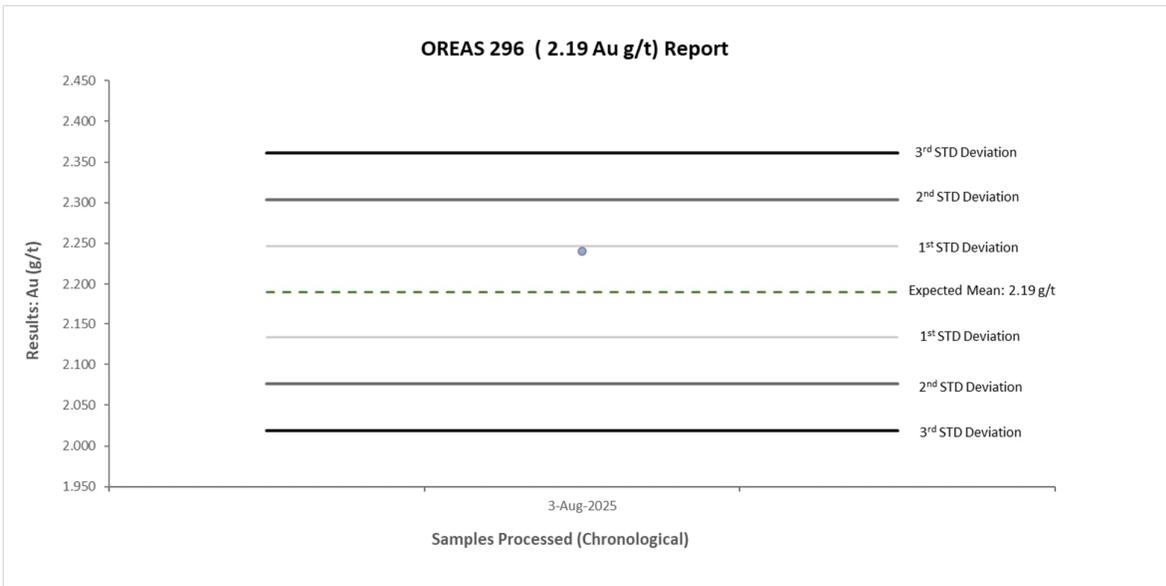


Figure 11.5: CRM Control Chart – OREAS 296, ALS Lab

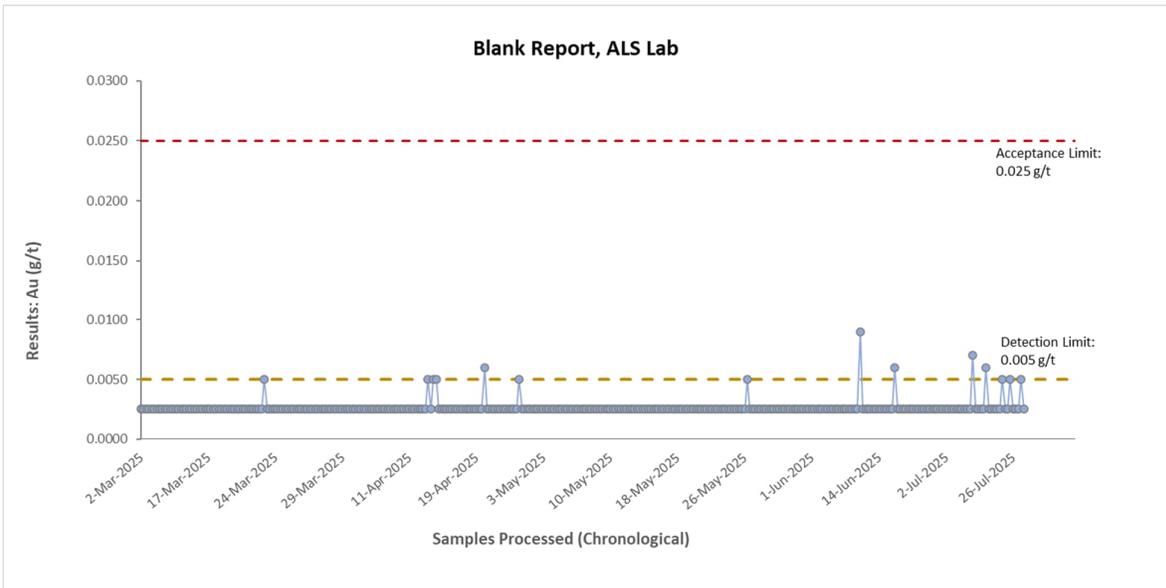


Figure 11.6: Blank Material Control Chart, ALS Lab

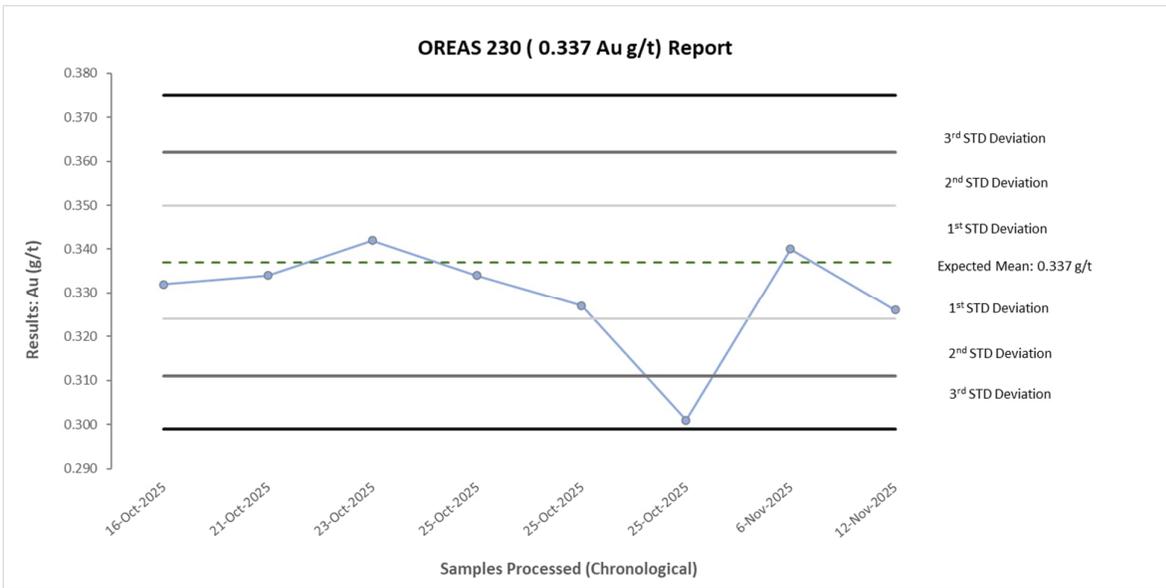


Figure 11.7: CRM Control Chart– OREAS 230, BV Lab

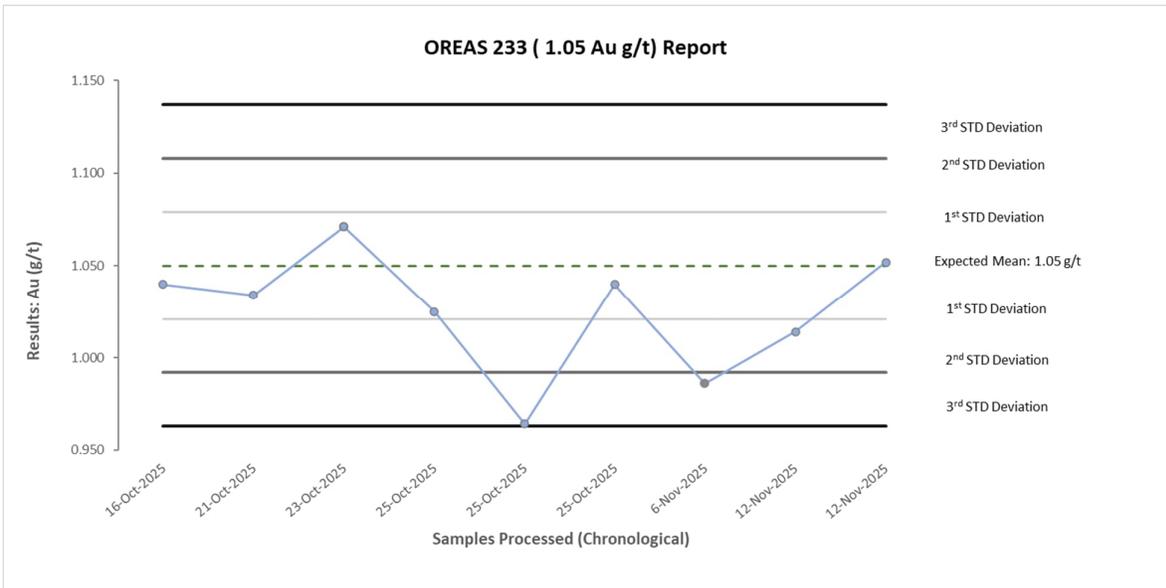


Figure 11.8: CRM Control Chart– OREAS 233, BV Lab

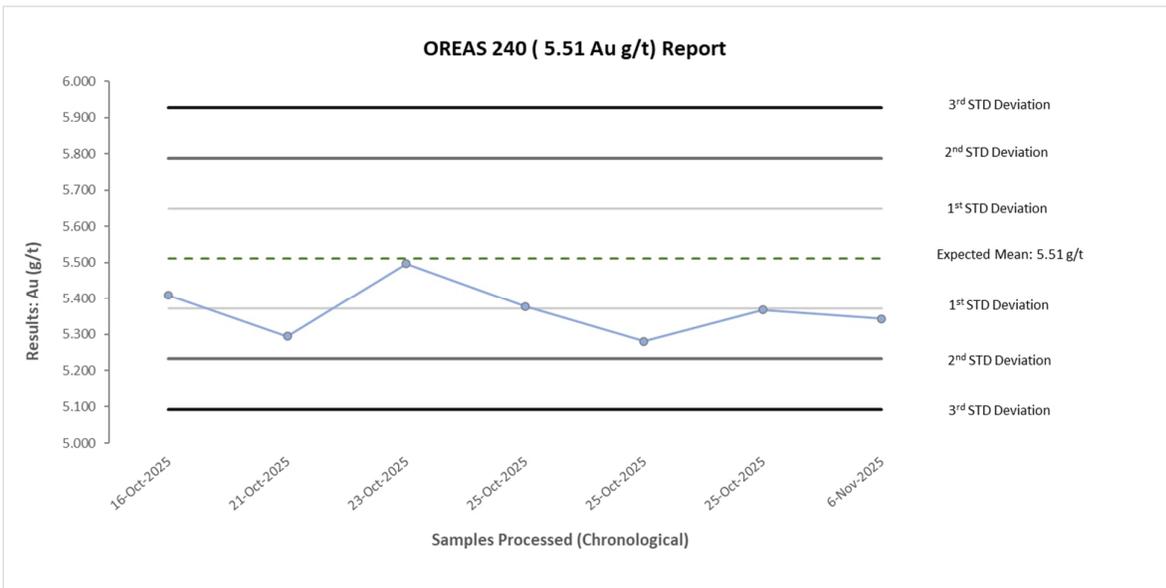


Figure 11.9: CRM Control Chart– OREAS 240, BV Lab

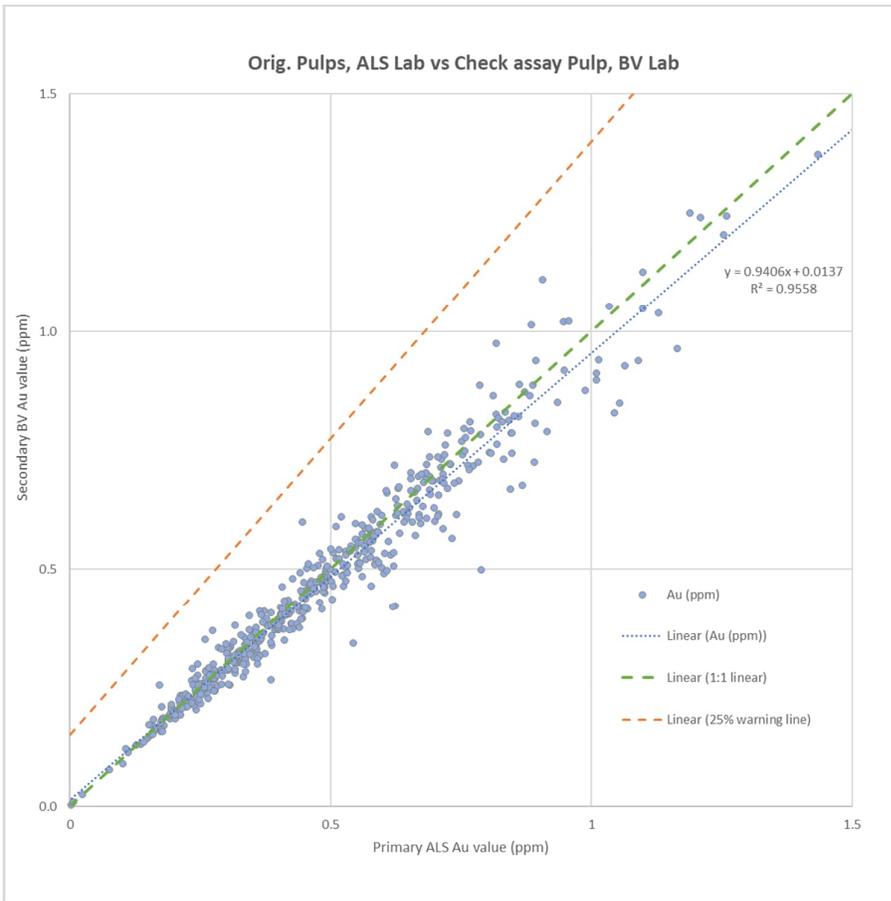


Figure 11.12: Cross-Plot of Third-Party Pulp Duplicates, ALS vs BV

11.3 QP Opinion

The QP responsible for the MRE reviewed the drilling, sampling, analytical and QA/QC procedures and sample chain of custody used by STLLR and is of the opinion that most of the procedures were consistent with industry standards but that there are possible concerns with the analytical sample preparation / sample reduction procedures chosen by STLLR that could have the potential to introduce a relative bias into the assay data which the QA/QC program would not be able to detect.

The sample preparation methodology used (ALS PREP-41) was designed for soil and sediment material which consisted of drying and sieving to 180 µm with the minus (fine) fraction retained for analysis. Upon drying, the tailings material hardened and was manually broken down using a mallet prior to sieving. This procedure, depending on the proportion of material passing through the sieve, has the potential to produce a split that is not representative of the full sample if coarser grain sizes were excluded.

The QP recommends that a representative 10% of remaining core be analyzed using a standard preparation procedure for rock such as ALS PREP-31 package consisting of crushing, pulverization and riffle splitting, or optionally photon analysis, to ensure a representative and unbiased assay preparation and analysis methodology to further evaluate the sample database.

Refer to Items 12.4 and 14.6.1 for further analysis and discussion.

12.0 DATA VERIFICATION

The data verification conducted by the mineral resource QP consisted of a personal inspection of the tailings project site, confirmation of drill collar locations, inspection of the dam construction, collection of two field samples for analysis, inspection of the core logging and storage facility, independent sampling of sonic core material and spot check comparisons of the STLLR database assay against original source certificates.

12.1 Site Visit

12.1.1 Hollinger Project Site

Mr. Brian Thomas conducted a personal site inspection on August 27, 2025, at the tailings project site, to observe site conditions, conduct spot check verification of drill collar locations, and collect field samples.

Collar surveys were taken for three holes using a hand-held Garmin Global Positioning System (GPS), as shown in Figure 12.1 and compared to the STLLR collar survey database. All collar locations were found to be a reasonable match within the 3 m accuracy of the GPS, as summarized in Table 12.1.

Table 12.1: Summary Comparison of QP Collar Measurements Compared to STLLR Survey Data

Name	STLLR		WSP		DIFFERENCE	
	Easting	Northing	Easting	Northing	Easting	Northing
HTF25-073	476,656.2	5,366,872.8	476,656.9	5,366,870.5	- 0.6	2.3
HTF25-090	476,902.5	5,367,018.2	476,901.9	5,367,017.7	0.6	0.5
HTF25-224	476,509.7	5,366,516.2	476,509.8	5,366,514.2	- 0.1	2.0

Hole collar positions were marked with rebar with a high-visibility cap, with hole number stamped into a metal tag, as shown in Figure 12.1.



Figure 12.1: Example Drill Hole Collar for Hole HTF25-224 on the Phase 1 Wall

Two field samples were taken from accessible tailings material at surface FS1, and FS2, to verify the presence of precious metals and confirm that the grades were within the expected ranges (locations shown in red in Figure 12.2). FS1 was from Phase 1 wall material and FS2 from the Phase 1 cell. The assay for FS1 was 0.42 g/t Au, which was found to be like near surface assays from hole HTF25-224 (0.46 g/t) and FS2 returned a grade of 0.34 g/t Au which was a good match with near surface intervals from holes HTF25-231 (0.34g/t) and HTF25-243 (0.30).



Source: Image courtesy of Google Earth June 19, 2024

Figure 12.2: Drill Hole Collar Survey and Field Sample Locations

12.1.2 Core Logging and Storage Facility

Mr. Brian Thomas conducted a site inspection of the core logging facility located on Highway 655 just north of Timmins, to review geological data collection, QA/QC and security procedures, and complete verification logging and sampling of sonic drill core. The site is secured by a locked gate and buildings where core is logged, sampled and stored. The Hollinger core boxes were found to be well organized and labelled in the yard and securely strapped to pallets (Figure 12.3). The logging, sampling, QA/QC and chain of custody procedures were reviewed with STLLR geology staff and were found to be consistent with industry practices.



Figure 12.3: Hollinger Core Storage

12.2 QP Data Verification

A selection of nine core samples was chosen for independent field duplicate sampling from holes distributed across the deposit representing intervals in the Phase 1 and 2 walls and cells. Samples of the remaining half core material were quarter split using a metal trowel and scooped into poly bags and zip tied. Individual bags were placed in rice sacks and secured for transport and delivered directly to the ALS office in Sudbury, ON by the QP.

Sample preparation was conducted using the ALS preparation package ALS PREP-31 consisting of drying, crushing, riffle splitting 250 g, and pulverizing, with gold analysis completed using the AU-AA24 package consisting of fire assay using a 50 g sample with an atomic absorption spectroscopy (AAS) finish. The preparation package chosen by the QP (ALS PREP-31) was slightly different than what was used by STLLR (ALS PREP-41) to ensure a representative split.

A comparison of the assay results is summarized in Table 12.2 with a graphical comparison plotted in Figure 12.4. The comparison of results indicates an overall grade difference between the independent QP samples and the STLLR samples being approximately -16% with total mean grades of 0.40 g/t and 0.48 g/t respectively.

Table 12.2: Comparison of Independent Assay Results to the STLLR Database

BHID	STLLR				WSP	
	From	To	Sample	Assay	Sample	Assay
HTF25-051	21.9	22.85	M589031	0.56	P449174	0.30
HTF25-051	23	24	M589032	0.25	P449175	0.26
HTF25-094	12.2	13	M575955	0.42	P449170	0.37
HTF25-126	7.6	8.6	M576984	0.35	P449176	0.30
HTF25-129	20.85	21.85	M586534	0.65	P449173	0.59
HTF25-215	12.2	12.95	M579427	0.79	P449177	0.66
HTF25-265	10	11	M577894	0.66	P449178	0.55
HTF25-271	16	17	M577873	0.51	P449172	0.46
HTF25-339	6.8	7.6	M577938	0.17	P449171	0.17

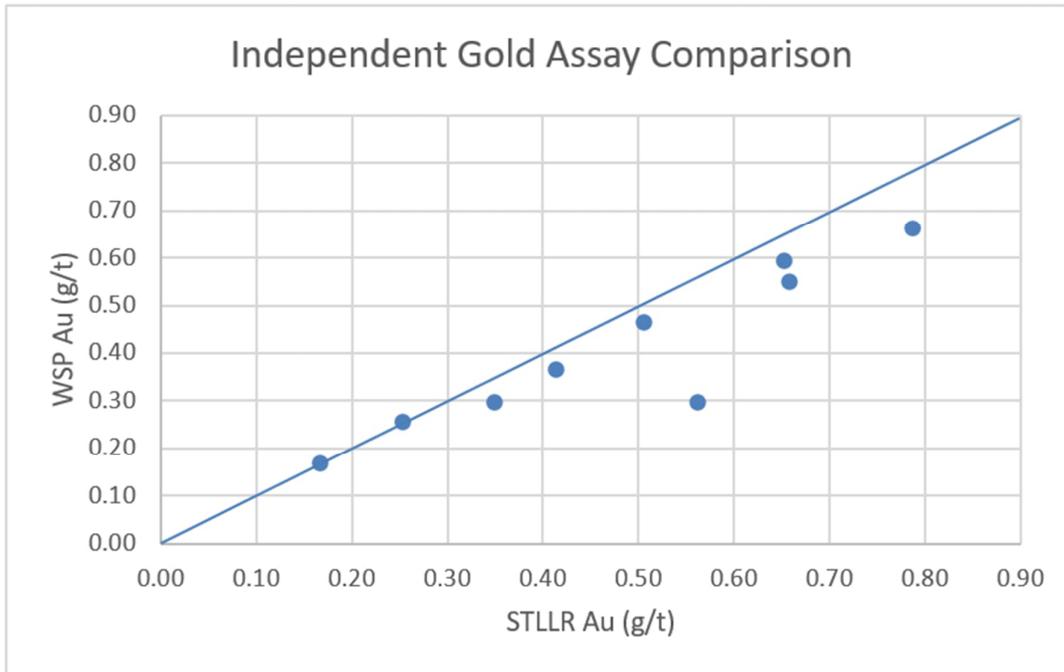


Figure 12.4: Scatterplot Comparison of Verification Samples and STLLR Samples

Since the sample size was limited, and the quarter core volume of the verification samples was smaller than the original half core samples, the QP requested STLLR to conduct further duplicate analysis using the ALS PREP-31 package on coarse rejects for 20 samples. The results of this comparison indicated a grade difference of -10.7% relative to the original sample grades.

Prior to the site inspection, STLLR completed their own evaluation based on 135 coarse reject samples using photon analysis. Review of the photon assay results compared to the original values indicated a total un-weighted mean difference of -9%, where the total mean grade of the original assays was 0.503 g/t vs 0.458 g/t for the total mean grade of the photon assays. A graphical comparison of these samples is shown in Figure 12.5.

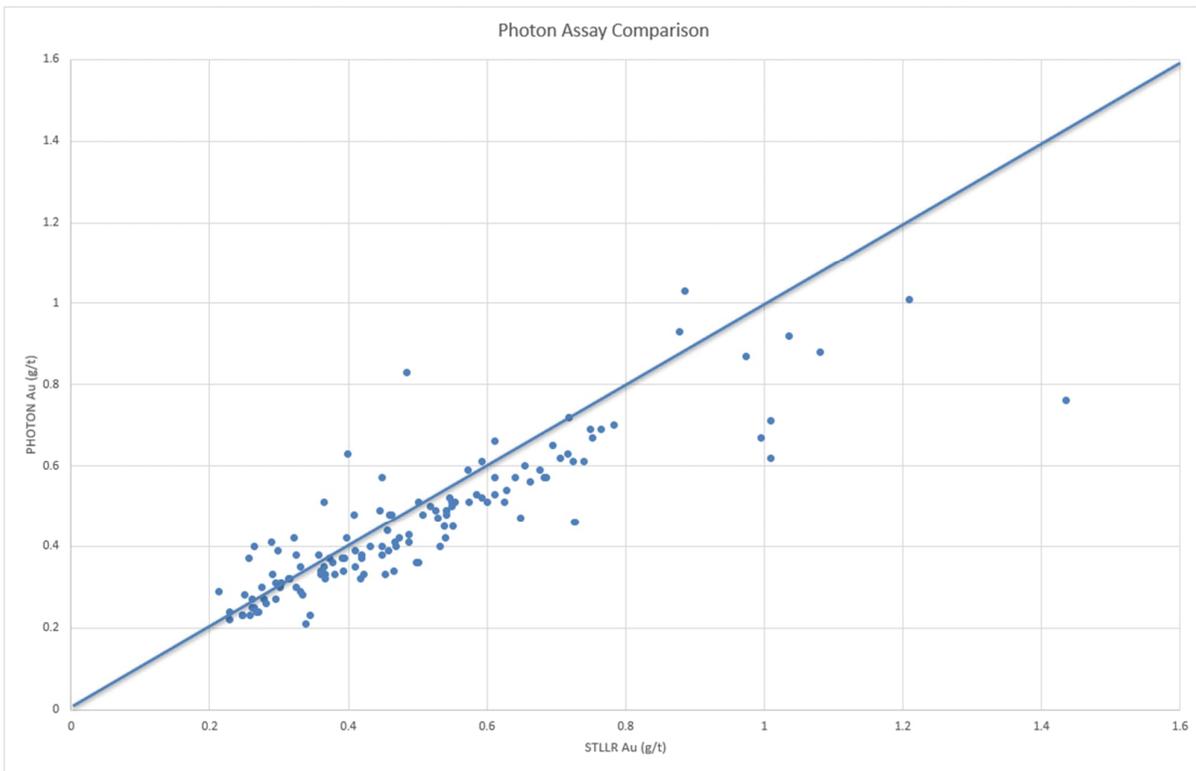


Figure 12.5: Scatterplot Comparison of Photon Duplicate Samples and STLLR Original Samples

All of the data from the three programs was then combined, totaling 162 samples, and a standard set of 6 QA/QC plots were generated for further evaluation as shown in Figure 12.6. Plots included a scatter plot, Thompson & Howarth, HARD (half absolute relative difference), QQ (quantile-quantile), HRD (half relative difference) and Cumulative HARD plot.

The results indicated a total mean grade difference of 0.048 g/t, (0.503 g/t for the primary samples vs 0.455 g/t for the combined coarse rejects and field duplicates) with the trend of the relative differences generally increasing with grade. The QQ plot indicates a deviation between sample populations above approximately 0.5 g/t. The scatter of points seen in the HARD and Thompson & Howarth plots, for a portion of the sample pair population, is higher than the expected thresholds for coarse duplicates of approximately 10-15% which can generally be interpreted as a sample preparation issue. Although, 80% of the population being below the 10% difference threshold in the Cumulative HARD plot could also be considered acceptable for coarse reject duplicates.

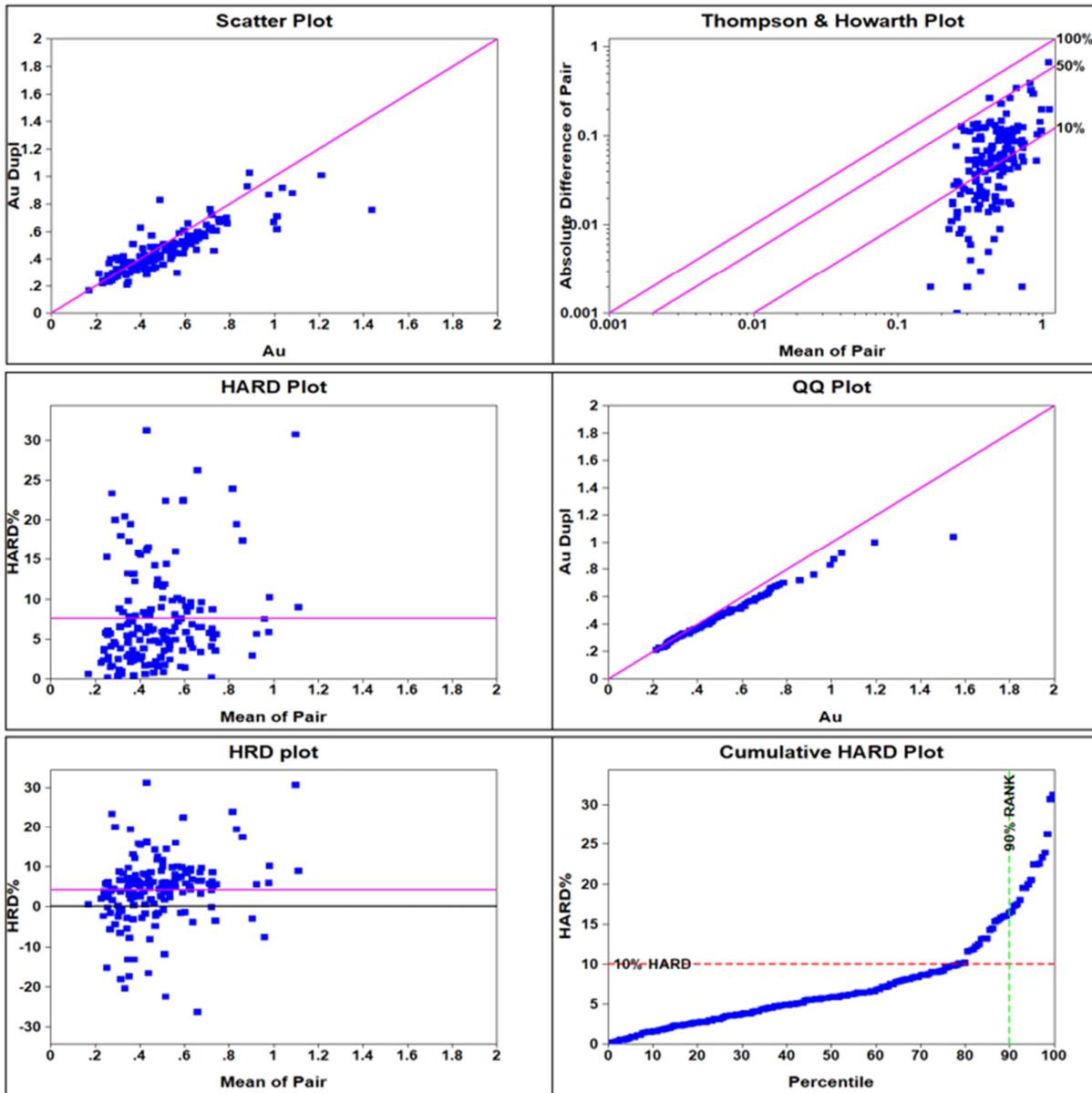


Figure 12.6: Summary QA/QC Plots

The QP concludes, based on this preliminary investigation, that the assay precision is marginal for approximately 20% of the sample population and that there is evidence of a small relative bias likely attributed to the sample preparation procedures used. Other considerations that could have cumulatively impacted the reproducibility of the duplicate samples are the differences in sample size, grain size of the tailings material, differing analytical methods and nugget effect.

Approximately 10% of the STLLR assay database (Au only) was also compared to the original lab certificates provided by ALS and no errors were identified during this check.

12.3 Metallurgical Data Verification

The metallurgical QP has examined the metallurgical test work data and associated reports, assessed the analytical procedures, evaluated the laboratory's qualifications, and reviewed the presentation of the test results. All aspects were found to be consistent with industry-standard practices. Additional statements on the adequacy of the metallurgical data are presented in Item 13.0.

12.4 Conclusions and Recommendations

The mineral resource QP conducted a personal site inspection of the project site and the core facility. No material issues were identified with the drilling, logging, sampling, QA/QC or chain of custody procedures and these procedures were determined to be consistent with industry practices.

Based on the limited duplicate sample data available, the QP identified that the sample preparation procedure used may have introduced a small relative bias in the assay data and resulted in marginal precision for a portion of the sample data. The QP concludes that the assay data is suitable for the purpose of modelling and grade estimation which form the basis of this maiden MRE but acknowledges that further testing and analysis is warranted. It is uncertain if the issues identified would have any material impact to the MRE as there was no indication of any grade bias issues in the metallurgical testwork, based on the 3 composite samples (100 kg) described in Item 13.0.

As stated in Item 11.0, the QP recommends that a representative 10% of remaining core be analyzed using a standard preparation procedure for rock such as ALS PREP-31 package consisting of crushing, pulverization and riffle splitting, or optionally photon analysis, to ensure a representative and unbiased assay preparation and analysis methodology in order to further evaluate the sample database. The reader is recommended to review Item 14.6.1 for further discussion of risk to the MRE.

13.0 MINERAL PROCESSING AND METALLURGICAL TESTING

A metallurgical testing program was conducted on three composite samples of Hollinger Tailings at the SGS Lakefield facility located in Ontario, Canada. The samples were received at SGS in July 2025, and tests were conducted later that year.

The objective of the test program was to evaluate different processing options to recover gold from the historic tailings. Gravity separation, leaching and flotation were investigated.

Mr. David Jin is aware of historical metallurgical testwork conducted over 35 years ago on the same tailings resource. These results are briefly summarized in Item 6.0.

13.1 Sample Composition

Three composites weighing roughly 100 kg were prepared by STLLR from original 50% split core to be used for the metallurgical testwork campaign. The various drilled samples were visually categorized and combined to form composites by sediment type (sand, silt and clay):

- Sandy Silt: HTM25-SASIL-A-OV (SGS #: Composite 1)
- Silty Clay: HTM25-SILCL-A-OV (SGS #: Composite 2)
- Silty Sand: HTM25-SILSA-A-OV (SGS #: Composite 3)

It is the opinion of the QPs that the composites were prepared to adequately represent the overall tailings resource in terms of spatial location, depth and average gold grade per sediment type.

The Sandy Silt Composite (Composite 1) was composed of samples taken at the following location and depth within the tailings resource (refer to Figure 13.1 and Figure 13.2):

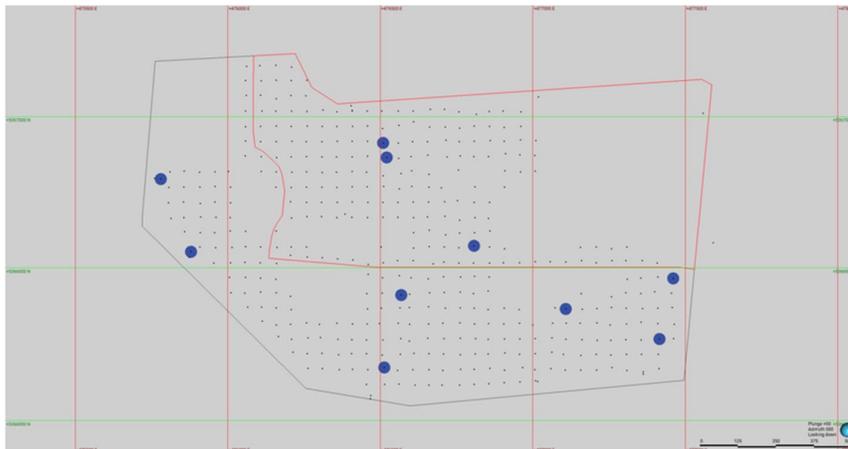


Figure 13.1: Sandy Silt Composite (Composite 1) – Samples Location

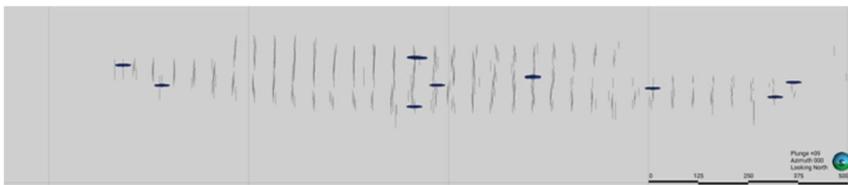


Figure 13.2: Sandy Silt Composite (Composite 1) – Samples Depth

The Silty Clay Composite (Composite 2) was composed of samples taken at the following location and depth within the tailings resource (refer to Figure 13.3 and Figure 13.4):

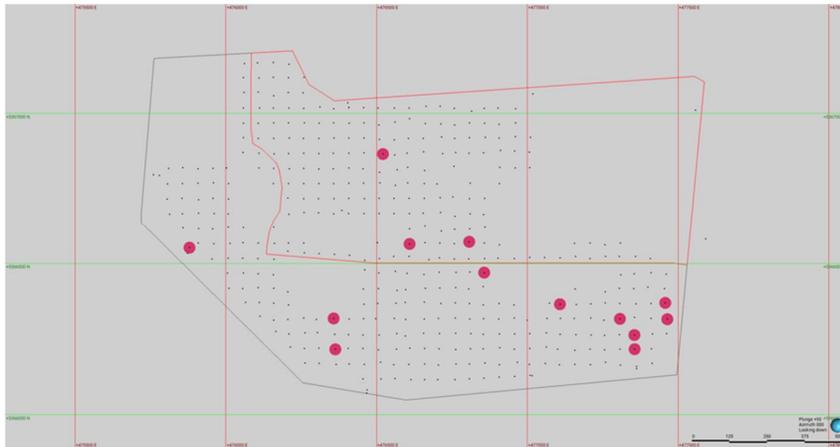


Figure 13.3: Silty Clay Composite (Composite 2) – Samples Location

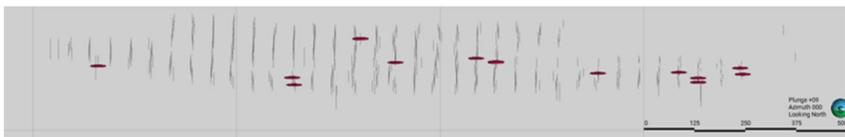


Figure 13.4: Silty Clay Composite (Composite 2) – Samples Depth

The Silty Sand Composite (Composite 3) was composed of samples taken at the following location and depth within the tailings resource (refer to Figure 13.5 and Figure 13.6).

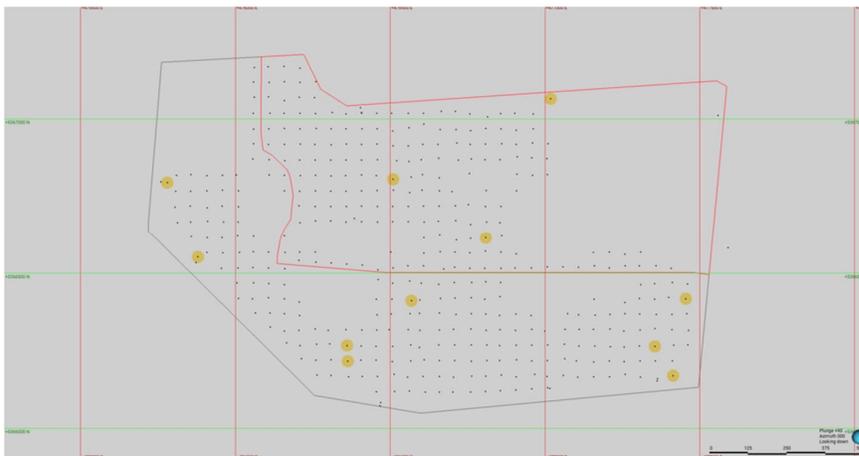


Figure 13.5: Silty Sand Composite (Composite 3) – Samples Location

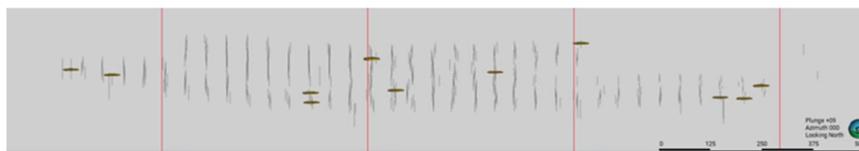


Figure 13.6: Silty Sand Composite (Composite 3) – Samples Depth

13.2 Head Sample Characterization and Mineralogical Analysis

All three composites were assayed for head composition, mineralogy and used for all the subsequent gravity, leaching and flotation tests. The composite samples were subject to fire assay to determine the gold content, a multi-element ICP scan, sulphur specification and carbon speciation analysis.

The composite grades varied from 0.33 g/t to 0.37 g/t Au and 1.98% to 2.40% S, with a consistent carbon content of approximately 3.2%. The head grade of silver was less than 2 g/t. Additionally, lead was detected at approximately 24 g/t. Results are summarized in Table 13.1.

Table 13.1: Composites Chemical Analysis

Analysis	Units	Comp 1 HTM25-SASIL-A-	Comp 2 HTM25-SILCL-A-	Comp 3 HTM25-SILSA-A-
		OV (Sandy Silt)	OV (Silty Clay)	OV (Silty Sand)
P ₈₀	(µm)	123	123	160
Au, cut A	(g/t)	0.31	0.34	0.34
Au, cut B	(g/t)	0.34	0.36	0.39
Au, average	(g/t)	0.33	0.35	0.37
S	(%)	2.40	2.05	1.98
S ⁻²	(%)	2.15	1.72	1.86
C(t)	(%)	3.17	3.19	3.2
C(g)	(%)	0.06	<0.05	<0.05
CO ₃	(%)	14.8	14.5	14.8
Ag	(g/t)	< 2	< 2	< 2
Al	(g/t)	59800	58500	53800
As	(g/t)	195*	197*	212*
Ba	(g/t)	277	274	235
Be	(g/t)	0.51	0.5	0.51
Bi	(g/t)	< 20	< 20	< 20
Ca	(g/t)	53000	53500	53600
Cd	(g/t)	< 2	< 2	< 2
Co	(g/t)	33	34	35
Cr	(g/t)	< 200	< 200	< 200
Cu	(g/t)	96	99	91
Fe	(g/t)	68000	66500	63800
K	(g/t)	16200	15100	13300
Li	(g/t)	13	13	19
Mg	(g/t)	24600	23900	23500
Mn	(g/t)	1730	1630	1620
Mo	(g/t)	< 5	< 5	< 5
Na	(g/t)	7490	8230	8770
Ni	(g/t)	68	72	69
P	(g/t)	384	397	395
Pb	(g/t)	25	23	23
Sb	(g/t)	< 10	< 10	< 10
Se	(g/t)	< 30	< 30	< 30
Sn	(g/t)	< 20	< 20	< 20
Sr	(g/t)	109	114	116
Ti	(g/t)	3860	3750	3740
Tl	(g/t)	< 30	< 30	< 30
V	(g/t)	185	175	161
Y	(g/t)	5.1	5	5.3
Zn	(g/t)	348	315	287

Note: *Calculated from assays of the flotation test products (concentrate and tails).

A particle size distribution analysis was performed, and composites 1, 2, and 3 displayed a P80 of 123 µm, 123 µm, and 160 µm, respectively. The samples top size was approximately 425 µm.

The mineralogical analysis was conducted by quantitative x-ray diffraction to determine the mineral species that make up the composite samples. The results revealed that the tailings are primarily composed of quartz, ankerite, and muscovite, with minor amounts of other gangue minerals such as albite, chlorite, calcite and dolomite. Sulphides accounted for about 4% of the samples and consisted mainly of pyrite with trace levels of arsenopyrite and pyrrhotite. Results are presented in Table 13.2.

Table 13.2 Mineralogy of Composites by XRD

Mineral / Compound	Comp 1	Comp 2	Comp 3	Formula
	HTM25-SASIL- A-OV (Sandy Silt) (%)	HTM25-SILCL- A-OV (Silty Clay) (%)	HTM25-SILSA- A-OV (Silty Sand) (%)	
Quartz	30.0	31.2	31.3	SiO ₂
Albite	4.9	6.2	7.1	NaAlSi ₃ O ₈
Muscovite	25.0	22.9	20.2	KAl ₂ (AlSi ₃ O ₁₀)(OH) ₂
Microcline	0.6	1.1	1.5	KAlSi ₃ O ₈
Chlorite	6.0	5.9	5.6	(Fe, ₂ Mg, ₂ Mn) ₅ Al(Si ₃ Al)O ₁₀ (OH) ₈
Paragonite	0.7	0.5	0.3	NaAl ₂ (AlSi ₃ O ₁₀)(OH) ₂
Calcite	2.3	2.3	1.5	CaCO ₃
Dolomite	4.5	3.9	1.3	CaMg(CO ₃) ₂
Ankerite	20.3	20.5	25.1	CaFe(CO ₃) ₂
Magnetite	0.4	0.6	0.3	Fe ₃ O ₄
Rutile	0.3	0.4	0.5	TiO ₂
Pyrite	3.3	3.4	3.7	FeS ₂
Siderite	0.7	0.3	0.7	FeCO ₃
Fluorapatite	0.2	0.3	-	Ca ₅ (PO ₄) ₃ F
Arsenopyrite	0.6	0.4	0.3	FeAsS
Pyrrhotite	0.2	0.1	0.0	Fe ₈ S ₉
Diaspore	-	-	0.6	αAlO.OH
TOTAL	100.0	100.0	100.0	

Note: The samples were air dried, screened through a 20 mesh (850 µm) screen and rotary split into 1 kg and 10 kg test charges.

13.3 Gravity Separation

SGS processed 10 kg of each composite sample through a Knelson MD-3 laboratory concentrator under standard lab conditions to evaluate the proportion of gold recoverable by gravity separation. The resulting concentrate was further upgraded on a Mozley (C-800) laboratory mineral separator table. However, gravity separation tests yielded very low gold recoveries (2.6% to 3.7%) and concentrate grades (<50 g/t) demonstrating that gravity methods are not viable for processing the Hollinger Tailings.

Gravity separation tests results can be found in Table 13.3.

Table 13.3: Gravity Separation Tests Results

Sample	Feed Size	Concentrate, Cumulative			Tailings		Au Head Grade	
		% Mass Rec. (%)	Au Grade (g/t)	Au Rec. (%)	Au Grade (g/t)	Calc. (g/t)	Direct (g/t)	
Comp 1 HTM25-SASIL-A-OV (Sandy Silt)	123	0.041	23.4	3.7	0.25	0.26	0.33	
Comp 2 HTM25-SILCL-A-OV (Silty Clay)	123	0.027	44.5	3.7	0.32	0.33	0.35	
Comp 3 HTM25-SILSA-A-OV (Silty Sand)	160	0.035	23.3	2.6	0.30	0.31	0.37	

13.4 Cyanide Leaching

Cyanide leaching tests were completed using standard bottle roll tests conducted under initial conditions consisting of a 40% solids slurry, no pre-aeration, 1 gram per litre (g/L) sodium cyanide (NaCN) concentration, and a Dissolved Oxygen (DO) target of 8-9 parts per million (ppm). Leaching was performed over a 48-hour period, with gold recovery measured every 12 hours.

Initial bottle roll tests on the “as received” composite samples (without regrinding) established baseline recoveries, which remained below 30% after 48 hours.

The effects of grind size, NaCN concentration and dissolved oxygen levels were investigated to improve recovery.

13.4.1 Effect of Grind Size

Additional tests were conducted on the same composites at progressively finer grind sizes (P80 of 75 µm, 53 µm, 45 µm and 30 µm). Finer grinds led to improved gold extraction; recoveries for composites 1 and 2 were in the range of 60%, while Composite 3 achieved approximately 69% recovery at the finest P80 tested of around 30 µm.

Duplicate bottle roll tests at 30 µm, 1 g/L NaCN and 8-9 ppm DO were completed to determine the reproducibility of the results. Residue grades were within the analytical accuracy limits of +/- 0.02 g/t.

Overall, the weighted average gold recovery across all three composites, representing the entire resource, was calculated at approximately 61.3%.

13.4.2 Effect of NaCN Concentration

NaCN concentration was increased to 2 g/L and bottle roll tests were performed on 30 µm samples under the same conditions as the initial tests (except for the NaCN concentration). The higher cyanide concentration did not improve gold extraction.

13.4.3 Effect of Dissolved Oxygen

Dissolved oxygen levels were increased to above 30 ppm to improve gold recovery. Results of bottle roll tests on 30 µm samples were compared with the previous tests at 8-9 ppm DO and did not show any improvement in gold extraction.

13.4.4 Bottle Roll Tests Results

In total, 28 bottle roll tests have been completed. Detailed results are shown in Table 13.4 through Table 13.6.

Table 13.4: Leach Tests Results for Composite 1

Test #	P80 Target (µm)	% Solids (%)	NaCN Conc. (g/L)	DO Target (ppm)	Gold Extraction				Residue assays	Head grade	
					12 h (%)	24 h (%)	36 h (%)	48 h (%)	Average (Au g/t)	Calculated (Au g/t)	Direct (Au g/t)
CN1	123	40	1.0	~8	<23.3	<23.6	<23.8	24.1	0.25	0.32	0.33
CN4	67	40	1.0	~8	37.1	42.0	37.5	42.6	0.19	0.32	
CN5	58	40	1.0	~8	43.1	43.2	48.3	44.0	0.18	0.31	
CN10R	40	40	1.0	~8	43.4	48.5	43.8	49.1	0.16	0.31	
CN13	32	40	1.0	~8	48.1	48.7	49.2	54.8	0.14	0.31	
CN14	33	40	2.0	~8	49.9	50.4	51.0	56.7	0.13	0.30	
CN20	33	40	1.0	~8	55.8	55.9	56.1	56.7	0.14	0.31	
CN21	32	40	1.0	~8	55.4	55.5	60.7	56.5	0.13	0.30	
CN22	33	40	1.0	~31	54.8	54.8	60.5	55.9	0.14	0.32	

Table 13.5: Leach Tests Results for Composite 2

Test #	P80 Target (µm)	% Solids (%)	NaCN Conc. (g/L)	DO Target (ppm)	Gold Extraction				Residue assays	Head grade	
					12 h (%)	24 h (%)	36 h (%)	48 h (%)	Average (Au g/t)	Calculated (Au g/t)	Direct (Au g/t)
CN2	123	40	1.0	~8	23.3	23.5	28.3	28.7	0.23	0.32	0.35
CN6	74	40	1.0	~8	38.3	43.2	48.4	44.2	0.18	0.31	
CN7	51	40	1.0	~8	43.5	43.7	44.0	53.4	0.16	0.34	
CN11	46	40	1.0	~8	60.6	---	53.4	58.1	0.15	0.35	
CN15	39	40	1.0	~8	55.3	55.7	56.2	56.9	0.14	0.33	
CN16	40	40	2.0	~8	59.0	59.4	50.3	55.7	0.14	0.31	
CN23	38	40	1.0	~8	53.8	58.7	54.5	59.6	0.14	0.33	
CN24	37	40	1.0	~8	55.1	55.6	55.7	56.5	0.13	0.30	
CN25	40	40	1.0	~31	70.1	66.0	71.3	67.3	0.11	0.32	

Table 13.6: Leach Tests Results for Composite 3

Test #	P80 Target (µm)	% Solids (%)	NaCN Conc. (g/L)	DO Target ppm	Gold Extraction				Residue assays	Head grade	
					12 h (%)	24 h (%)	36 h (%)	48 h (%)	Average (Au g/t)	Calculated (Au g/t)	Direct (Au g/t)
CN3	160	40	1.0	~8	<22.6	22.9	23.0	27.9	0.24	0.33	0.37
CN8	75	40	1.0	~8	47.9	56.2	56.6	53.4	0.18	0.38	
CN9	54	40	1.0	~8	48.7	48.9	53.2	54.0	0.17	0.37	
CN12	45	40	1.0	~8	56.0	56.5	56.9	61.4	0.15	0.38	
CN17	34	40	1.0	~8	67.7	68.3	69.0	69.7	0.12	0.40	
CN18	33	40	2.0	~8	71.6	64.2	64.8	69.4	0.12	0.38	
CN26	33	40	1.0	~8	67.2	63.5	67.9	68.8	0.11	0.35	
CN27	33	40	1.0	~8	64.5	69.6	65.1	66.1	0.11	0.32	
CN28	32	40	1.0	~31	53.5	53.7	54.3	55.0	0.14	0.31	

13.5 Diagnostic Leach

A sequential diagnostic leach was performed on the residue from test CN7 on Composite 2 to examine the gold deportment and determine the maximum gold extractable by cyanidation. This sample was selected due to its superior performance at 53 µm. This procedure also quantified the proportion of gold recoverable only through oxidative treatment and identified the fraction that would remain unrecoverable.

The diagnostic leach involved regrinding the selected sample to a finer size, followed by a second cyanide leach. The residue from this cyanide leach was subsequently treated with aqua regia, enabling identification of gold requiring oxidative pre-treatment for recovery. Any gold remaining after aqua regia leaching was classified as unrecoverable.

The sample was reground to approximately 10 µm and leached with sodium cyanide. Results indicated that a maximum of 74.9% of the gold in Composite 2 was recoverable by cyanide leaching alone and this would only be achievable with ultrafine grinding.

However, based on this diagnostic leach test, approximately 22.4% of the gold present in the Hollinger Tailings would require an oxidative process, such as pressure oxidation (POX), for recovery. In a conventional cyanide leach mill flowsheet, this portion of gold would typically remain in the tailings. The remaining 2.7% of gold was found to be locked within silicate minerals or associated with fine sulphides encapsulated in silicates and was considered unrecoverable under the tested conditions.

13.6 Flotation

Flotation tests were conducted on the composite samples to assess the potential for achieving better gold recovery and producing a high-grade, marketable concentrate.

The flotation procedure consisted of seven stages of rougher flotation at natural pH for a total of 35 minutes of flotation time. Copper sulphate (sulphide activator), potassium amyl xanthate (PAX) and AERO 208 collectors and Methyl Isobutyl Carbinol (MIBC) (frother) were added. A baseline test on Composite 2 was completed with AERO 3477 and 3501 instead of AERO 208 but all subsequent tests were completed with AERO 208. The concentrates were collected at each stage, filtered, dried and submitted along with the final tailings, for gold, a multi-element ICP scan and sulphur analysis.

The initial flotation test, performed on a single Composite 2 sample ground to approximately 85 µm, demonstrated higher gold recovery compared to cyanide leaching (65.4%). The rougher concentrate grade obtained was 1.96 g/t Au.

Further flotation tests were carried out on all three composites at finer grind sizes of 53 µm and 38 µm. The highest gold recovery was achieved at the finest grind, with values ranging from 79.0% to 85.1%. The weighted average recovery across all composites was 82.5% for gold and 96.1% for sulphur. The rougher concentrate grades were below 4 g/t Au.

In total, seven flotation tests were performed. The results of the tests conducted on 38 µm samples are presented in Table 13.7.

Table 13.7: Flotation Results (P80 of 38 µm)

Test #	Head Grade		Mass Pull	Flot Conc Assays			Rec. to Flot Conc		
	Direct (Au g/t)	Calculated (Au g/t)	Ro Con (%)	Au (g/t)	Ag (g/t)	S (%)	Au (%)	S (%)	
Comp 1 HTM25-SASIL-A-OV (Sandy Silt)	F3	0.33	0.38	11.9	2.52	2.3	18.9	79.0	97.7
Comp 2 HTM25-SILCL-A-OV (Silty Clay)	F5	0.35	0.39	13.6	2.36	2.0	13.7	82.3	95.6
Comp 3 HTM25-SILSA-A-OV (Silty Sand)	F7	0.37	0.36	10.0	3.09	2.5	17.4	85.1	95.5
Weighted average tailings	-	0.35	0.38	11.7	2.69	2.3	16.5	82.5	96.1

13.7 Cyanidation of Flotation Tailings

The rougher tailings from Test F4 on Composite 2 ground to approximately 53 µm were leached under the same initial conditions as the bottle roll tests performed on whole ore.

The results showed that 45.4% of the gold in the flotation tailings can be leached with low NaCN consumption. The overall gold recovery by flotation plus cyanide leaching of the flotation tailings was 86.9%.

13.8 Deleterious Elements

Based on the available metallurgical test results, there are no known processing factors or deleterious elements present that would significantly impact the potential economic extraction of Hollinger Tailings material.

14.0 MINERAL RESOURCE ESTIMATES

The MRE and other information in this Item are forward-looking information. The factors that could cause actual results to differ materially from the forward-looking information include any significant differences from one or more of the following material factors or assumptions that were applied in drawing the conclusions or making the estimates, forecasts or projections set forth in this Item, including: the suitability of the sample preparation method for assay, the assumptions used by the QP to prepare the data for resource estimation, the assumptions made in creating the dam walls structure, the interpretation of the mineral domain models, the selection of grade interpolation method, sample search and estimation parameters used for grade interpolation, continuity of mineralization and factors used to determine reasonable prospects for economic extraction.

14.1 Introduction

The Project's Maiden MRE was disclosed by STLLR on November 25, 2025, in a news release, titled "STLLR Gold's Hollinger Tailings Project Maiden MRE Provides a Strong Foundation for Exploring Future Short-Term Development Under Ontario's New Recovery of Minerals Regime" and this NI 43-101 Technical Report is in support of that disclosure.

The MRE for the Project has been prepared in accordance with NI 43-101 and following the requirements of Form 43-101F1. The MRE follows the Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Estimation of Mineral Resource and Mineral Reserves Best Practices Guidelines (November 2019) and was classified following CIM Definition Standards for Mineral Resources & Mineral Reserves (May 2014).

The QP for this MRE is Mr. Brian Thomas, P.Geol., an independent QP, as defined under NI 43-101 and an employee of WSP based in Sudbury, Ontario, Canada. The effective date of this MRE is November 25, 2025.

The MRE outlined in the following sections were derived from drill hole data and a lithological model (created in Leapfrog Geo software) provided by STLLR, using a 3D block modelling approach in Datamine Studio RM (Datamine) software.

14.2 Drill Hole Data

The MRE is based entirely upon data provided from a 2025 sonic drilling program, completed by STLLR. The drill hole database consisting of 423 drill holes, totalling approximately 11,230 m of core, was made available on March 20, 2025. 10,717 sampled intervals were assayed for Au. The database also includes lithological, mineralization, and geotechnical measurements and descriptions taken from drill core logs.

The drill hole database volume covers most of the Project area on a nominal 50 m grid (Figure 14.1). Areas not covered include:

- The Northwest corner, for which drilling permits were not available at the time of drilling.
- The Northeast corner, which was actively being used as a dump site during the drilling program.
- Several ponds of shallow (but unmeasured) depth.



Figure 14.1: Plan View of the Drill Hole Collar Locations Relative to the Hollinger Tailings Facility

The database was analyzed for interval errors and out of range values and was reviewed in 3D space to validate the hole locations and de-surveyed hole traces. No issues were identified. To confirm vertical orientation of drill holes the drill contractor used a Reflex EZ-shot downhole orientation survey. The results showed not significant deviation or offset. Because of the nature of the material being drilled, the short vertical lengths of the holes and confirmation from downhole survey measurements, the holes are assumed to be vertical.

The drill hole data is supported by a QA/QC process as described previously in Item 11.0. The QP has also completed independent sample verification as summarized in Item 12.0. STLLR's data collection procedures were found to be mostly consistent with standard industry practice with the possible exception of the sample preparation procedures.

The (length-weighted) histogram of Au in the full assay database (prior to domaining) is shown in Figure 14.2. The bulk of the values follow a slightly positively skewed distribution, and this represents the samples within tailings material. The spike of very low values represents samples in non-tailing material (Item 14.3.1). There was one sample that did not have an Au value.

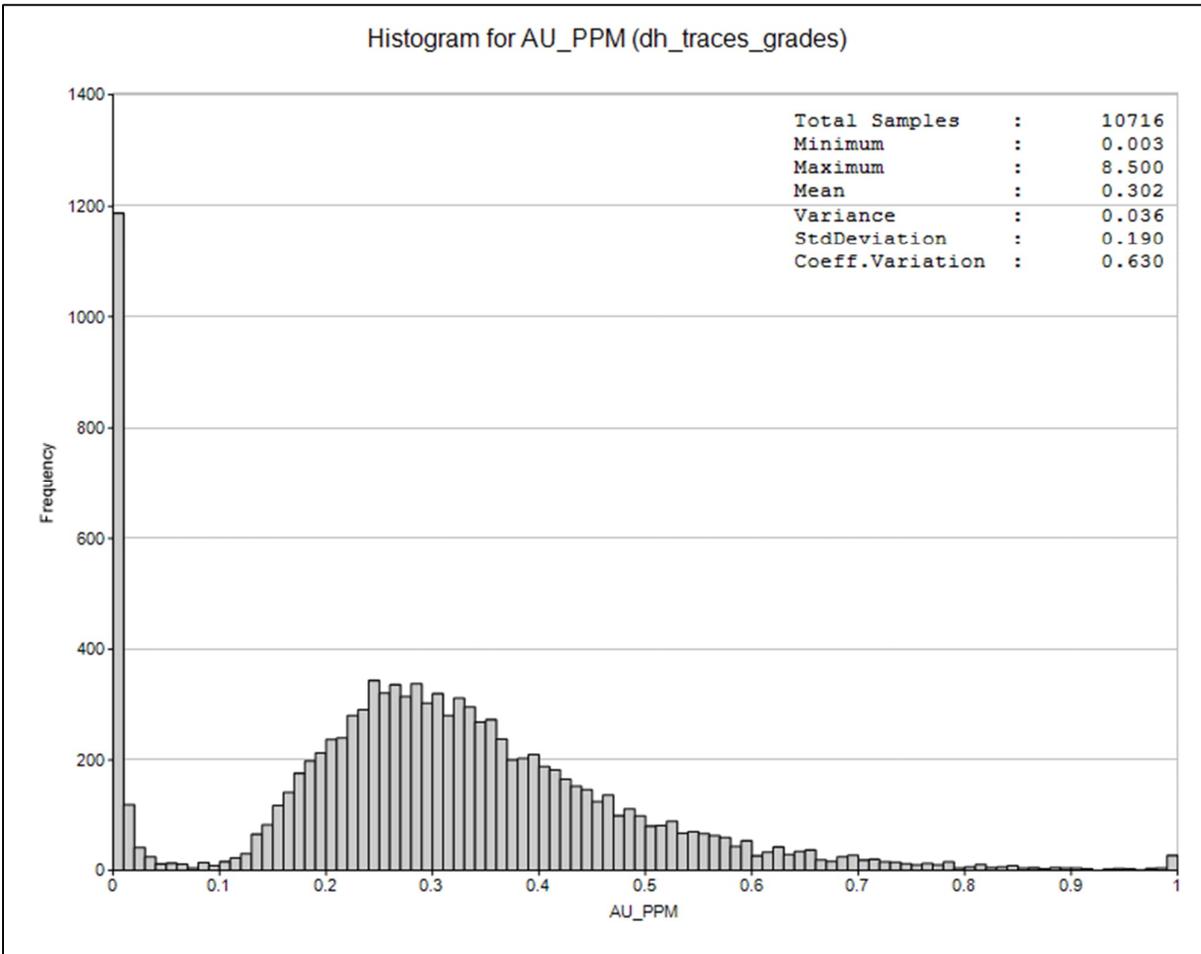


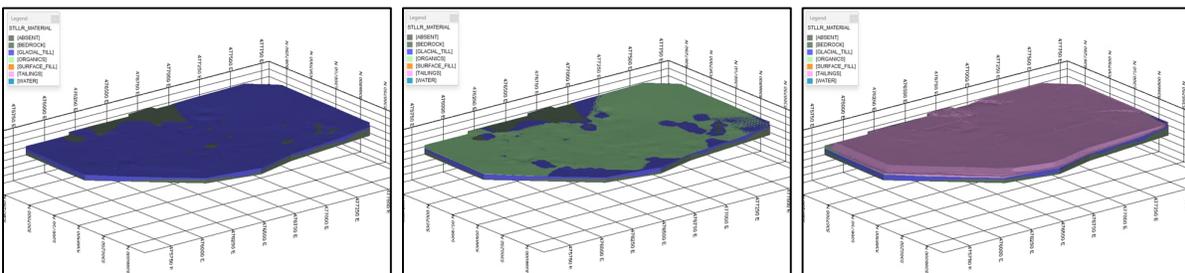
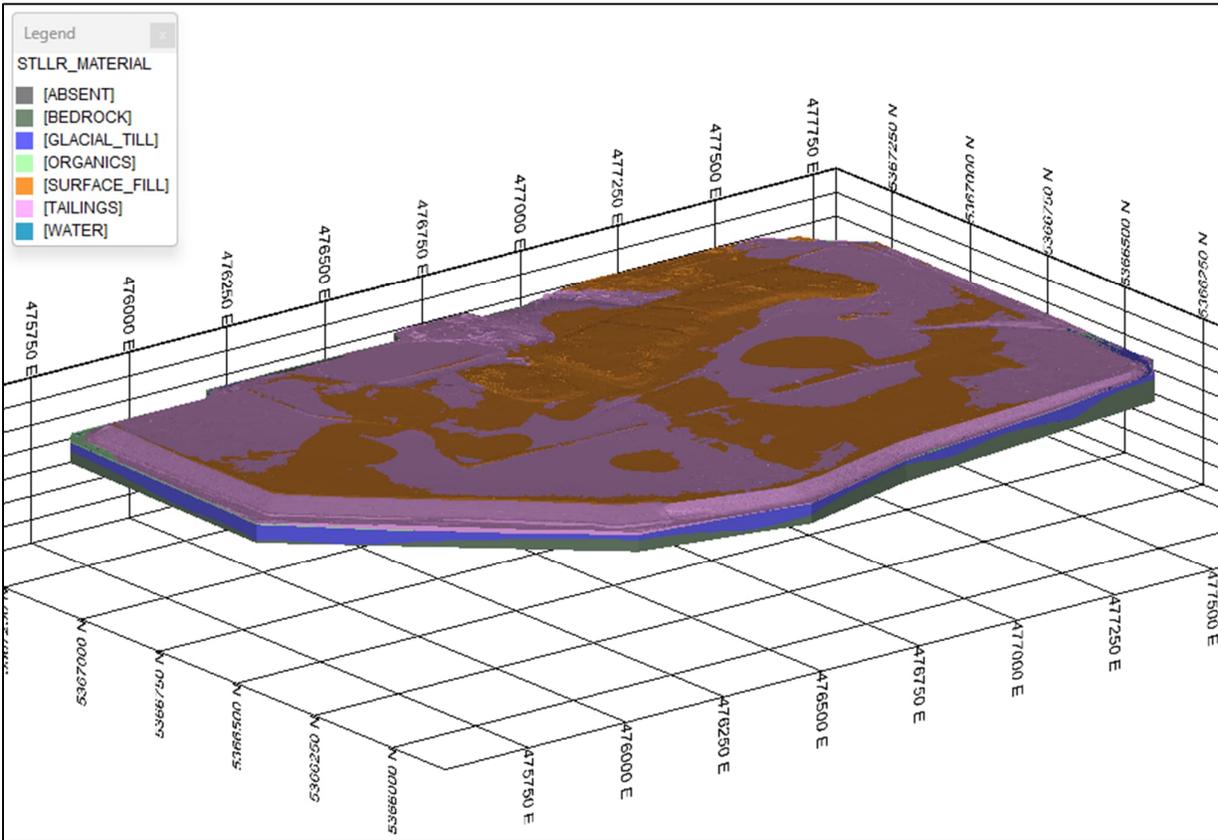
Figure 14.2: Histogram of Au in the full assay database.

14.3 Domaining

Domaining, in preparation for estimation control, consisted of two components, a lithological/material model and a dam structure model. Also, account was made for the ponds.

14.3.1 Lithological/Material Model

The present land surface is capped by landfill materials, vegetation, water, and waste that overlie the tailings deposit. A laterally extensive organic horizon underlies the tailings, followed by glacial till with occasional gravel horizons, and finally the bedrock surface. For the purposes of creating domains these “material” units were identified as Surface Fill, Tailings, Organics, Glacial Till, and Bedrock. STLLR created solid models of these five units using the implicit modelling radial basis function in Leapfrog Geo software. It is the QP’s opinion that the models are representative of the materials recorded in the drill hole logs and the expected trends of the materials.



Top - All combined; bottom left – glacial till on the bedrock; bottom middle – with the organics added; bottom right – with the tailings added

Figure 14.3: Lithological/Material Model (isometric view facing Northeast)

14.3.2 Dam Structure Model

Historical records and images show the state of the tailings dam at various points in time. The primary source of technical information on the dam was the Canadian Mining and Metallurgical Bulletin, Volume 54 in June 1951. An article entitled “Mill Tailing Disposal at Hollinger” by “The Mill Staff” details the history of tailings disposal for the Hollinger Mine and the construction and operation of the tailing facility. The article includes a plan sketch which is shown in Figure 14.4.

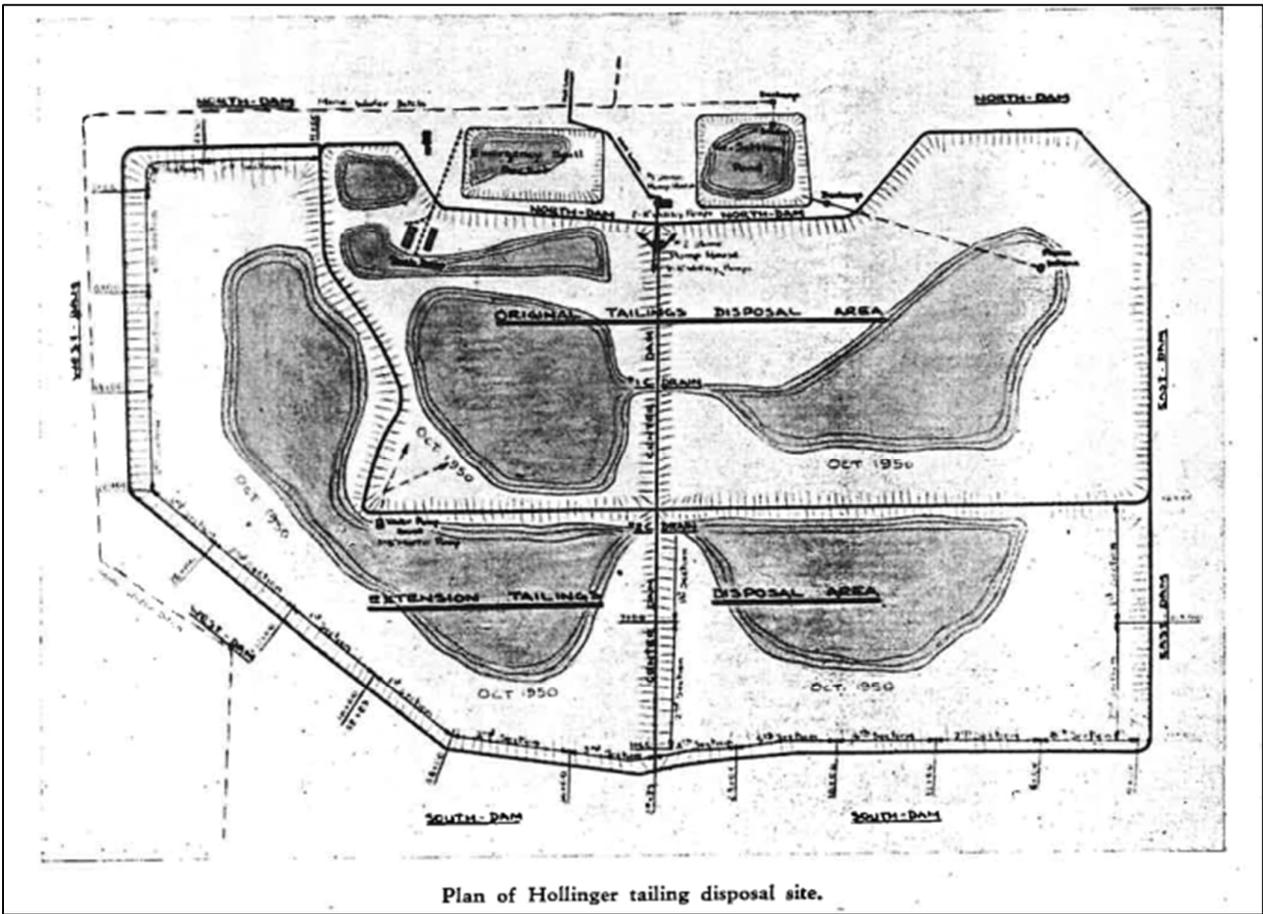


Figure 14.4: Plan Sketch of the Hollinger Tailings Facility from CMM Bulletin, Vol. 54 in June 1951.

The plan sketch shows the exterior walls of the original tailings disposal area (1924 to 1936), the exterior walls of the extension tailings disposal area (1936 to 1969) and some of the internal structure.

Historical images from 1951 and 1969 were georeferenced and compared to a present-day image (Figure 14.5). The red line in the images represents the toe of the current exterior dam wall, traced from the 2024 lidar survey. The exterior dam walls are consistent between the sketch and the images. In the present-day image, roads can be seen on the top of the exterior walls of both the original tailings disposal area and extension tailings disposal area. The major north-south interior walls are also evident and consistent but not with the same level of clarity as the exterior walls. There is also evidence of additional partitioning walls within the original tailings disposal area.

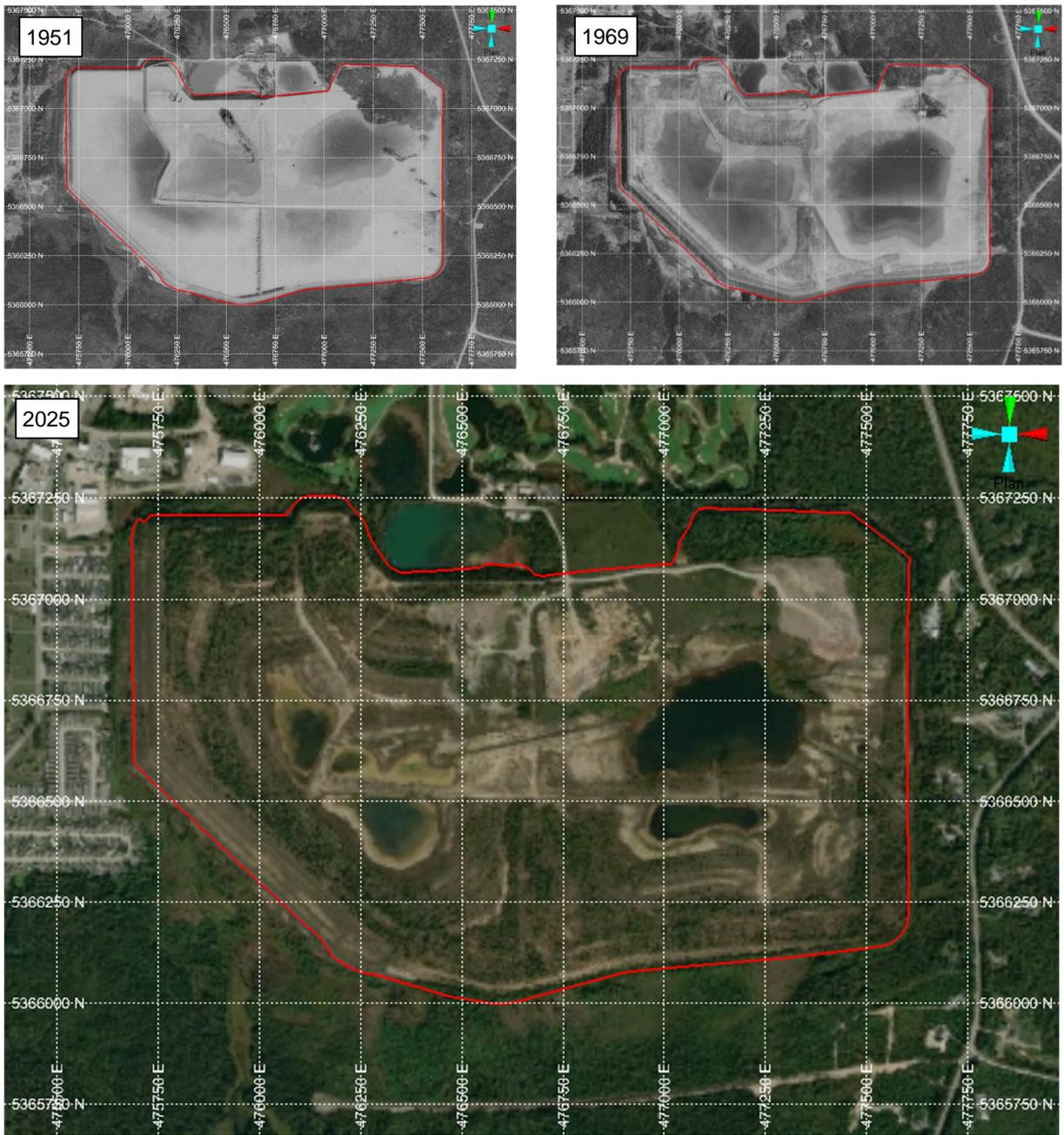


Figure 14.5: Georeferenced Images from 1951, 1969 and 2025

Visual interrogation of the drill hole data relative to the dam structure showed the following:

- Noticeably higher Au grades within the original tailings disposal area exterior walls. This is attributed to a “fine sandy product classified from tailings pulp at the mill” and compacted to make the dam walls.
- No marked elevation in Au grades in the extension tailings disposal area exterior walls. This is attributed to the use of “any material at hand” (which would largely have been the unclassified tailings).
- Elevated Au grades along the major north-south interior walls, but not as evident as in the original tailings disposal area exterior walls.
- Higher Au grades within the original tailings disposal area than within the extension tailings cell area.
- A general trend of increasing Au grade within the extension Tailings Facility toward the exterior walls.

Based on these observations, the following components of the dam structure were modelled:

- Original tailings disposal area exterior walls (labelled as Phase 1 Wall).
- Material inside the original tailings disposal area exterior walls (labelled as Phase 1 Cell).
- Extension tailings disposal area exterior walls (labelled as Phase 2 Wall).
- Material inside the extension tailings disposal area exterior walls (labelled as Phase 2 Cell).

The dam walls were modelled as follows:

- The slope of the exterior walls of the combined/final tailings dam were taken as the existing slopes.
- The slope of the exterior wall of the Phase 1 dam which is inside the total combined/final tailings was modelled at 34° (“the outer face is sloped at 1½ to 1”).
- The interior slope of both the Phase 1 and Phase 2 walls was modelled at 45° (“the inner face is sloped at 1 to 1”).
- The top of the dam walls was modelled at 6 m (“20 feet wide at the top”).

The resulting dam walls are shown in Figure 14.6, relative to the drill holes. The QP reviewed the assumptions in preparing the dam structure model during the site visit and considers them reasonable based on the available information. It should be recognized that there is some uncertainty in the slopes and dimensions of the dam walls and recommendations have been made to address this uncertainty. There is also some evidence of localized collapse in the Phase 1 wall but there is insufficient information to adjust the dam structure model to account for this. There is evidence of a north-south dividing wall in the central region but details on the exact location and specifications were limited and therefore this wall was not modeled.

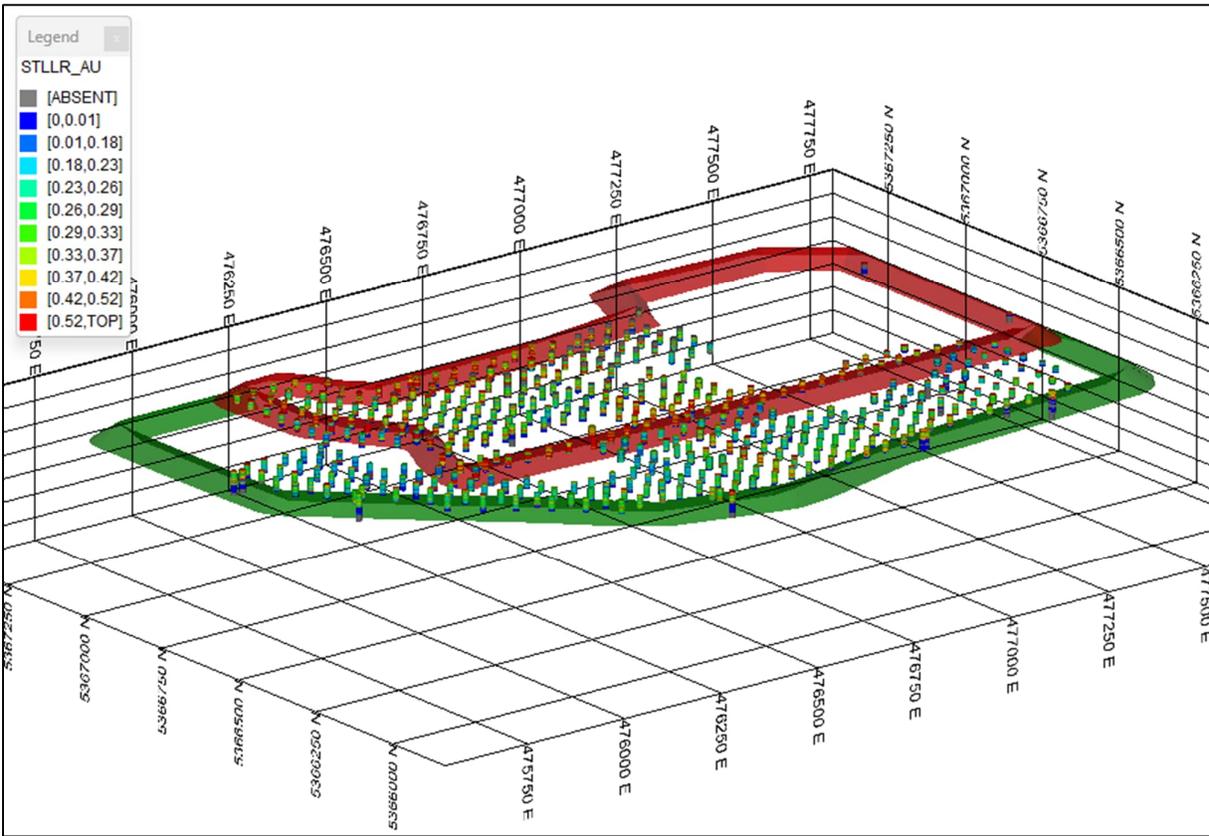


Figure 14.6: Dam Exterior Walls (Phase 1 is red and Phase 2 is green).

14.3.3 Ponds

As noted in Item 14.2, there are several ponds on the site where drilling was not possible. No information on depth was available on the ponds, so simple assumptions were made to account for the pond volumes. Figure 14.7 shows the pond locations relative to a 2025 georeferenced image. For each of the ponds, the outer boundary is the 0-depth contour and then each contour within the outer boundary is 1 m in depth. One of the ponds has an assumed depth of 2 m, three have an assumed depth of 3 m and the largest pond has an assumed depth of 5 m. There is uncertainty around these assumptions which could result in minor adjustments to the MRE once actual depths have been determined.

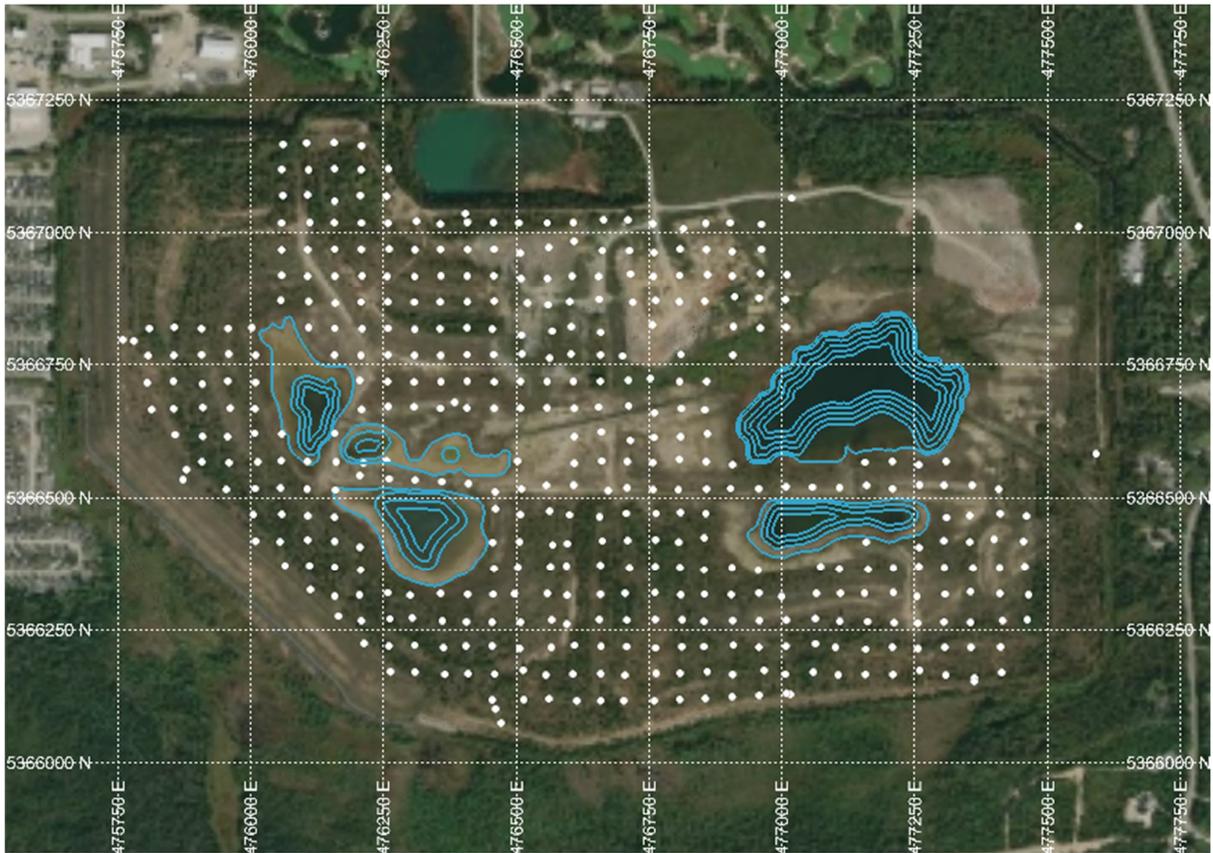


Figure 14.7: Pond contours.

14.4 Exploratory Data Analysis

The drill holes were domained using the lithological/material model (MATERIAL=SURFACE_FILL, TAILINGS, ORGANICS, GLACIAL_TILL and BEDROCK) and dam structure model (OBJECT=PHASE1_CELL, PHASE1_WALL, PHASE2_CELL and PHASE2_WALL). Note that the OBJECT domain is only assigned where MATERIAL=TAILINGS.

When examining the results of the dam structure domaining, it was noted that there were several instances where there were high grade samples very close to the Phase 1 wall. Small changes to the dam wall location and/or wall slope and these samples would be included in the Phase 1 wall volume. If these samples were not addressed it would result in high-grade spreading in the Phase 2 cell, counter to the grade trends observed in the Phase 2 cell volume. It was decided to manually re-code these samples. This affected 70 samples in 22 holes.

14.4.1 Descriptive Statistics

The (length-weighted) histogram of Au in the Tailings is shown in Figure 14.8. As previously noted, the values follow a slightly positively skewed distribution, with a mean value of 0.35 g/t. The (length-weighted) histogram of Au in the Organics and Glacial Till is shown in Figure 14.9. There are 92 recorded assays in the Organics that have a mean value of 0.24 g/t and 1,537 recorded assays in the Glacial Till that have a mean value of 0.03 g/t. The Au in the Organics and Glacial Till is attributed to contamination material from the Tailings. There are two recorded assays in the Surface Fill, including one highly anomalous Au value of 8.5 g/t, which is considered due to external contamination and has no relationship to the tailings material. This sample was removed from the database before proceeding.

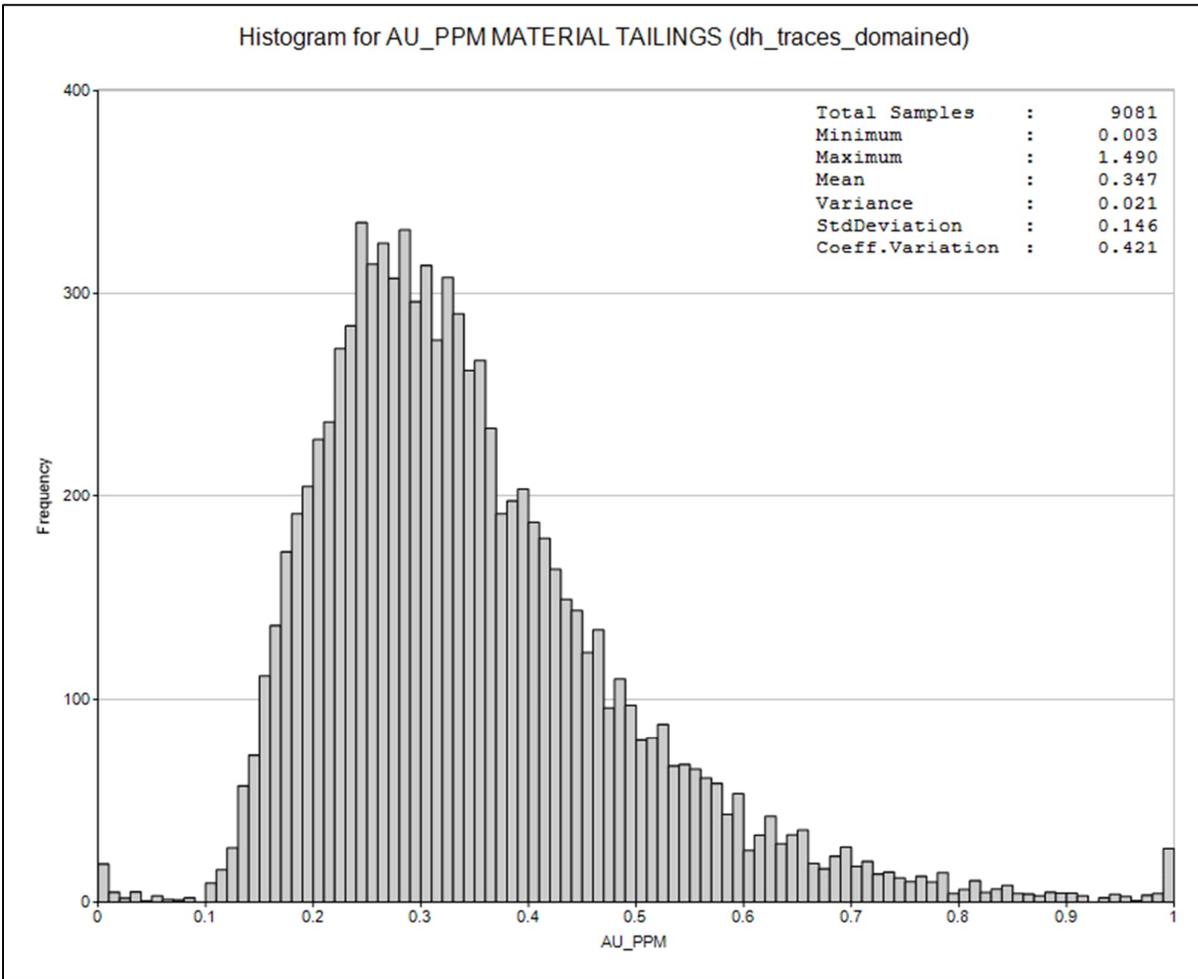


Figure 14.8: Histogram of Au in the Tailings

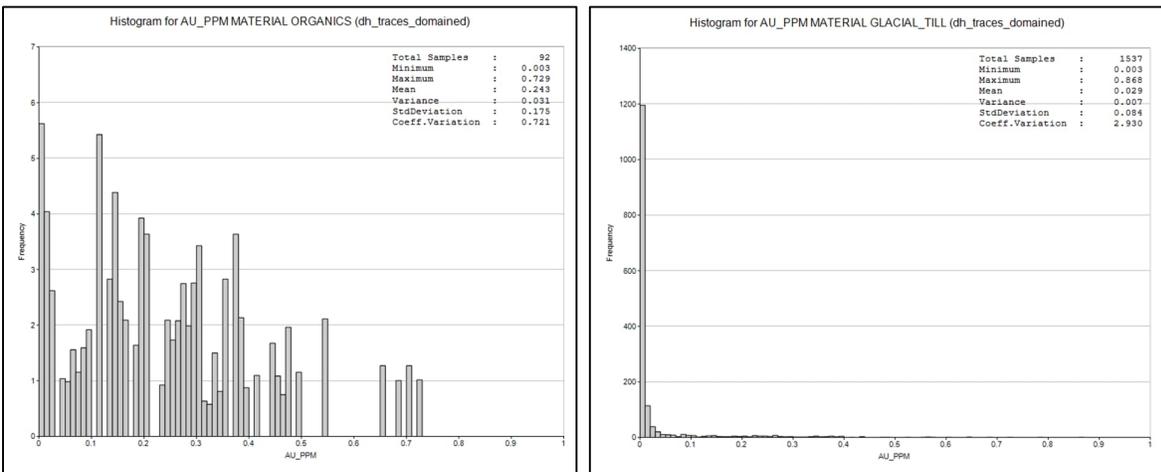


Figure 14.9: Histograms of Au in the Organics (left) and Glacial Till (right)

The (length-weighted) statistics of Au for the dam structure components in the Tailings are shown in Table 14.1. The number of samples in the Phase 2 wall is low, and they are poorly distributed throughout the Phase 2 wall volume. This fact, combined with the method of their construction (Item 14.3.2), led to the decision to combine the Phase 2 wall and cell for the purpose of estimation.

Table 14.1 shows some intervals within the Tailings have not been sampled and assayed. Interrogation of the database indicated these were intervals where core was lost or insufficient core was available for assay. For this reason, these samples were left as “missing”; and therefore, did not have any influence on the grade estimation.

Table 14.1: Sample Statistics for the Dam Structure Components

OBJECT	Intervals	Samples	Missing	Minimum	Maximum	Mean	Variance	St. Dev.	CV
PHASE1_CELL	3,537	3,514	23	0.0025	1.435	0.387	0.018	0.134	0.347
PHASE1_WALL	785	782	3	0.006	1.210	0.543	0.022	0.149	0.275
PHASE2_CELL	4,508	4,487	21	0.0025	1.490	0.289	0.014	0.116	0.403
PHASE2_WALL	302	298	4	0.0025	0.883	0.330	0.011	0.103	0.313

The (length-weighted) histograms of Au in the Tailings for the Phase 1 wall, Phase 1 cell and Phase 2 combined wall/cell are shown in Figure 14.10, Figure 14.11, and Figure 14.12, respectively.

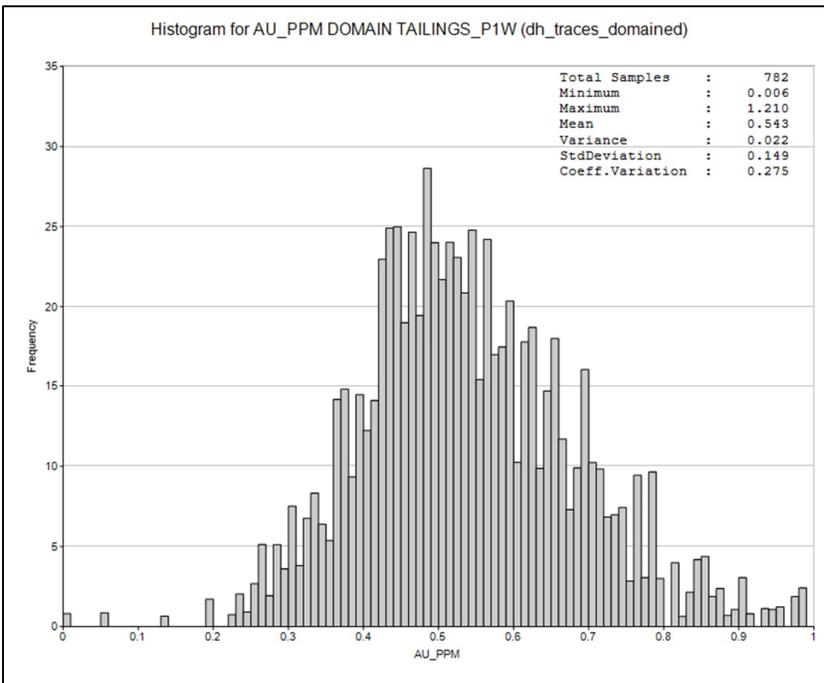


Figure 14.10: Histogram of Au in the Tailings Phase 1 Wall

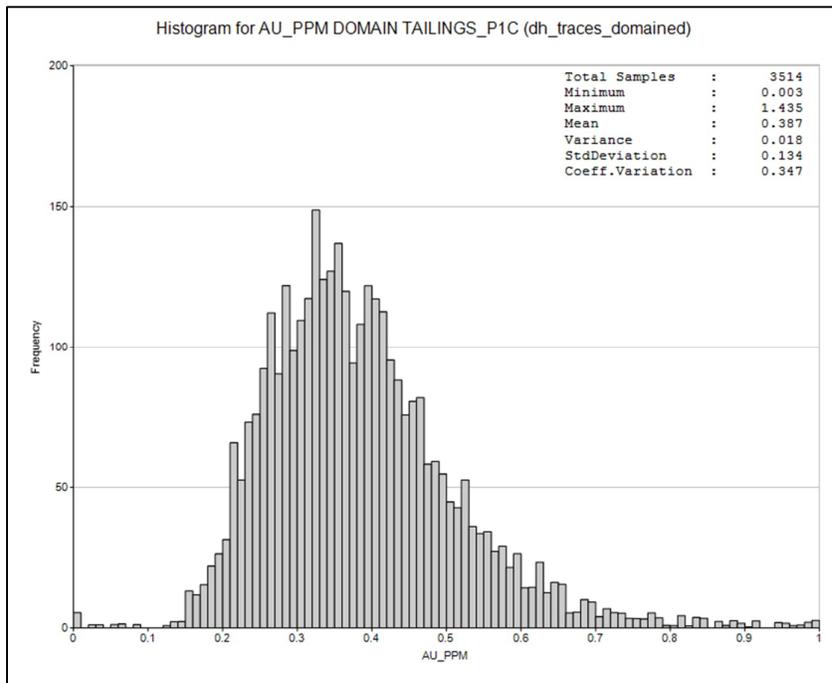


Figure 14.11: Histograms of Au in the Tailings Phase 1 Cell

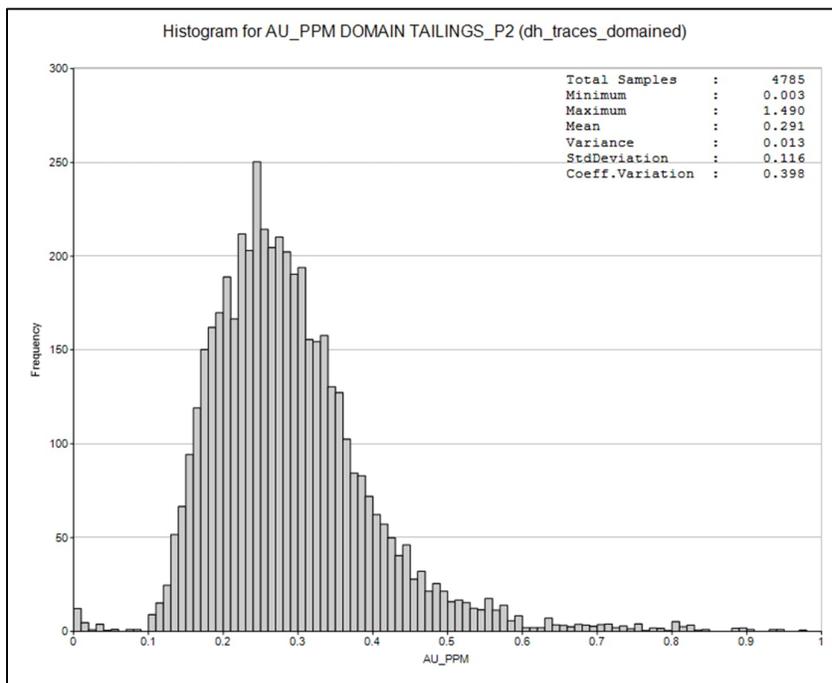


Figure 14.12: Histograms of Au in the Tailings Phase 2 Wall and Cell Combined

14.4.2 Outlier Analysis

A probability plot of Au and XY scatterplot of Au versus sample length (within the Tailings material) were used to assess the requirement for capping (Figure 14.13). A cap of 1.3 g/t was applied (prior to compositing), which impacted only five samples from three holes. The process of capping did not change the mean, length-weighted Au grade to the third decimal place (0.347 g/t) but resulted in a minor reduction in the coefficient of variation (CV) from 0.421 to 0.420.

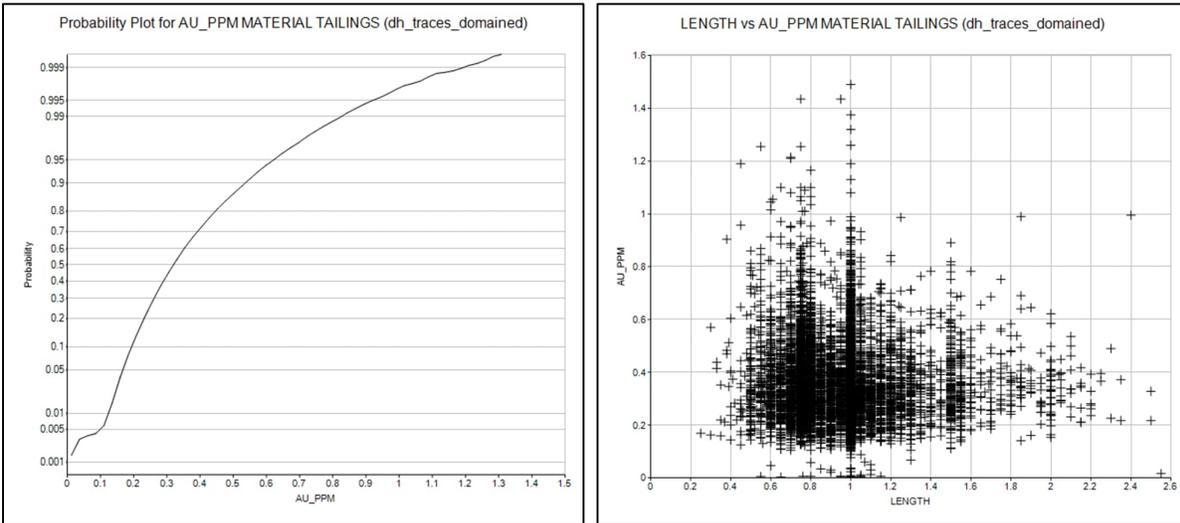


Figure 14.13: Probability Plot of Au and Length/Au Scatter Plot (Tailings Material Only)

14.4.3 Compositing

The histogram of sample length in the Tailings is shown in Figure 14.14. Based on this, samples were composited to 1 m lengths. Bench compositing was used to align the composites with model blocks.

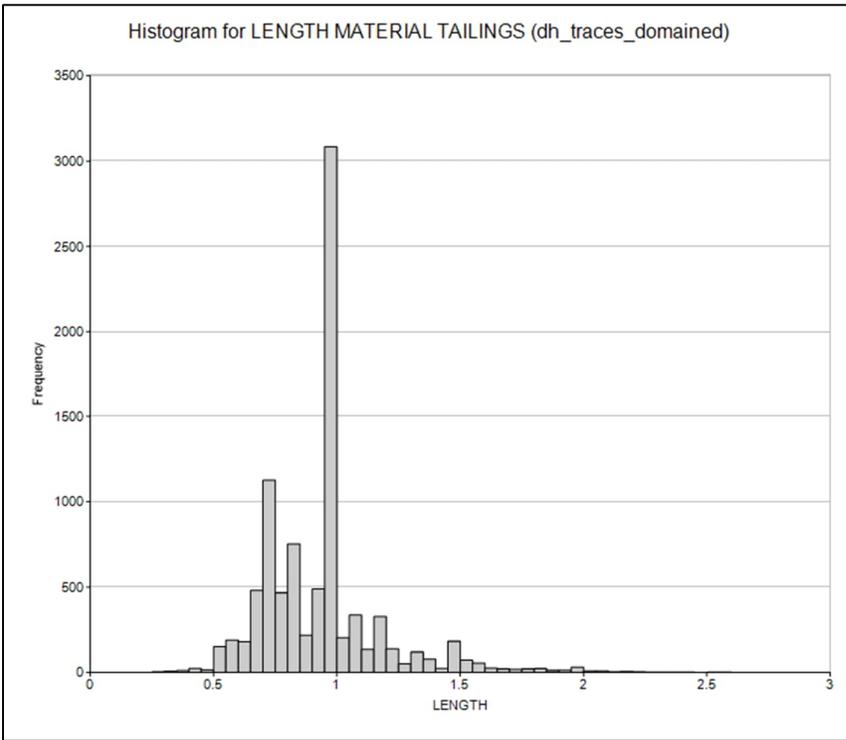


Figure 14.14: Histogram of sample length (Tailings Material Only)

Table 14.2 summarizes the descriptive statistics for the populations of original and composited sample data. The process of compositing did not change the mean, length-weighted Au grade to the third decimal place but resulted in reductions in the CV.

Table 14.2: Comparison of Sample Statistics

DOMAIN	Type	Intervals	Samples	Missing	Min. Au (g/t)	Max. Au (g/t)	Mean Au (g/t)	Variance	St. Dev.	CV
TAILINGS_P1 C	Samples	3,537	3,514	23	0.0025	1.435	0.387	0.018	0.134	0.347
TAILINGS_P1 C	Composites	3,329	3,325	4	0.0025	1.260	0.387	0.015	0.122	0.314
TAILINGS_P1 W	Samples	785	782	3	0.006	1.210	0.543	0.022	0.149	0.275
TAILINGS_P1 W	Composites	792	791	1	0.058	1.195	0.543	0.018	0.135	0.249
TAILINGS_P2	Samples	4,810	4,785	25	0.0025	1.490	0.291	0.013	0.116	0.398
TAILINGS_P2	Composites	5,068	5,061	7	0.0025	1.300	0.291	0.012	0.108	0.371

14.4.4 Bulk Density

A total of 67 dry density measurements (from 15 holes) were available for analysis. The locations of the measurements are shown in Figure 14.15 and a histogram of the measurement is shown in Figure 14.16. Of the holes containing measurements, four are in the Phase 1 wall, two are in the Phase 1 cell, eight are in the Phase 2 wall and one is in the Phase 2 cell. The number and distribution of measurements is poor and needs to be improved. This is addressed in Recommendations (Item 14.6.2).

With limited data, only two basic conclusions can be drawn for the measurements. They are:

- The highest density is in the Phase 1 wall.
- There is a rough trend of density increasing with depth, possibly due to compaction.

These conclusions were used to establish density in the block model (Item 14.5.6).



Figure 14.15: Location of Dry Density Measurements

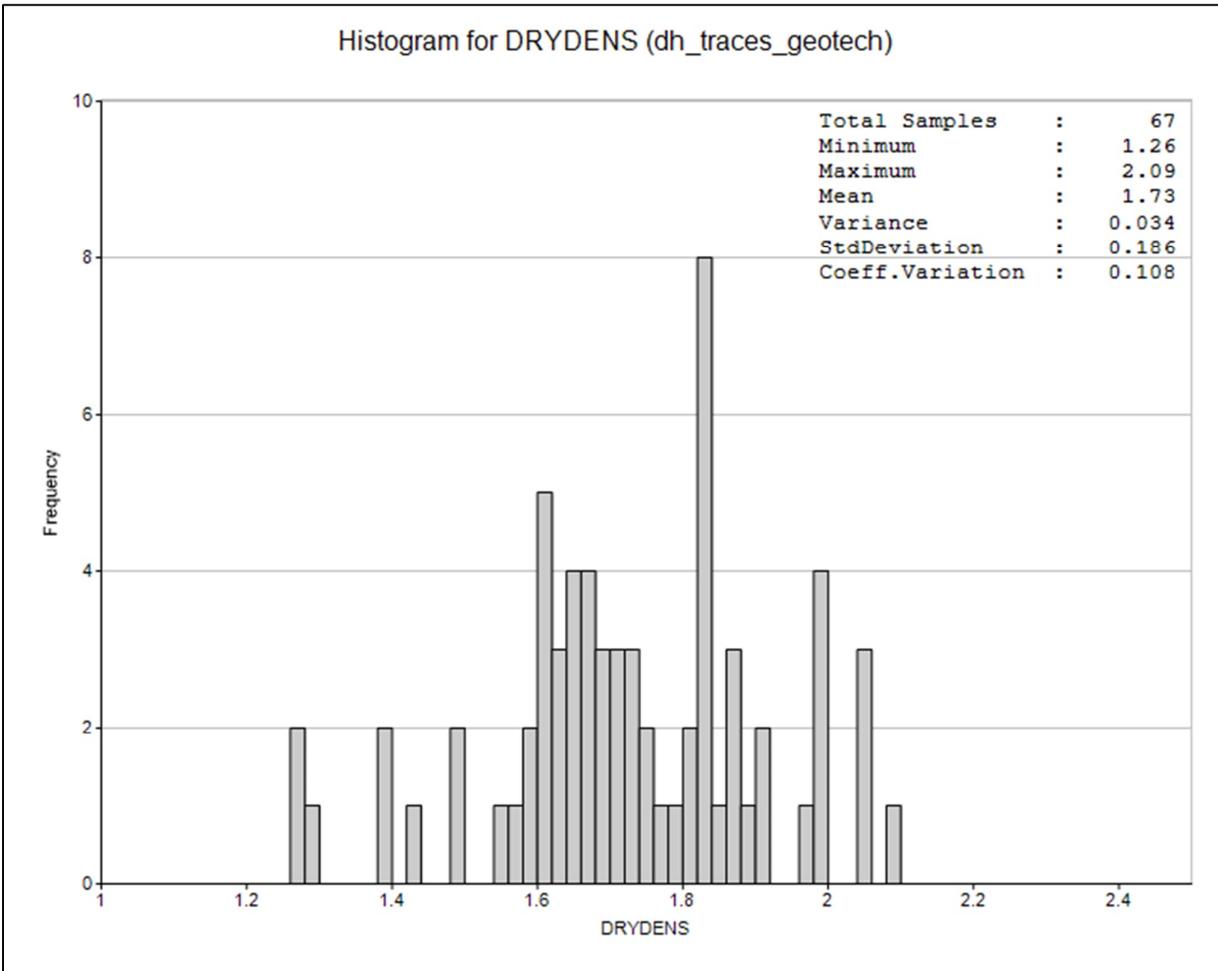


Figure 14.16: Histogram of Dry Density Measurements

A full description of the density measurement process is outlined in Item 11.0.

14.5 Block Model and Resource Estimation

14.5.1 Assessment of Spatial Grade Continuity

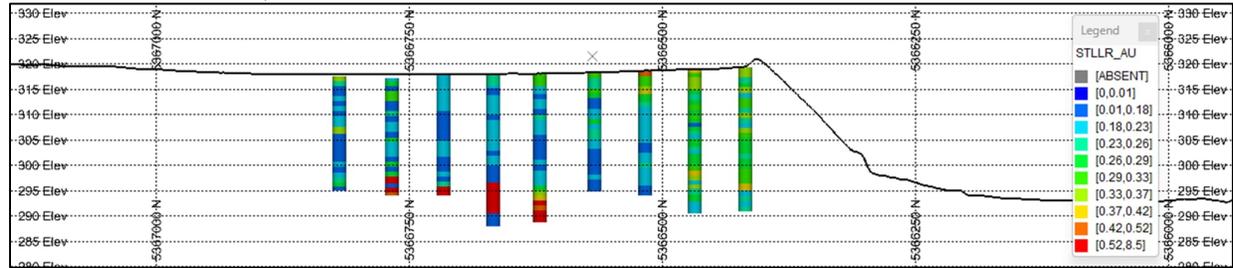
The continuity of Au grade was assessed by examining North-South and East-West sections. The higher-grade values in the Phase 1 wall were evident and captured by the dam structure model (Item 14.1). There is some “stratification” in the Phase 1 wall, but this is unrelated to the “stratification” in the Phase 1 cell. In many areas there is notable lateral stratification of grade within both the Phase1 cell and Phase 2 cell. Estimation controls were chosen to preserve that stratification.

Figure 14.17 and Figure 14.18 show the Au grade on drill holes in North-South sections from 476,000 E to 477,400 E (in 200 m increments). When viewing the sections, note the following:

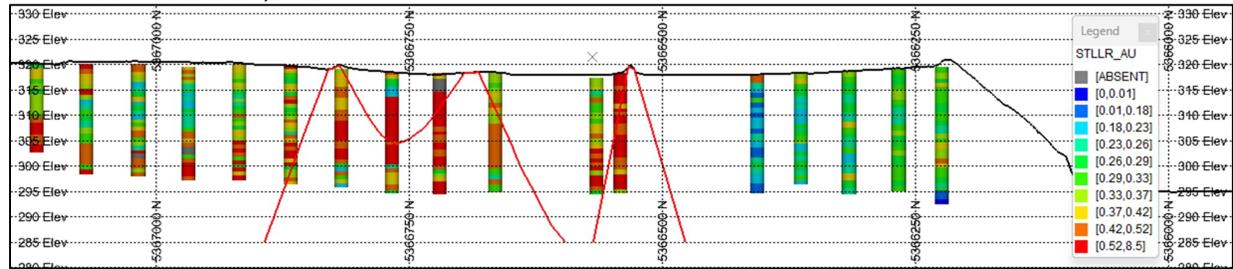
- The horizontal extent of the deposit is significantly greater than the vertical extent, so a 5-fold vertical exaggeration has been used to provide greater clarity. This will exaggerate vertical differences and distort slope angles of the dam walls.
- The section width is 50 m (plus/minus 25 m).

- The red lines are slices through the Phase 1 wall construction solids.

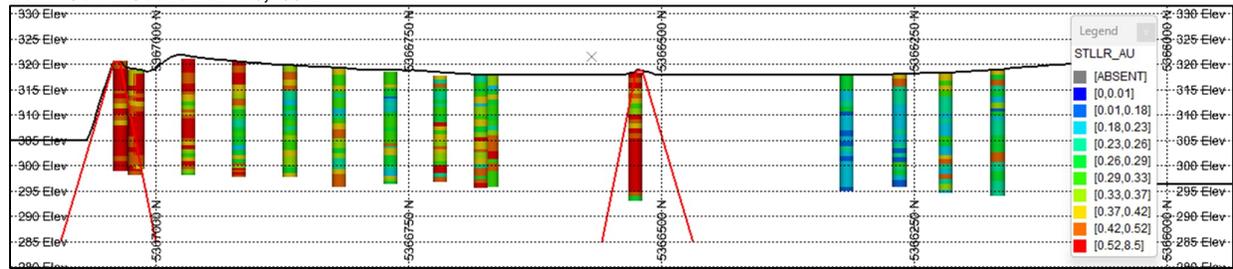
North-South Section at 476,000 E



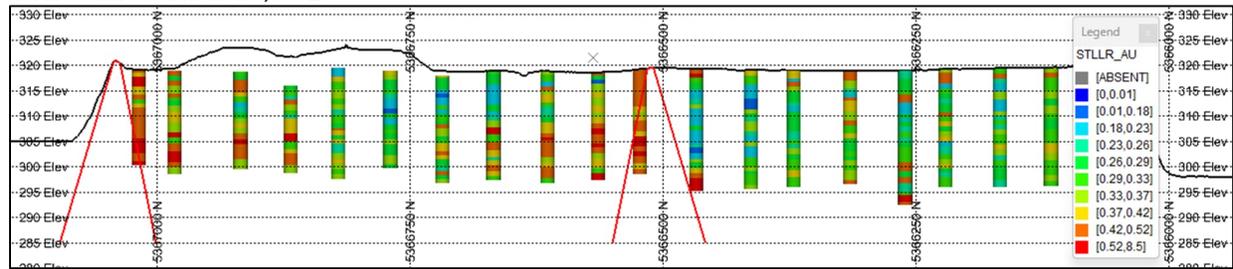
North-South Section at 476,200 E



North-South Section at 476,400 E



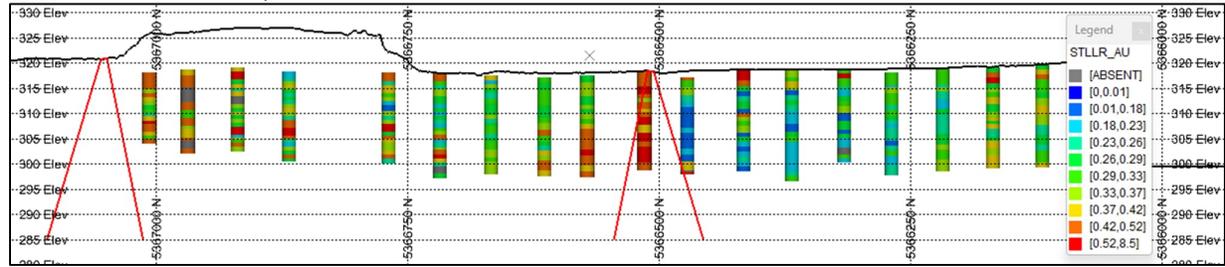
North-South Section at 476,600 E



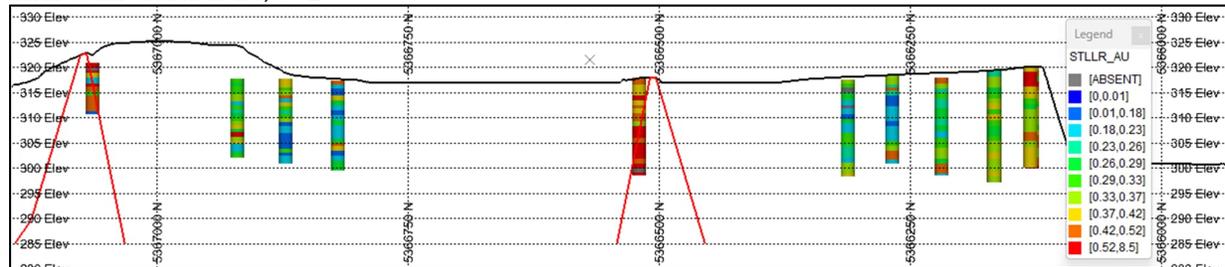
Note: All images in this Figure have a 5-fold vertical exaggeration. 476,000 E, 476,200 E, 476,400 E, 476,600 E, showing Au grade on drill holes

Figure 14.17: North-South Sections

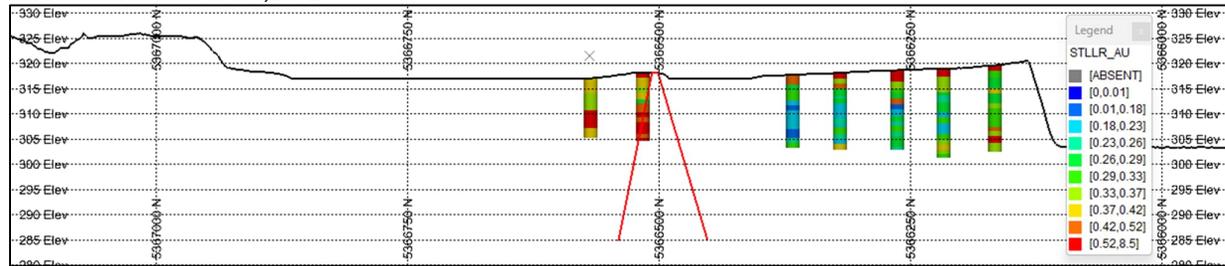
North-South Section at 476,800 E



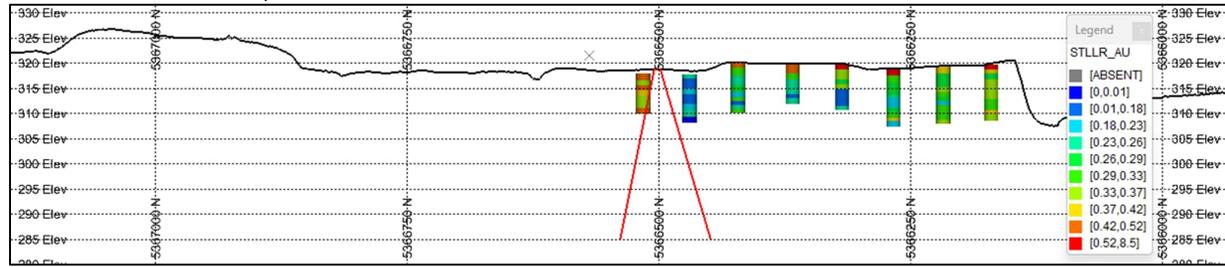
North-South Section at 477,000 E



North-South Section at 477,200 E



North-South Section at 477,400 E



Note: All images in this Figure have a 5-fold vertical exaggeration. 476,800 E, 477,000 E, 477,200 E, 477,400 E, showing Au grade on drill holes

Figure 14.18: North-South Sections

14.5.2 Block Model Definition

The volume definition for the block model is summarized in Table 14.3. Block shape and size is typically a function of the geometry of the deposit, density of sample data, and expected smallest mining unit (SMU). On this basis, a parent block size of 10 m (E-W) by 10 m (N-S) by 1 m (Elevation) was chosen. This level of granularity was considered necessary to preserve the trends observed in the drill hole data. Additional work to establish the mining blocks will be done in the Preliminary Economic Assessment. Sub-blocking to 2.5 m by 2.5 m by 0.5 m was permitted at lithological/material contacts and dam structure contacts.

Table 14.3: Block Model Volume Definition

Direction	Minimum	Maximum	Block Size (m)	Number of Blocks
Easting	475,600	477,700	10	210
Northing	5,365,950	5,367,300	10	135
Elevation	280	350	1	70

Note: Coordinates in UTM NAD 83

14.5.3 Interpolation Methods

Inverse Distance squared (ID²) was the grade interpolation method chosen as the basis of the 2025 MRE. This method assigns estimation weights to the samples within the search volume relative to the distance of the sample data from the centre of the block. The closer the sample, the higher the weights, as described in the following formula where p is defined as the power of 2.

$$v_1 = \frac{\sum_{i=1}^n \frac{1}{d_i^p} v_i}{\sum_{i=1}^n \frac{1}{d_i^p}}$$

Nearest Neighbour (NN), and Inverse Distance cubed (ID³) were estimated for global comparison and validation purposes but were not used for final resource reporting.

14.5.4 Search Strategy

The search estimation parameters used for grade estimation are summarized in Table 14.4.

A two pass, elliptical search strategy was utilized, with individual controls for the Phase 1 wall, Phase 1 cell and combined Phase 2 wall/cell. No discernable trend in the horizontal plane was identified, so the Northing and Easting search distances were the same. For the Phase 1 cell and Phase 2 cell, the elevation search distance was small to preserve the horizontal stratification detailed in Item 14.5.1. For the Phase 1 cell the elevation search distance was larger to reflect the lesser stratification and smaller sample population. Minimum and maximum number of samples, and maximum samples per drill hole, were chosen to prioritize horizontal continuity over vertical continuity and to ensure at least two drill holes were used in any estimate.

Table 14.4: Search Volume Controls Used for Au Grade Estimation

DOMAIN	Pass	North	East	Elevation	Min. No. of Samples	Max. No. of Samples	Max. No. of Samples from a hole
TAILINGS_P1C	1	70	70	3	6	12	3
TAILINGS_P1C	2	175	175	7.5	4	12	3
TAILINGS_P1W	1	70	70	35	6	12	3
TAILINGS_P1W	2	175	175	87.5	4	12	3
TAILINGS_P2	1	70	70	3	6	12	3
TAILINGS_P2	2	175	175	7.5	4	12	3

14.5.5 Model Validation

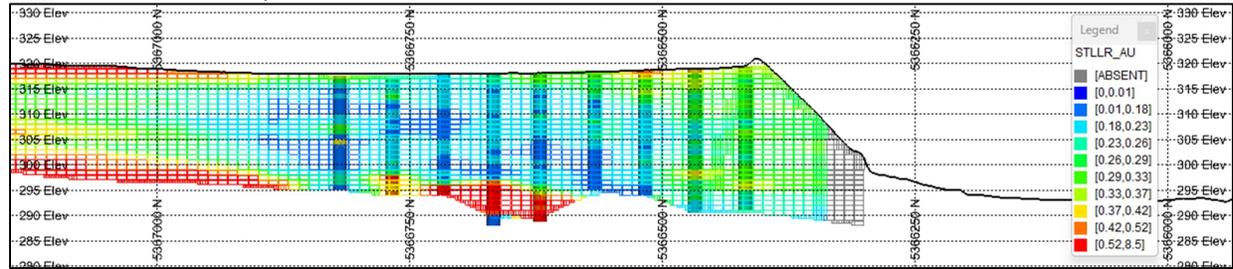
The block model validation process included visual comparisons between block estimates and composite grades in plan, North-South section, and East-West section along with a global comparison of mean grades and swath plots.

Figure 14.19 and Figure 14.20 provide comparisons of the block model Au estimates and Au composite grades in North-South sections from 476,000 East to 477,400 East (in 200 m increments). When viewing the sections, note the following:

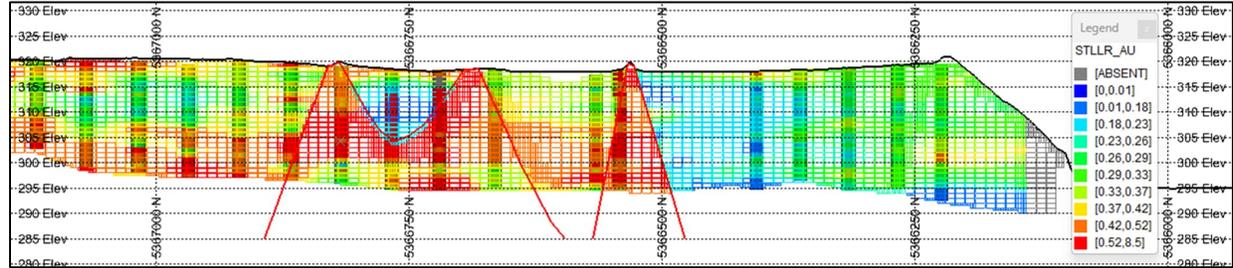
- The horizontal extent of the deposit is significantly greater than the vertical extent, so a 5-fold vertical exaggeration has been used to provide greater clarity. This will exaggerate vertical differences and distort slope angles of the dam walls.
- The section width is 50 m (plus/minus 25 m).
- The red lines are slices through the Phase 1 wall construction solids.
- Grey blocks are those for which insufficient samples were available to make an estimate.
- Empty space between the top of the (tailings) blocks and the topography (black line) represents either surface fill or ponds.

No material grade bias issues were identified in the estimates, and the block grades compared well to, and reflect the trends seen in, the composite data.

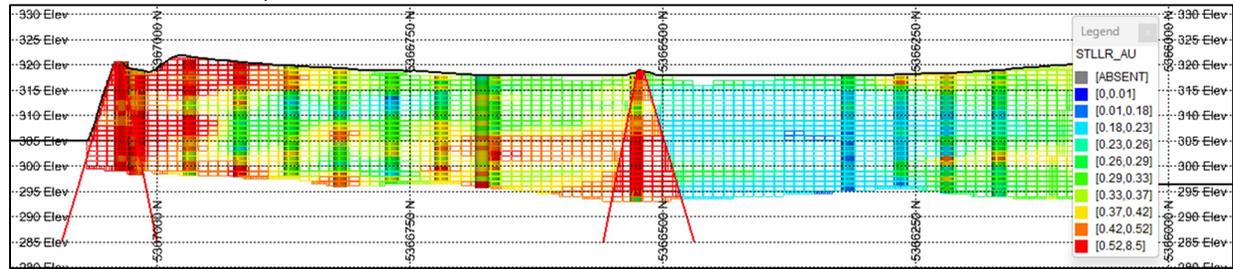
North-South Section at 476,000 E



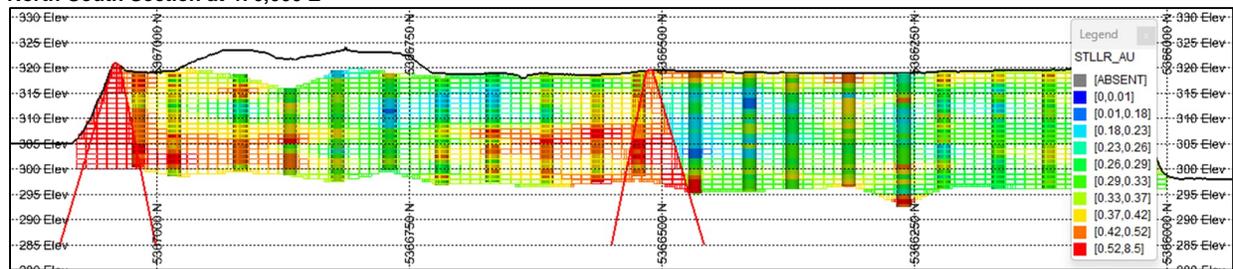
North-South Section at 476,200 E



North-South Section at 476,400 E



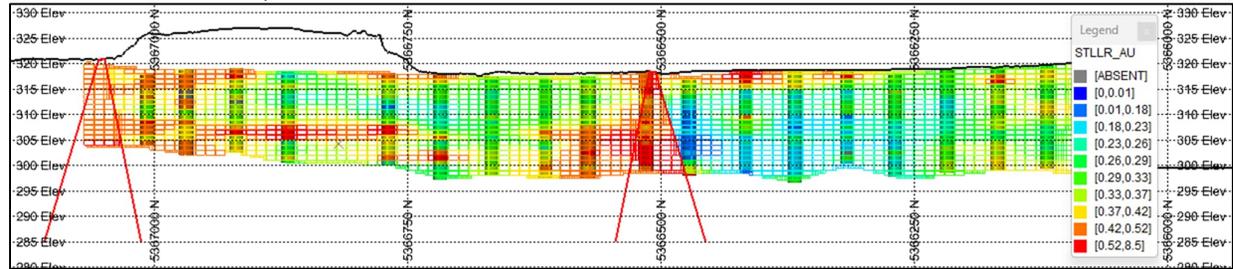
North-South Section at 476,600 E



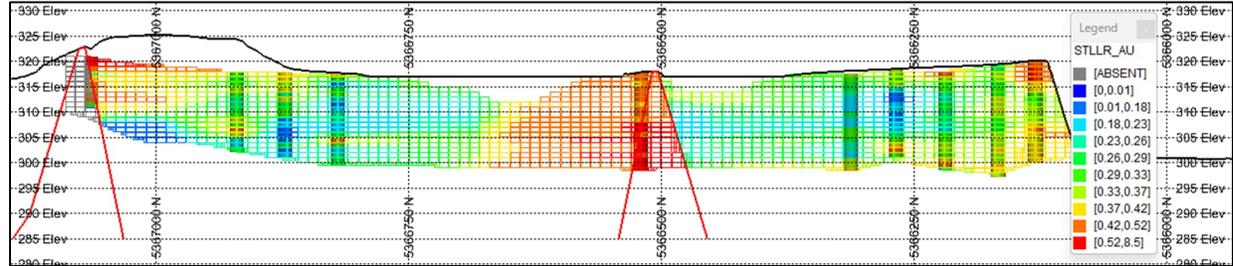
Note: All images in this Figure have a 5-fold vertical exaggeration. 476,000 E, 476,200 E, 476,400 E, 476,600 E, showing Au grade in the block model relative to the drill hole composites.

Figure 14.19: North-South Sections

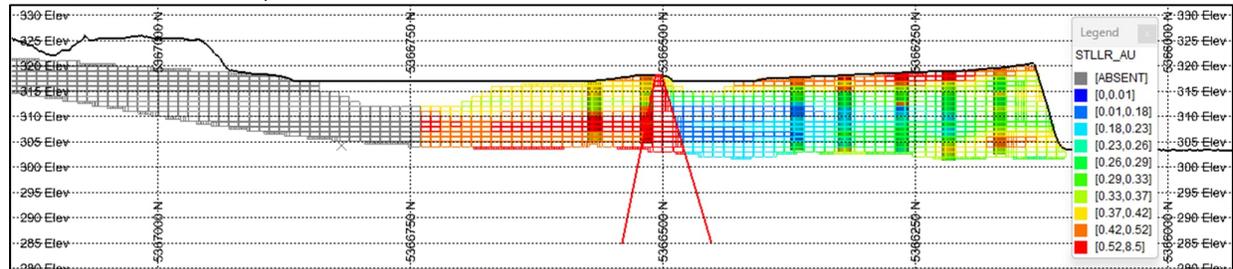
North-South Section at 476,800 E



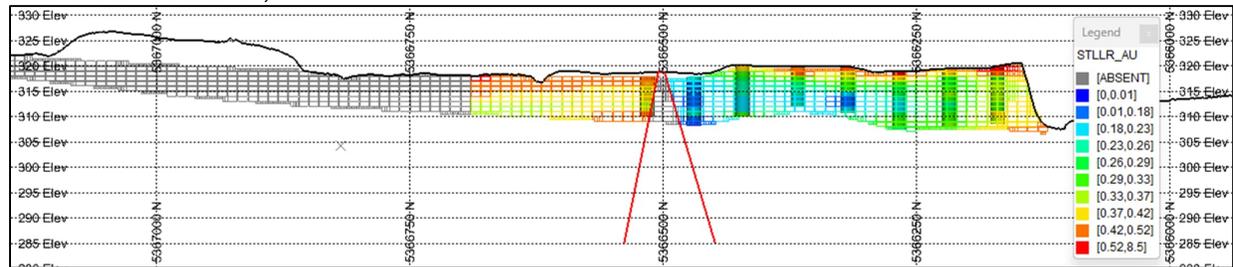
North-South Section at 477,000 E



North-South Section at 477,200 E



North-South Section at 477,400 E



Note: All images in this Figure have a 5-fold vertical exaggeration. 476,800 E, 477,000 E, 477,200 E, 477,400 E, showing Au grade in the block model relative to the drill hole composites.

Figure 14.20: North-South Sections

Global statistical comparisons between the composite samples, NN estimates, ID³ estimates and the final estimates (ID²) were compared to assess global bias, where the NN model estimates represent de-clustered composite data. Clustering of the drill hole data can result in differences between the global means of composites and NN estimates. The results summarized in Table 14.5 indicate that no material global bias was found in the block model.

Table 14.5: Statistical Comparison of Global Mean Au Grades

DOMAIN	Composite Mean (g/t)	NN Mean (g/t)	ID² Mean (g/t)	ID³ Mean (g/t)	ID² Mean Difference (%)	ID³ Mean Difference (%)
TAILINGS_P1C	0.387	0.383	0.382	0.382	-0.249	-0.165
TAILINGS_P1W	0.543	0.540	0.550	0.550	1.887	1.811
TAILINGS_P2	0.291	0.290	0.290	0.290	-0.129	-0.085

Notes: The comparison is for all blocks in the model irrespective of classification.

Swath plots of Au grades were generated from 50-m slices in the North-South direction (Figure 14.21) and the East-West direction (Figure 14.22). The swath plots compare the ID² model grades to the NN model grades (de-clustered composite grades) and the drill hole composite grades. Review of all the swath plots did not identify any significant bias in the model that is material to the MRE, as there was good agreement between the de-clustered composites (NN model) and the final ID² model grades.

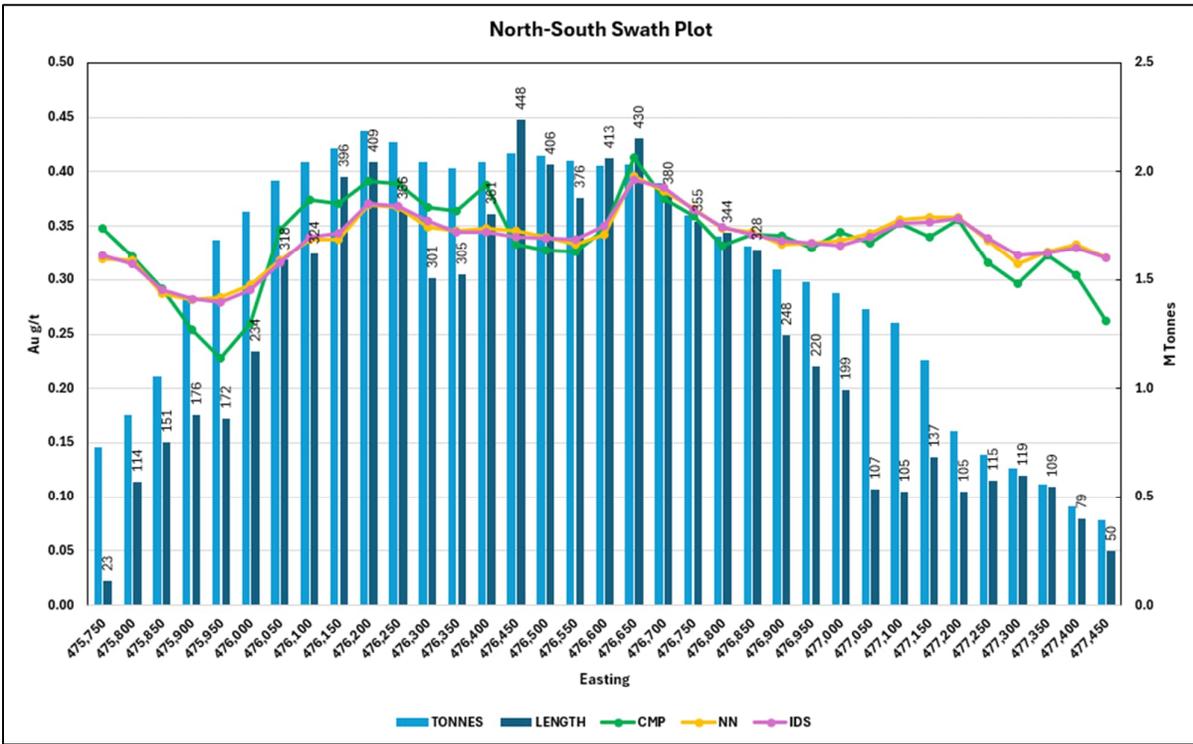


Figure 14.21: North-South Swath Plot

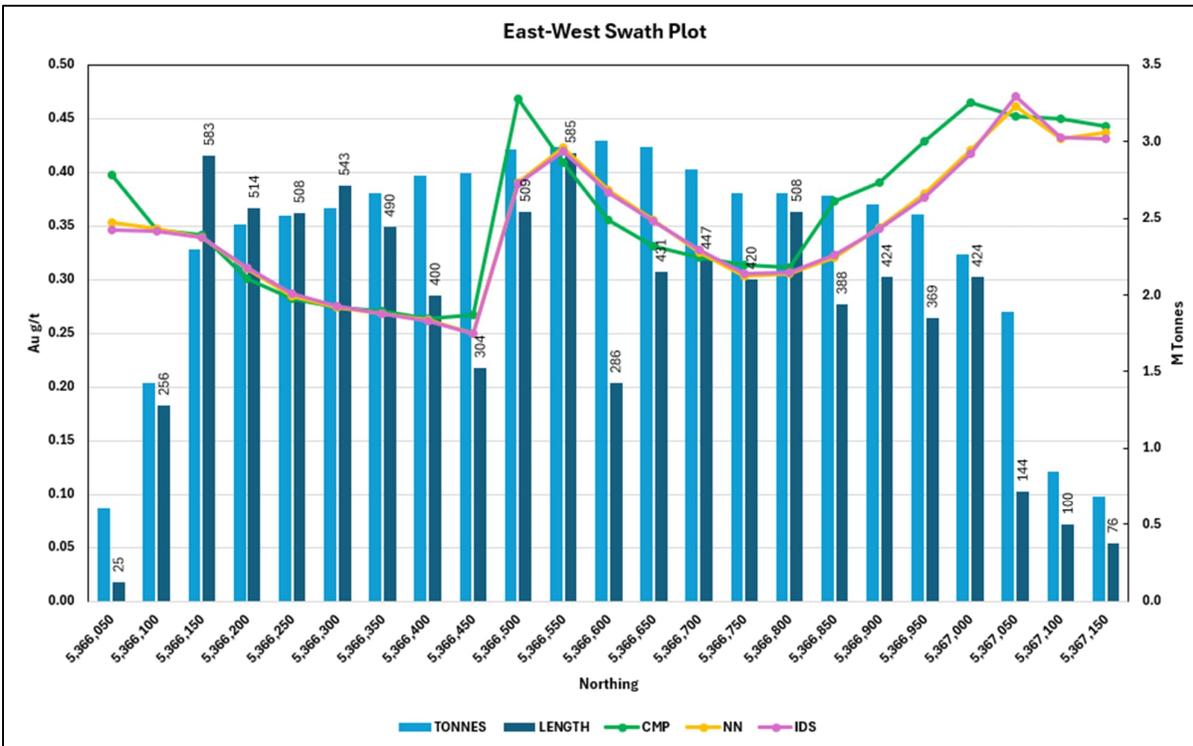


Figure 14.22: East-West Swath Plot

14.5.6 Bulk Density

Item 14.4.4 discussed the limited dry density measurements. Based on the information available, the following simple rules were adopted to attempt to account for varying levels of compaction with depth:

- For the Phase 1 wall, density was set to 1.9 g/cm³.
- For the Phase 2 wall, density was set to 1.8 g/cm³.
- For the Phase 1 cell and Phase 2 cell:
 - Blocks below 310 m elevation were given a density of 1.8 g/cm³.
 - Blocks between 310 m and 315 m elevation were given a density of 1.7 g/cm³.
 - Blocks above 315 m elevation were given a density of 1.6 g/cm³.

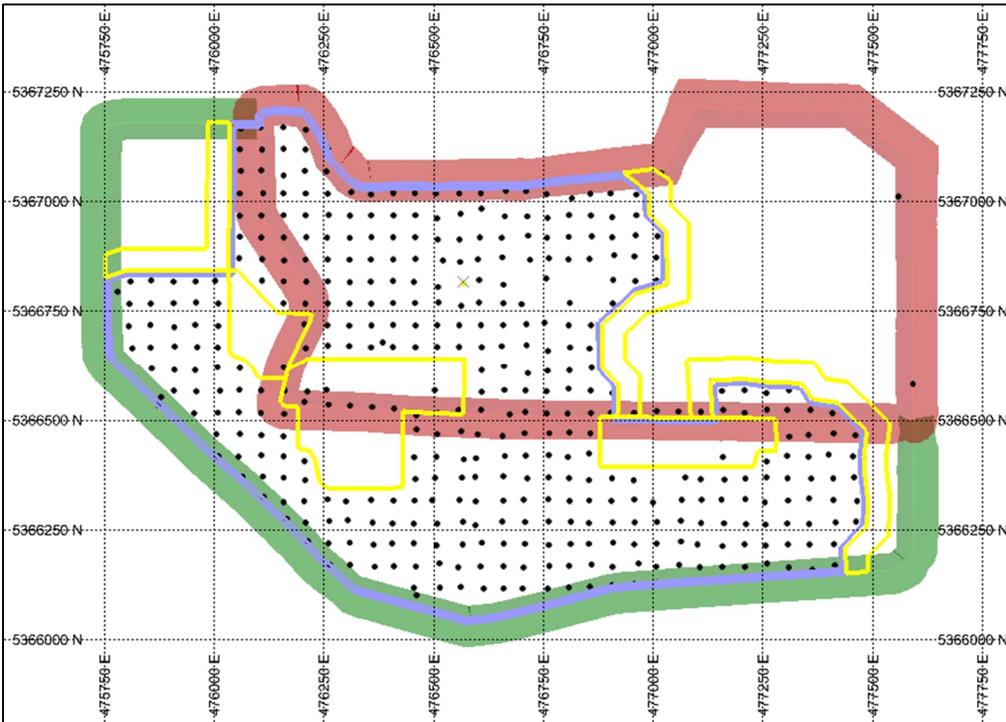
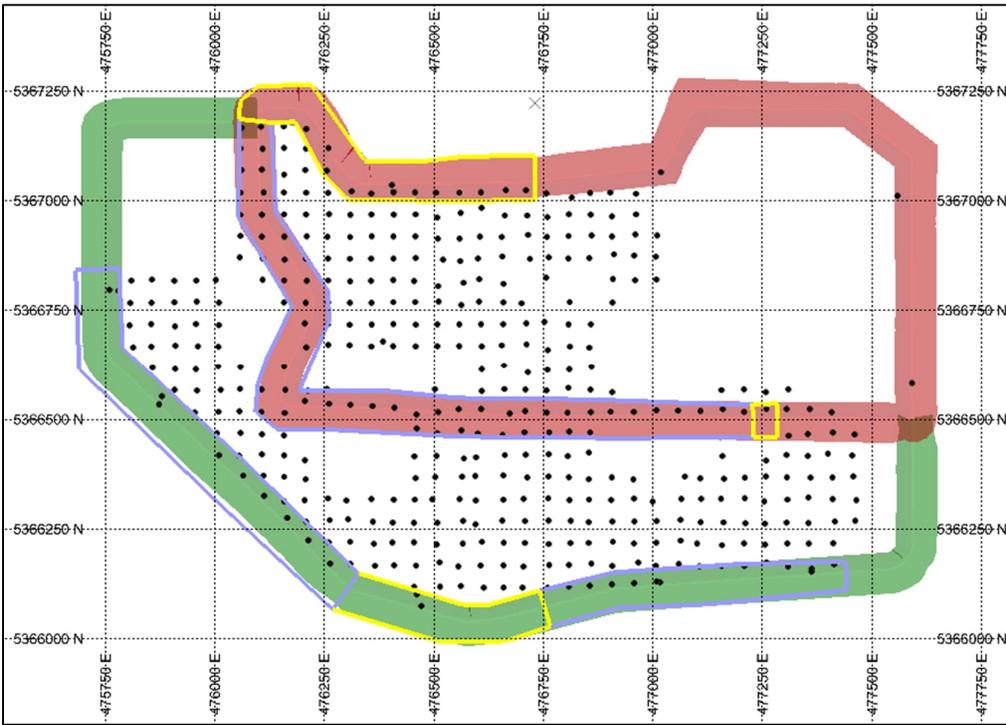
It is recognized that additional work is required to improve understanding of density and this is addressed in Recommendations (Item 14.6.2).

14.5.7 Resource Classification

The MRE was classified following the CIM Definition Standards for Mineral Resources and Mineral Reserves (May 2014). Resource classifications were assigned to broad regions of the block model based on QP confidence and judgement related to drill hole spacing, geological understanding, continuity of mineralization in conjunction with data quality, density and block model representativeness.

Classification was assigned by using plan polygons, independently for the dam walls and the dam cells (Figure 14.23), as follows:

- For the Phase 1 dam walls, Indicated Mineral Resources were defined at a nominal 50 m drill spacing along the wall and where the drill hole locations aligned well with the centreline of the wall. Inferred Mineral Resources were defined at a nominal 50 m drill spacing along the wall and where the drill hole locations were poorly aligned with the centreline of the wall (i.e., intersecting the toe of the wall).
- For the Phase 2 dam walls, Indicated Mineral Resources were defined where some drill holes intersected the wall and there was a nominal 50 m grid drill spacing adjacent to the wall. Inferred Mineral Resources were defined where very few drill holes intersected the wall and there was a nominal 50 m grid drill spacing adjacent to the wall.
- For the Phase 1 and Phase 2 cells, Indicated Mineral Resources were defined at a nominal 50 m grid drill spacing. Inferred Mineral Resources were defined as within 50 m of the exterior boundary of drill hole coverage and for areas inside the Indicated Mineral Resources polygon that had no drill hole coverage because of ponds.



Note: Blue polygons – Indicated Mineral Resource. Yellow polygons - Inferred Mineral Resource.

Figure 14.23: Mineral Resource Classification (Top - Dam Walls, Bottom – Dam Cells)

14.5.8 Reasonable Prospects for Eventual Economic Extraction (RPEEE)

Mineral Resources are reported at a 0.21 g/t Au break-even cut-off grade, and are supported by the following economic assumptions for potential open pit mining:

- Gold Price: CA\$ 4,140 (US\$3,000).
- Exchange Rate: \$ 1.38 CA\$ to \$ 1 US\$.
- Mining Recovery: 100%
- Mining Dilution: 0%.
- Gold Recovery: 61.3% (Item 13.0).
- Gold Payable: 99.95%.
- Royalty: 1.5%.
- Operating Costs: CA\$ 17 / tonne (\$ 2 Mining, \$ 2.50 Transportation, \$ 12 Processing, \$ 0.50 General, and Administration).

A Mineral Resource pit shell was created using the controls defined above and a pit wall slope angle of 30° (Figure 14.24, purple). Material below the 0.21 g/t Au break-even cut-off grade within the pit shell was isolated and the contiguous volumes greater than 2,500 m³ (Figure 14.24, blue) were considered to be separable (from ore) and, therefore, treated as waste and not included in the Mineral Resource.

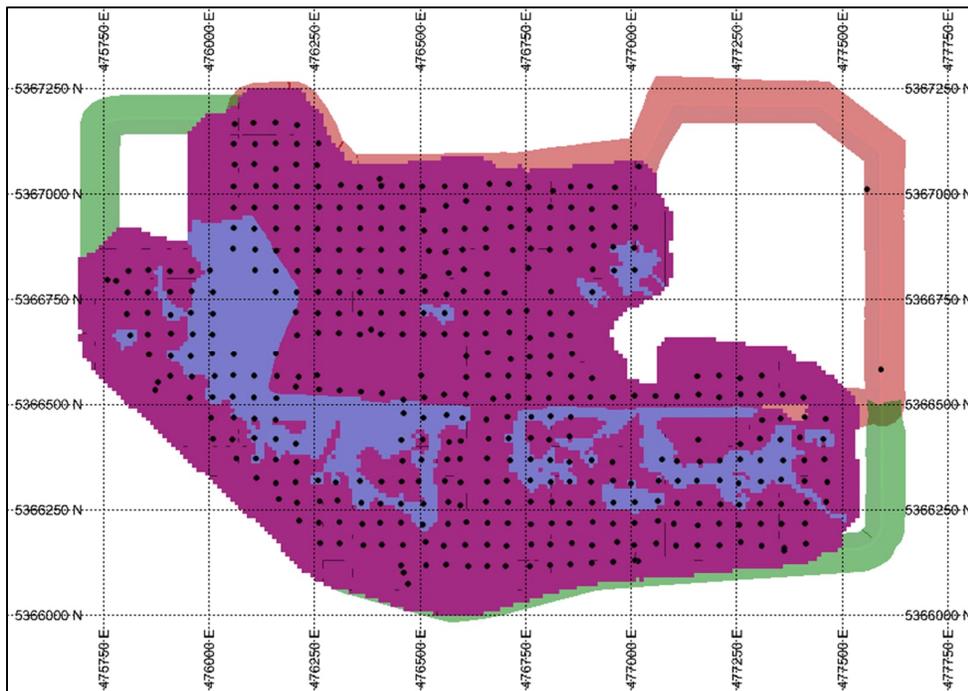


Figure 14.24: Mineral Resource Pit Shell

14.6 Mineral Resource Statement

Mineral Resources are not Mineral Reserves, and do not demonstrate economic viability. There is no certainty that all, or any part, of this Mineral Resource will be converted into Mineral Reserve. Inferred Mineral Resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorized as Mineral Reserves.

Table 14.6 summarizes the Indicated and Inferred Mineral Resources for the Project.

Table 14.6: Mineral Resource Estimate (Effective Date November 25, 2025)

Area	Indicated Resource			Inferred Resource		
	Tonnes (Mt)	Au Grade (g/t)	Contained Au (ozs)	Tonnes (Mt)	Au Grade (g/t)	Contained Au (ozs)
Phase 1	16.1	0.41	212,000	4.1	0.43	56,000
Phase 2	20.2	0.31	200,000	3.6	0.31	37,000
Total	36.2	0.35	412,000	7.7	0.37	93,000

Notes:

- (1) These mineral resources are not mineral reserves as they do not have demonstrated economic viability. The Hollinger MRE follows current CIM Definition Standards (2014) and CIM MRMR Best Practice Guidelines (2019). The resource estimate is presented as in-situ and undiluted and is considered to have reasonable prospects for eventual economic extraction.
- (2) The mineral resources are constrained by a resource pit shell based on a 0.21 g/t Au cut-off representing a truck and loader extraction scenario. The cut-off grade of 0.21 g/t Au was calculated using the following parameters: operating cost = CA\$17.00/t; payable gold = 99.95%; gold price = US\$3,000/oz; US\$/CA\$ exchange rate = 1.38; mill recovery of 61.3%.
- (3) The independent and qualified person for the Hollinger MRE, as defined by NI 43-101, is Brian Thomas, P.Geo. of WSP. The effective date of the MRE is November 25, 2025.
- (4) The estimation encompasses wireframes representing Phase 1 and Phase 2 walls and cells which contain the tailings material.
- (5) High-grade capping of assays was set at 1.3 g/t Au.
- (6) The estimate was completed with a sub-blocked model in Datamine Studio RM, with a parent block size of 10 m x 10 m x 1 m (X,Y,Z) and a minimum sub-block size of 2.5 m x 2.5 m x 0.5 m (X,Y,Z), using inverse distance squared (ID2) interpolation method based on 1m composite samples.
- (7) Density values for tailings material were assigned between 1.6 g/cm³ and 1.9 g/cm³ according to depth and differences between material in walls and cells. Estimates are reported on a dry, in-situ basis.
- (8) Hollinger Mineral Resources were classified as Indicated and Inferred. Indicated mineral resources were defined for blocks where drill hole spacing is 50 m or less and Inferred mineral resources where drill hole spacing is greater than 50 m.
- (9) Potential mining continuity was evaluated inside the pit shell by generating grade shells. Grade shells below cut-off within the resource pit shell with volumes greater than 2,500 m³ were assumed to be sortable and were excluded from the MRE. Grade shells below cut-off with volumes less than 2,500 m³ were assumed to be too small for sorting and included in the MRE.
- (10) The resource tonnage was rounded to the nearest 100,000 tonnes and the metal contents are presented in troy ounces (tonnes x grade / 31.10348) rounded to the nearest thousand ounces. Any discrepancies in the totals are due to rounding effects.
- (11) The Hollinger MRE is based on a 61.3% gold recovery rate via cyanide leaching at a 30-micron grid size. The Company also tested flotation at a 38-micron grind size and achieved 82.5% gold recovery with a 11.7% mass pull and grading 2.69 g/t Au, 2.3 g/t Ag and 16.5% sulphur.
- (12) As of the effective date of the MRE, the QP is not aware of any known environmental, permitting, legal, title-related, taxation, socio-political, or marketing issues or any other relevant issue that could materially affect the Hollinger MRE.

The sensitivity of the Indicated Mineral Resource to the cut-off is shown in Table 14.7 and Figure 14.25. Scenarios with cut-off grades below 0.21 g/t are not supported by reasonable prospects for eventual economic extraction and are shown for informational purposes only (MRE cut-off outlined in bold).

Table 14.7: Indicated Mineral Resource Cut-off Sensitivity Table

Cutoff (g/t)	Tonnes (Mt)	Au Grade (g/t)	Contained Au (ozs)
0.15	37.8	0.35	421,200
0.16	37.7	0.35	420,900
0.17	37.6	0.35	420,200
0.18	37.4	0.35	419,200
0.19	37.1	0.35	417,500
0.20	36.7	0.35	415,100
0.21	36.2	0.35	412,000
0.22	35.4	0.36	406,000
0.23	34.4	0.36	398,400
0.24	33.2	0.36	389,900
0.25	32.0	0.37	380,000
0.26	30.6	0.37	368,600
0.27	29.0	0.38	355,200
0.28	27.3	0.39	339,700
0.29	25.5	0.39	323,400
0.30	23.6	0.40	305,500

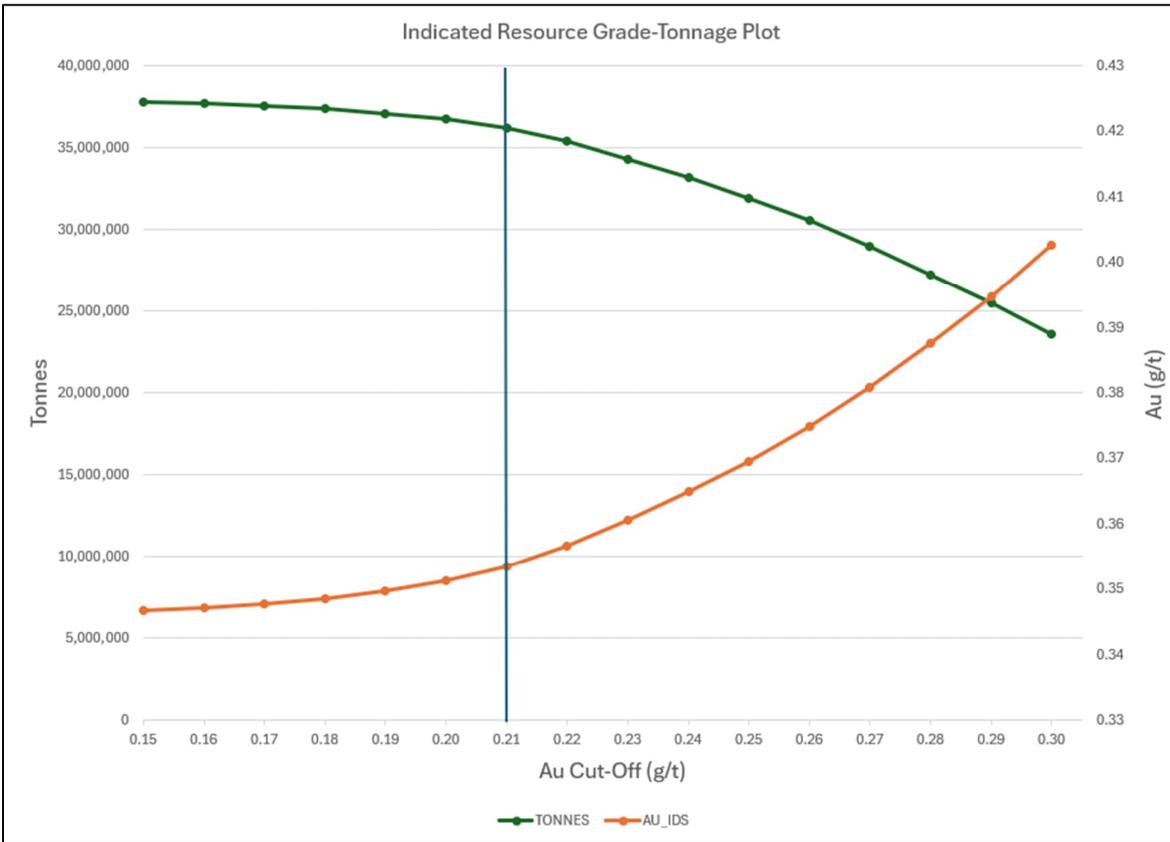


Figure 14.25: Indicated Mineral Resource Cut-off Grade/Tonnage Plot

Sensitivity of the Inferred Mineral Resource to the cut-off is shown in Table 14.8 and Figure 14.26 (MRE cut-off outlined in bold).

Table 14.8: Inferred Mineral Resource Cut-off Table

Cutoff (g/t)	Tonnes (Mt)	Au Grade (g/t)	Contained Au (ozs)
0.15	8.7	0.35	98,900
0.16	8.7	0.35	98,600
0.17	8.5	0.36	97,900
0.18	8.4	0.36	97,100
0.19	8.2	0.36	96,100
0.20	8.0	0.37	94,900
0.21	7.7	0.37	93,000
0.22	7.3	0.38	89,900
0.23	6.9	0.39	87,300
0.24	6.6	0.40	85,000
0.25	6.4	0.40	83,200
0.26	6.2	0.41	81,500
0.27	6.0	0.41	79,800
0.28	5.8	0.42	78,400
0.29	5.6	0.42	76,500
0.30	5.4	0.43	74,400

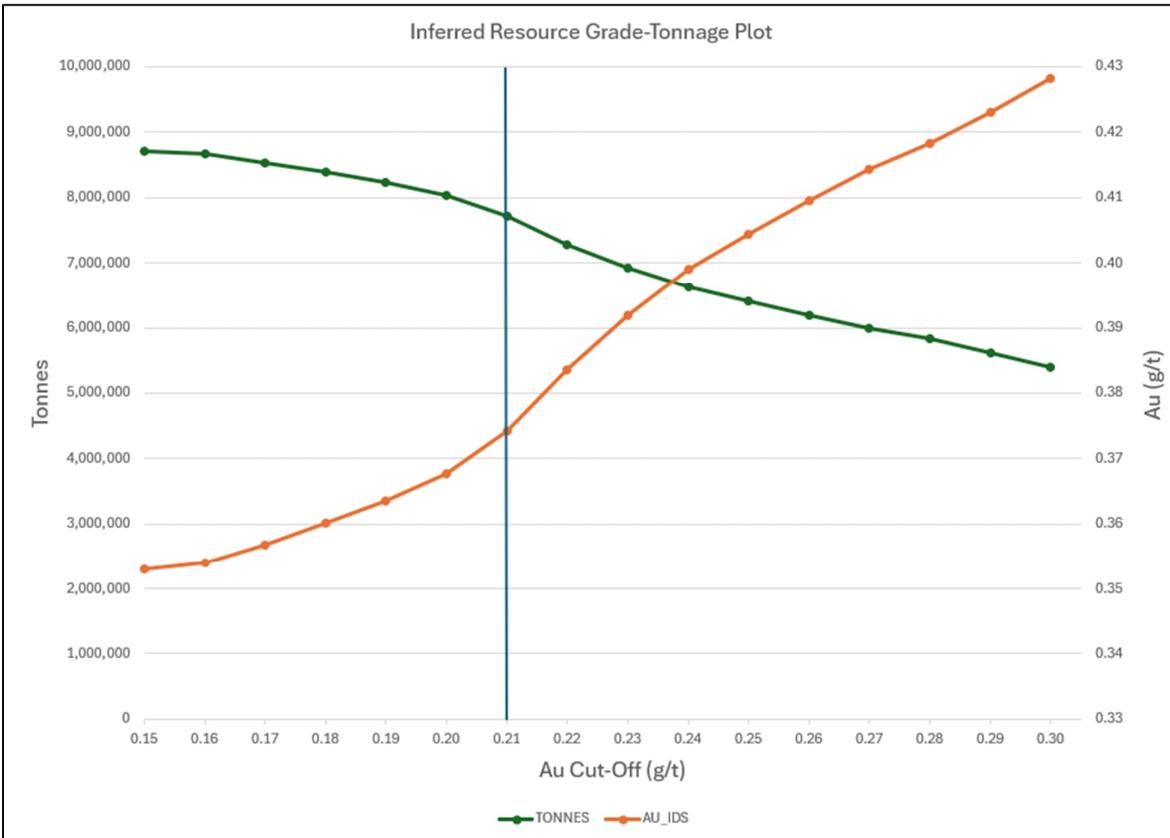


Figure 14.26: Inferred Mineral Resource Cut-off Grade/Tonnage Plot

14.6.1 Risks and Opportunities

The following risks and opportunities have been identified.

Potential risks are:

- The sample preparation methodology used may have the potential to introduce a bias into the sample data. Evaluation of coarse duplicate samples, as discussed in Item 12.0, indicated marginal precision for a portion of the sample population. No bias was identified in the metallurgical composite samples (sourced from original split core material) used for testworks described in Item 13.0, where the composite grades were consistent or higher than the expected grades. Further analysis of duplicate samples is recommended to evaluate the sample database for potential issues related to the sample preparation methodology.
- The location and dimensioning of the dam walls is based on information from 1951. The Phase 1 wall has the highest-grade material in the tailings deposit. There is uncertainty regarding the slope angles and dimensions of the walls which could impact the quantity and distribution of metal in the deposit. The Phase 1 wall accounts for about 11% of the Indicated Resource contained Au oz and 20% of the Inferred Resource contained Au oz, so while there is some uncertainty, it is unlikely to be material to the Mineral Resource. A recommendation has been made to mitigate the risk.
- There is a limited amount of density data. The method of density assignment used is reasonable based on the limited information available but there is some risk that the density is lower than defined. A recommendation has been made to mitigate the risk.

Potential opportunities include:

- There are several areas not covered by drill holes that are either identified as Inferred Resource or have no Mineral Resource at all. This includes the Northwest corner (Phase 2), which will have significant depth of tailings; the pond areas (Phase 1 and 2), some of which will have significant depth of tailings; and the Northeast corner (Phase 1), which although has shallower depths of tailings. Drilling in these areas has the potential to add Indicated and Inferred Resource.
- Uncertainty in the depth of the ponds could result in minor adjustments to the MRE.

The QP is not aware of any known environmental, permitting, legal, title-related, taxation, socio-political, or marketing issues or any other relevant issue that could materially affect the Hollinger MRE.

14.6.2 Recommendations

The QP has the following recommendations:

- It is recommended that STLLR conduct further investigation into the potential impacts of the sample preparation methodology used by analyzing approximately 10% of the remaining split core material and that any future analytical work uses either ALS PREP-31 or similar sample preparation procedures, or photon assay analytical methods which could avoid sample preparation issues.
- Gather additional dry bulk density data on an approximate 200-250 m grid spacing.
- Conduct infill drilling to target the existing gaps in the higher-grade Phase 1 wall and infill the areas where current drilling intersects the wall at poor angles or locations and in the pond areas.
- Complete step-out drilling outside of the current resource at a grid spacing of 50 x 50 m or 100 x 100 m to increase the size of the Indicated and/or Inferred resource.
- Consider a ground penetrating radar survey to confirm the slopes and locations of the Phase 1 and 2 walls and determine if other potential internal cell walls are present.

15.0 MINERAL RESERVE ESTIMATES

This Item is not applicable to this Technical Report.

16.0 MINING METHODS

This Item is not applicable to this Technical Report.

17.0 RECOVERY METHODS

This Item is not applicable to this Technical Report.

18.0 PROJECT INFRASTRUCTURE

This Item is not applicable to this Technical Report.

19.0 MARKET STUDIES AND CONTRACTS

This Item is not applicable to this Technical Report.

20.0 ENVIRONMENTAL STUDIES, PERMITTING, AND SOCIAL OR COMMUNITY IMPACT

This Item is not applicable to this Technical Report.

21.0 CAPITAL AND OPERATING COSTS

This Item is not applicable to this Technical Report.

22.0 ECONOMIC ANALYSIS

This Item is not applicable to this Technical Report.

23.0 ADJACENT PROPERTIES

The Project is located within the Timmins Mining Camp of northeastern Ontario, a region with more than a century of continuous mining activity and several major gold deposits. A number of mineral properties are situated adjacent to, or in the vicinity of, the Project. The deposits listed below are either currently producing in the area, or were developed alongside the Hollinger Mine, the source of the Hollinger Tailings discussed in this Technical Report.

The following descriptions are based solely on publicly available information, including company technical reports, assessment files, and government geological sources.

The QP has not independently verified the technical information for these adjacent properties, and the information is not indicative of the nature of the deposit, style of mineralization or grade profiles of the Project that is the subject of this Technical Report.

23.1 Hollinger Open Pit Mine

The Hollinger open pit is located approximately 2 km north of the Project. The original Hollinger Mine was discovered in 1909 by Benny Hollinger and became one of the most prolific gold mines in Canada, producing 19.3 million oz of gold between 1910 and 1968.

After the underground operations ceased in 1968, the site remained a legacy property. In the 2000s, exploration and feasibility work began, eventually leading to the decision to convert the site into an open pit mine. The project was formally launched in early 2014 by Porcupine Gold Mines, a subsidiary of Goldcorp Canada. Ore was safely extracted from in and around old workings, up until mid 2024, when mining operations were suspended. The number of oz produced at the Hollinger open pit between 2015 and 2024 is not publicly available. The only publicly available record is from 2024, when 79,000 oz of gold was produced from 2.01 Million tonnes (Mt) at an average grade of 1.35 g/t (Discovery Silver, 2025).

23.2 Dome Mine and Mill Complex

The Dome Mine lies approximately 11 km east of the Project and started production in 1910. Its discovery fueled the Porcupine Gold Rush, establishing Timmins as a major mining center, alongside the Hollinger and McIntyre mines, contributing significantly to Canada's early gold output. Public disclosures report past production from both open pit and underground operations, to around 17 million oz of Au. Even though mining operations ceased in 2017, there remain significant mineral resources at the Dome Mine as well as exploration potential, according to its current operator, Discovery Silver Corp. The 2025 Preliminary Economic Assessment report includes an inferred mineral resource totaling 2.29 Mt at an average grade of 1.49 g/t of gold.

The Dome Complex also includes the Dome Mill, which was built in the early 1980s, with upgrades completed in 1988, 1995, and 2004. The Dome process plant has a permitted capacity of up to 15,000 tpd, and a current operating capacity of approximately 12,000 tpd. The process plant operates 24 hours per day, 365 days per year and recovers approximately 92% of the gold in the combined mill feed (Discovery Silver, 2025).

23.3 McIntyre Mine

The McIntyre Mine is situated in the north shore of Pearl Lake, and approximately 3.5 km northeast of the Project. It was discovered between 1909 and 1911 and was in production between 1912 and 1988, with intermittent shutdowns. It produced 10.7 million oz of gold, with an average grade of 8.38 g/t. Along with the Hollinger and Dome mines, they form the "Big Three" historic mines that helped turn the Timmins gold camp into one of the world's great gold producing districts. Similarly to the Hollinger Mine, the McIntyre Mine

mineralization was hosted in quartz-carbonate veins. In addition to gold, McIntyre also produced copper ore starting in the 1960s.

The McIntyre tailings were reprocessed between 1988 and 1989, by a company called ERG Resources. The reclamation work removed a significant amount of tailings, leaving a pit which has been subsequently filled with water, forming Little Pearl Lake.

23.4 Hoyle Pond Mine

The Hoyle Pond Mine is located approximately 22 km east of the Project. It's an underground gold mine, which was discovered in 1969 by Texas Gulf Sulphur Company. Mining began in 1985 under then owner Kidd Creek Mines Ltd., and since then, it has produced over 4.0 million oz of gold. During its history, Hoyle Pond has been recognized as being among the highest-grade gold mines in North America with a strong track record for reserve replacement. Current mineral resources for Hoyle Pond include 1.16 Mt at an average grade of 12.9 g/t for 484,000 oz in the indicated category, and 578,000 tonnes at 15.24 g/t for 283,000 oz in the inferred category (Discovery Silver, 2025).

23.5 Bell Creek Mine and Mill Complex

The Bell Creek Complex includes the Bell Creek underground gold mine and the Bell Creek processing facility. The complex lies 19 km northeast of the Project. Gold mineralization on the Bell Creek property was first discovered in the early 1980s. The mine was developed in 1986, and the on-site mill was commissioned in 1987. Between 1987 and 1994 Bell Creek produced 576,000 short tons of ore at an average grade of 5.6 g/t, yielding 112,739 oz of gold. Historical gold recovery averaged around 93%.

The mine ceased operations in 1994, until 2007 when Lake Shore Gold Corp. (LSG), acquired the Bell Creek Mine and Mill from Porcupine Joint Venture, a joint venture between Placer Dome (later Goldcorp Canada), and Kinross Gold Corp. Under LSG, the mill was refurbished and underwent a series of expansions between 2010 and 2013. Current mill average throughput is reported at 4,400 tpd (Pan American Silver, 2025). The Bell Creek mine reported production between 2010 and 2020 was 4.07 Mt at an average grade of 3.9g/t, for a total of 486,700 oz of gold, according to the 2021 Updated Mineral Resource and Mineral Reserve Estimate for the Bell Creek Mine.

23.6 Timmins West Mine

The Timmins West Mine is an underground gold mine complex, situated 25 km west of the Project. It comprises three main deposits: the Timmins Deposit, Thunder Creek Deposit, and 144 Gap Deposit. The Timmins Deposit was the first to go into production in 2011, followed by the Thunder Creek Deposit. The 144 Gap Deposit was discovered in 2014. The mine is operated by Lake Shore Gold Corp. (a wholly own subsidiary of Pan American Silver Corp.). The ore is processed at the Bell Creek Mill. According to the 2021 Updated Mineral Resource and Mineral Reserve Estimate for the Timmins West Mine, the reported production between 2009 and 2021 was 9.38 Mt at an average grade of 3.7 g/t, for a total of 1.09 million oz of gold.

23.7 Kidd Creek Met Site

Glencore owns and operates the Kidd Creek mine, mill and metallurgical sites 23 km east of the City of Timmins. The Kidd Creek deposit type is a volcanic massive sulphide with mineralization occurring within rhyolitic volcanic and volcanoclastics. The massive sulphides are predominantly pyrite, pyrrhotite, sphalerite, and galena with underlying chalcopyrite stringer zones. Kidd Creek mine was discovered on November 8, 1963, by diamond drill hole K55-1 and was operational by 1966. The mine transitioned from an open pit mine to an underground mine in 1972 and has mined over 150,000 tonnes of ore producing copper, zinc and silver. The mine is scheduled to cease production in 2026 and commence closure plans in 2027. The Kidd Creek

Metallurgy site is 27 km from the Kidd Creek Mine, and has a concentrator, copper smelter, copper refinery, a zinc refiner, a cadmium plant, indium plant and acid plant (Glencore Website, 2025).

24.0 OTHER RELEVANT DATA AND INFORMATION

The authors are unaware of any additional data, information, or explanation that is necessary to make this Technical Report understandable and not misleading.

25.0 INTERPRETATION AND CONCLUSIONS

25.1 QA/QC and Database

The mineral resource QP conducted a personal site inspection of the project site and the core facility. No material issues were identified with the drilling, logging, sampling, QA/QC or chain of custody procedures and these procedures were determined to be consistent with industry practices.

Based on the limited duplicate sample data available, the QP identified that the sample preparation procedure used may have introduced a small relative bias in the assay data and resulted in marginal precision for a portion of the sample data. The QP concludes that the assay data is suitable for the purpose of modelling and grade estimation which form the basis of this maiden MRE but acknowledges that further testing and analysis is warranted. It is uncertain if the issues identified would have any material impact to the MRE as there was no indication of any grade bias issues in the metallurgical testwork, based on the 3 composite samples (100 kg) described in Item 13.0.

25.2 Mineral Resource Estimates

The MRE for the Project has been prepared in accordance with NI 43-101 and following the requirements of Form 43-101F1. The MRE follows the Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Estimation of Mineral Resource and Mineral Reserves Best Practices Guidelines (November 2019) and was classified following CIM Definition Standards for Mineral Resources & Mineral Reserves (May 2014).

The QP has taken reasonable steps to make the MRE as representative as possible. However, factors that could cause actual results to differ materially from the forward-looking information include any significant differences from one or more of the following material factors or assumptions that were applied in drawing the conclusions or making the estimates, forecasts or projections set forth in this Item, including: the suitability of the sample preparation method for assay, the assumptions used by the QP to prepare the data for resource estimation, the assumptions made in creating the dam walls structure, the interpretation of the mineral domain models, the selection of grade interpolation method, sample search and estimation parameters used for grade interpolation, continuity of mineralization and factors used to determine reasonable prospects for economic extraction.

25.3 Metallurgical

In the opinion of QP, the composite samples were appropriately prepared to represent the overall tailings resource in terms of spatial distribution, depth, and average gold grade per sediment type. Gravity separation testing resulted in low gold recoveries, indicating that gravity methods are unsuitable for processing the Hollinger Tailings.

Initial bottle roll assays indicated baseline recoveries of direct leaching without regrinding remained low. Finer grinding improved gold extraction; recoveries for composites 1 and 2 were in the range of 60%, while Composite 3 achieved approximately 69% recovery at the finest tested P80 of around 30 µm. The diagnostic leach underscores the potential to enhance gold recovery from the Hollinger Tailings by integrating oxidization procedures.

Flotation conducted at fine grind sizes yielded strong gold recoveries, reaching up to 85.1%. Concentrate grades had a weighted average of 2.69 g/t.

25.4 Project Risk Summary

The Project Risk Summary is provided Table 25.1.

Table 25.1: Project Risk Summary

Risk Category	Specific Risk	Potential Outcomes	Mitigating Measures
Sample Preparation	Potentially biased sample data with marginal precision for a portion of the population	Adjustment of mineral resources.	Further evaluation of 10% of remaining core to characterize risk.
Dry density data	Limited measurements	Potential adjustments resource tonnage and metal content.	Collect more density measurements on a 200 – 250 m grid spacing.
Dam construction	Volume of higher-grade material in walls	Confirmation of metal content.	Conduct a GPR survey.

26.0 RECOMMENDATIONS

26.1 QA/QC and Database

The QP recommends that a representative 10% of remaining core be analyzed using a standard preparation procedure for rock such as ALS PREP-31 package consisting of crushing, pulverization and riffle splitting, or optionally photon analysis, to ensure a representative and unbiased assay preparation and analysis methodology in order to further evaluate the sample database.

26.2 Mineral Resource Estimates

The QP has the following recommendations:

- Collect more dry bulk density data on an approximate 200-250 m grid spacing.
- Conduct infill drilling to target the existing gaps in the higher-grade Phase 1 wall and infill the areas where current drilling intersects the wall at poor angles or locations and in the pond areas.
- Complete step-out drilling outside of the current resource at a grid spacing of 50 x 50 m or 100 x 100 m to increase the size of the Indicated and/or Inferred resource.
- Consider a ground penetrating radar survey to confirm the slopes and locations of the Phase 1 and 2 walls and determine if other potential internal cell walls are present.

26.3 Metallurgical

In future studies, it is recommended to expand testing across drill samples from multiple locations to capture variability in gold recovery, conduct direct cyanidation at finer grind sizes with repeatability studies for consistency, and incorporate oxidative pre-treatment methods to address refractory gold. Furthermore, broader flotation trials should be conducted if market conditions are favourable. Consideration should also be given to developing a dedicated flowsheet tailored to local mill treatment options, as well as evaluating rare earth element recovery for its potential economic benefits.

26.4 Project Recommendations

Table 26.1 provides overall recommendations for the next phase of the Project.

Table 26.1: Project Recommendations

Type	Description	Amount (CA\$ thousands)
QA/QC Database	Conduct field duplicate analysis of 10% of tailings samples	54 ¹
MRE	Collect dry bulk density measurements on a 200-250 m grid spacing	350 ²
	Infill drilling, targeting existing gaps and pond areas	515
	Step-out drilling to increase resource	2,330 ³
	Ground penetrating radar survey	30 ⁴
Metallurgical	Expanded metallurgical test work	200 ⁵
	Albion tests	60 ⁵
Total		3,539

Notes:

1. 1,200 samples at \$45 per sample
2. 200 m spaced grid, 700 m of drilling at \$466 per metre rounded up
3. 5,000 m at \$466 per metre
4. Assumed only equipment rental
5. Cost estimate provided by WSP

27.0 REFERENCES

- ASTM D2216. Standard Test Method for Laboratory Determination of Water (Moisture) Content of Soil and Rock by Mass. ASTM International. West Conshohocken, PA. <http://www.astm.org/>.
- ASTM D2488. Standard Practice for Description and Identification of Soils (Visual-Manual Procedure). ASTM International. West Conshohocken, PA. <http://www.astm.org/>.
- ASTM D4044-96(2008). Standard Test Method for (Field Procedure) for Instantaneous Change in Head (Slug) Tests for Determining Hydraulic Properties of Aquifers. ASTM International. West Conshohocken, PA. <http://www.astm.org/>.
- ASTM D4318. Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils. ASTM International. West Conshohocken, PA. <http://www.astm.org/>.
- ASTM D6913. Standard Test Methods for Particle-Size Distribution (Gradation) of Soils Using Sieve Analysis. ASTM International. West Conshohocken, PA. <http://www.astm.org/>.
- ASTM D7928. Standard Test Method for Particle-Size Distribution (Gradation) of Fine-Grained Soils Using the Sedimentation (Hydrometer) Analysis. ASTM International. West Conshohocken, PA. <http://www.astm.org/>.
- ASTM D854. Standard Test Methods for Specific Gravity of Soil Solids by Water Pycnometer. ASTM International. West Conshohocken, PA. <http://www.astm.org/>.
- Ayers, J.A., Trowell, N.F., Amelin, Y., and Corfu, F. (1999). Project Unit 95-24. Geological compilation of the Abitibi Greenstone Belt in Ontario: Toward a revised stratigraphy based on compilation and new geochronology results. In Summary of Field Work and Other Activities 1998, Ontario Geological Survey Miscellaneous Paper 169, p. 14 – 24.
- Bateman, R., Ayer, J.A., Dubé, B. and Hamilton, M.A. (2005). The Timmins–Porcupine gold camp, northern Ontario: the anatomy of an Archaean greenstone belt and its gold mineralization: Discover Abitibi Initiative. Ontario Geological Survey, Open File Report 6158, 90p.
- Bieniawski, Z.T. (1989). Engineering Rock Mass Classifications. Wiley, New York.
- Blue Heron Environmental (BH). (2024). 2023 Water Quality Monitoring Report for Erocon Waste Management.
- Burrows, D.R., Spooner, E.T.C., Wood, P.C., and Jemielita, R.A. (1993). Structural controls on formation of the Hollinger-McIntyre Au quartz vein system in the Hollinger Shear Zone, Timmins, southern Abitibi greenstone belt, Ontario. *Economic Geology*, v.88, p.1643-1663.
- C. von Hessert. (1984). Report to Energy & Resources (CAM) Limited On the Hollinger Tailings Dump, Timmins, Ontario. C. von Hessert & Associates Ltd, Toronto, Canada.
- Canadian Geotechnical Society. (2006). Canadian Foundation Engineering Manual, 4th Edition. BiTech Publishers Ltd., British Columbia, Canada.
- Coad, P. (2000). Cameco Gold Inc., Report on the 1999 Phase 2 Work Program, Kayorum Project, Tisdale Township, Ontario, NTS 42IA06.
- Cowan, Dick, (June 26, 2021). Hollinger Tailings Case Study, Timmins: Emergency to Legislative Changes, Orphaned & Abandoned Mines Workshop, Ministry of Northern Development and Mines, Winnipeg, Manitoba

- Davis, James B., Millions, William J., McNulty, Gerald, and Moneta Porcupine Mines Inc. (November 1, 1996) Agreement.
- Discovery Silver. (2025. December 8). Dome Mill. <https://discoverysilver.com/projects/porcupine/dome-mill>
- Discovery Silver. (2025. December 8). Dome Mine. <https://discoverysilver.com/projects/porcupine/dome-mine>
- Discovery Silver. (2025. December 8). Hoyle Pond. <https://discoverysilver.com/projects/porcupine/hoyle-pond>
- Discovery Silver. (2025. December 8). Porcupine Operations.
<https://discoverysilver.com/projects/porcupine/porcupine-operations>
- Dubé, B., Mercier-Langevin, P., Ayer, J., Pilote, J., and Monecke, T. (2020). Gold deposits of the world-class Timmins-Porcupine camp, Abitibi green-stone belt, Canada. Society of Economic Geologists, Special Publication 23, p. 53–80.
- Erocon Waste Management Inc. (November 2021). Hollinger Tailings Wood Waste Landfill Design and Operations Plan.
- Glencore Canada Corporation. (2025). Glenore Official Website. www.glencore.com.
- Hvorslev, M.J. (1951). Time Lag and Soil Permeability in Ground-Water Observations. Bull. No. 36. Waterways Exper. Sta. Corps of Engrs, U.S. Army, Vicksburg, Mississippi. pp. 1-50.
- Kallio, E., Roque, P., Barnett, R. (2025. January 13). Porcupine Complex Ontario, Canada NI 43-101 Technical Report on Preliminary Economic Assessment. Discovery Silver.
- Kayorum and Moneta. (February 21, 1989). Sale Agreement between Kayorum Gold Mines Ltd. and Moneta Porcupine Mines Inc.
- Labrador Mining and Exploration Company Limited and Moneta Porcupine Mines Inc. (May 28, 1987). Agreement.
- Labrador Mining and Exploration Company Limited and Moneta Porcupine Mines Inc. (February 21, 1989). Agreement.
- Lachapelle, E., Mainville, A., Felsher, D. (2021. June 30). National Instrument 43-101 Technical Report, Updated Mineral Resource and Mineral Reserve Estimate for the Bell Creek Mine Property, Hoyle Township, Timmins, Ontario, Canada. Pan American Silver.
- Lachapelle, E., Mainville, A., Felsher, D. (2021. June 30). National Instrument 43-101 Technical Report, Updated Mineral Resource and Mineral Reserve Estimate for the Timmins West Mine Property, Bristol Township, Timmins, Ontario, Canada. Pan American Silver.
- Mill Staff. (April 1951). Mill Trailing Disposal at Hollinger, Hollinger Consolidated Gold Mines, Limited, Annual General Meeting, Quebec, City, Quebec, Transactions, Volume LIV, 255-263)
- Ministry of Environment, Conservation and Parks (2022). AMENDED ENVIRONMENTAL COMPLIANCE APPROVAL A770068
- Morin, M.A. (July 1993) Report for the Work Performed Up tot June 30, 1993, Under the Exemption Order In-Council (MNDM-2) For the Timmins Tailings Projects.
- Morin, M.A., Cooper, L., Reitzel, S., n.d. The Remediation of the Hollinger Tailings Stack - A Case Study in Government Response to a Problem.

- Ontario Inc. and Erocon Waste Management Ltd. Land Purchase Option Agreement. (January 22, 2025). 1001108570.
- Ontario Geological Survey (1973). Report on Magnetometer and Electromagnetic Surveys Covering Albert Lepic Property Claim P 354953 Tisdale Township Ontario by H. D. Carlson, Ph. D., P. Eng. Consulting Geologist. (Assessment File Number 42A06NW0016, AFRO Num 2.1298, RGP File Number T-1582). <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NW0016>.
- Ontario Geological Survey (1983). Diamond Drill Report of HK-83-3. (Assessment File Number 42A06NW0004 AFRO Num 17, RGP File Number T-2585, Work Report Number W8306.00217) <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NW0004>.
- Ontario Geological Survey (1983). Laboratory Results (Assaying and Analyses and Expenditure) issued to Mr Jean Roy, (508825 Ontario Limited) Box 1184, Timmins, ON P4N 7J5 (Assessment File number 42A06NW0026, AFRO Num 2.6960, RGP File Number T-2556, Work Report Number W8406.00267). <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NW0026>.
- Ontario Geological Survey (1984). Report to Energy and Resources (Cam) Limited on the Hollinger Tailings Dump Timmins, Ontario by Von Hessert & Associates Ltd. (Assessment File Number 42A06NW0023, AFRO Number 63.4650). <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NW0023>.
- Ontario Geological Survey (1985). Laboratory Results (Assaying and Analyses and Expenditure) issued to Mr Jean Roy, (508825 Ontario Limited) Box 1184, Timmins, ON P4N 7J5 (Assessment File number 42A06NW0025, AFRO Num 2.7981, RGP File Number T-2556, Work Report Number W8406.00267). <https://www.geologyontario.mines.gov.on.ca/assessment/42A06NW0025>.
- Ontario Geological Survey (1987). Diamond Drilling Performed for 508825 Ontario Limited on Claim No. P577600. (Assessment File number 42A06NW0021, AFRO Num 26, RGP File Number T-2556). <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NW0021>
- Ontario Geological Survey (1987). Diamond Drilling Performed for 508825 Ontario Limited on Claim No. P577600. (Assessment File number 42A06NW0021, AFRO Num 26, RGP File Number T-2556). <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NW0021>
- Ontario Geological Survey (1991). Cogema Canada Limited Kayorum Project, Surface Mapping and Sampling (1991 Program). (Assessment File number 42A06NW2001, AFRO Num OM91-123, RGP File Number T-3526). <https://www.geologyontario.mines.gov.on.ca/assessment/42A06NW2001>
- Ontario Geological Survey (1991). Cogema Canada Ltd Kayorum Project, Tisdale and Delopo Townships, Porcupine Mining District, Ontario. Operations Report on Total Field Magnetic, VLF-EM and Horizontal Loop EM Surveys. (Assessment File number 42A06NW0017, AFRO Num 63.6079, RGP File Number T-3526). <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NW0017>
- Ontario Geological Survey (1993). Cogema Canada Limited Kayorum Project Diamond Drill Program, Summer 1992. (Assessment Report Ref 93-CND-64-07. Assessment File Number 42A06NW0040. <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NW0040>
- Ontario Geological Survey. (1980). Report on an Aeromagnetic Survey South Timmins Area Ontario for Amax Minerals Exploration Limited. (Assessment File number 42A06NE0007, AFRO Num 2.3367, RGP File Number T-1978). <https://www.geologyontario.mines.gov.on.ca/persistent-linking?assessment=42A06NE0007>.

O. Reg 169/92: Exemption For Emergency Activities on Three Abandoned Mines Sites in the Township of Tisdale and Deloro City of Timms. (March 25, 1992). MNDM 02.

Pan American Silver. (2025, December 8). Timmins Ontario, Canada.
<https://panamericansilver.com/operations/gold-segment/timmins>

Pyke, D.R. (1982). Geology of the Timmins area, District of Cochrane. Ontario Geological Survey, Report 219, 141 p., Map 2455.

Skeries, R and Nicholson, K (2012). Moneta Porcupine Mines Kayorum Property Summary Report, Porcupine Mining Division, Timmins, Ontario NTS 42A/06. [Unpublished internal report]. Exploration Department, Moneta Porcupine Mines, Inc.

Skeries, R and Nicholson, K. (2012). Moneta Porcupine Mines Kayorum Property Summary Report, Porcupine Mining Division, Timmins, Ontario NTS 42A/06. Internal Report.

Statistics Canada. (2021). 2021 Census of Population geographic summary: Kirkland Lake, Town (T) [Census subdivision], Ontario. Retrieved December 9, 2025, from <https://www12.statcan.gc.ca/census-recensement/2021/dp-pd/geo/summary-sommaire/index-eng.cfm?Lang=E>

Statistics Canada. (2021). 2021 Census of Population geographic summary: Timmins, City (CY) [Census subdivision], Ontario. Retrieved December 9, 2025, from <https://www12.statcan.gc.ca/census-recensement/2021/search-recherche/productresults-resultatsproduits-eng.cfm?LANG=E&GEOCODE=2021A00053556027>

STLLR Gold Inc. (2025). Internal Report on Drilling Program, STLLR Gold Inc. Hollinger Tailings Project in Deloro, Mountjoy, Ogden and Tisdale Townships, Porcupine Mining Division, Northeastern Ontario, NAD83 UTM Zone 17N (573,445E and 5,372,432N) for the Period of January 1, 2025, to September 30, 2025. [Unpublished report]. Exploration Department, STLLR Gold Inc. Timmins, ON.



wsp.com